AGENDA Lexington Planning Board

Thursday, July 19, 2018 Selectmen's Meeting Room, Town Office Building, 1625 Massachusetts Avenue 7:00 PM

Staff Reports

- 1. General Updates (as needed)
- 2. Hartwell Avenue Zoning Initiative Update

Development Administration

- 1. 167-177 Cedar St (Winding Road): Conventional Subdivision Tripartite Reduction Request
- 2. 443 Lincoln Street: Definitive Balanced Housing Development Discuss Decision
- 3. 8 Adams Street: Definitive Site Sensitive Development (Public Hearing)
- 4. 55 & 56 Watertown Street (Belmont Country Club): Planned Development (Public Hearing)

Board Administration

- 1. Board Member Updates
- 2. Comprehensive Plan Update
- 3. Upcoming Meetings & Anticipated Schedule
- 4. Minutes

Adjourn



Meeting broadcast by LexMedia

LEXINGTON PLANNING BOARD

ITEM NUMBER:

AGENDA ITEM TITLE:

General Updates (as needed)

PRESENTER:

Carol Kowalski

SUMMARY:

The general update is a standing agenda item providing the Planning Office staff the opportunity to update the community and Board on day-to-day matters.

SUGGESTED MOTION:

Staff's update requires no action on the part of the Board.

FOLLOW-UP:

DATE AND APPROXIMATE TIME ON AGENDA:

7/19/2018

LEXINGTON PLANNING BOARD

AGENDA ITEM TITLE:

Hartwell Avenue Zoning Initiative Update

PRESENTER:

Carol Kowalski

SUMMARY:

This is a standing agenda item to provide updates to the Planning Board on the status of the Hartwell Zoning Initiative.

SUGGESTED MOTION:

Staff's update requires no action on the part of the Board.

FOLLOW-UP:

DATE AND APPROXIMATE TIME ON AGENDA:

7/19/2018

ITEM NUMBER:

LEXINGTON PLANNING BOARD

AGENDA ITEM TITLE:

167-177 Cedar St (Winding Road): Conventional Subdivision Tripartite Reduction Request

<u>ITEM</u> NUMBER:

PRESENTER:

David Kucharsky

SUMMARY:

Applicant, Finnegan Development, is seeking to reduce their existing tripartite agreement by \$171,673.16.

SUGGESTED MOTION:

FOLLOW-UP:

DATE AND APPROXIMATE TIME ON AGENDA:

7/19/2018

LEXINGTON PLANNING BOARD

AGENDA ITEM TITLE:

443 Lincoln Street: Definitive Balanced Housing Development Discuss Decision

PRESENTER:

<u>ITEM</u> <u>NUMBER:</u>

SUMMARY:

During the June 21st meeting the Planning Board closed the public hearing. Board will discuss their decision on this item. Please click **here** to view latest plans and relevant documents. A revised plan set showing changes made to the on-site trail connections was added 07/16/2018.

SUGGESTED MOTION:

FOLLOW-UP:

DATE AND APPROXIMATE TIME ON AGENDA:

7/19/2018

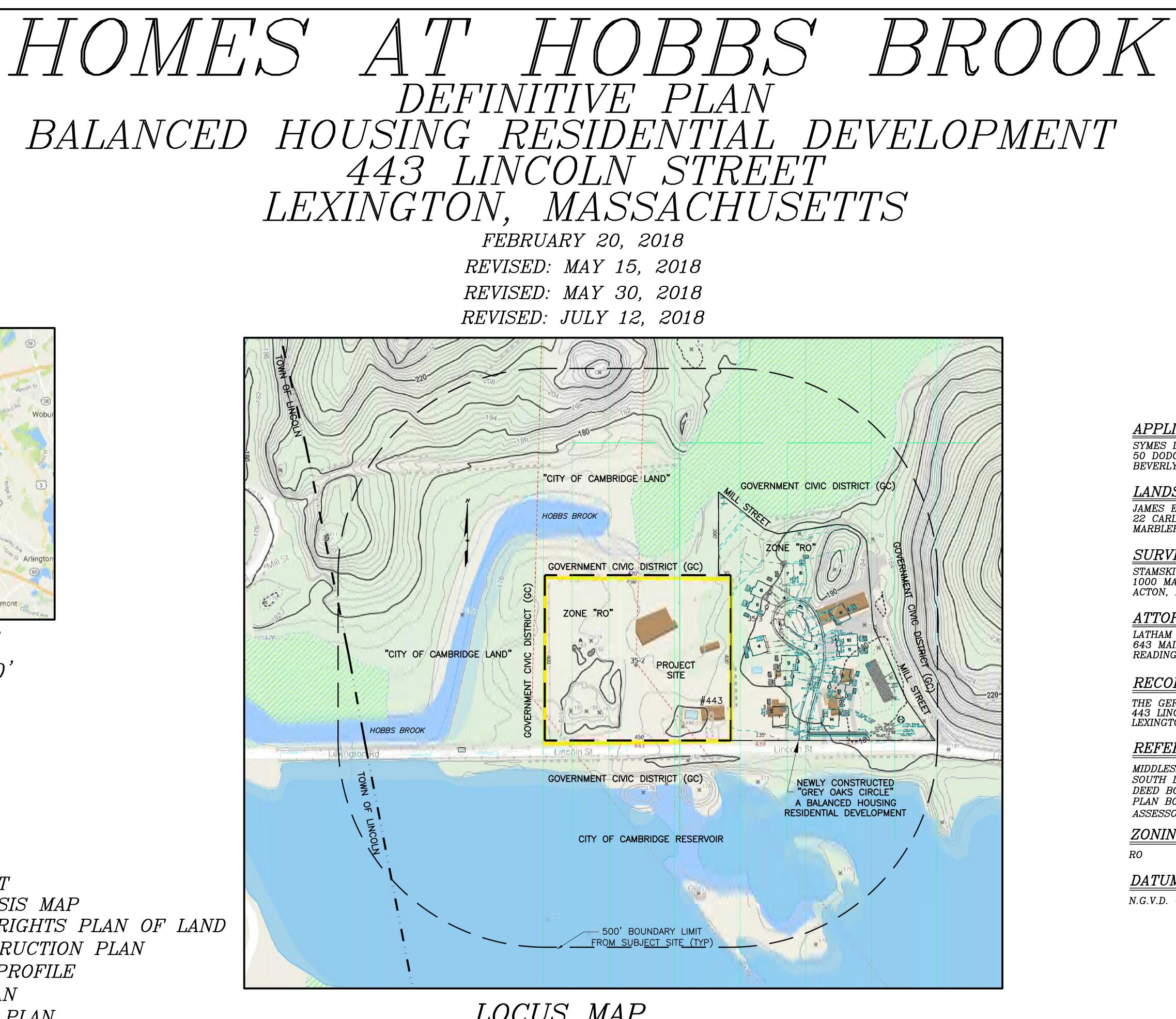
ATTACHMENTS:

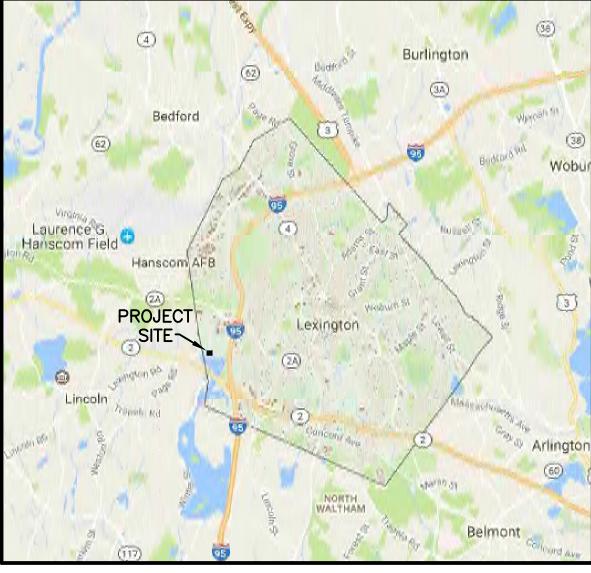
Description

Plan Set (revised 07/16/2018)

Туре

Backup Material





TOWN LOCUS SCALE: 1"=10,000'

SHEET INDEX

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SHEET	1	TITLE SHEET	
SHEET	2	SITE ANALYSIS MAP	
SHEET	3	PROPERTY RIGHTS PLAN OF LAND	
SHEET	4	SITE CONSTRUCTION PLAN	
SHEET	5	PLAN AND PROFILE	
SHEET	6	UTILITY PLAN	
SHEET	7	LANDSCAPE PLAN	
SHEET	8	CONVENTIONAL SUBDIVISION PROOF	PLAN
SHEET	9-10	CONSTRUCTION DETAILS	
SHEET	11	EROSION AND SEDIMENT CONSTROL	PLAN

LOCUS MAP SCALE: 1"=120'

0 60 120 240 360 480

480 FT

APPLICANT

SYMES DEVELOPMENT & PERMITTING, LLC 50 DODGE STREET BEVERLY, MA 01915

LANDSCAPE ARCHITECT

JAMES EMMANUEL, ASSOCIATES 22 CARLTON ROAD MARBLEHEAD, MA 01945

SURVEYOR/ENGINEER

STAMSKI AND MCNARY, INC. 1000 MAIN STREET ACTON, MA 01720

ATTORNEY

LATHAM LAW OFFICES, LLC 643 MAIN STREET READING, MA 01867-3096

RECORD OWNER

THE GERTRUDE M. PIANTEDOSI TRUST 443 LINCOLN STREET LEXINGTON, MA

REFERENCE

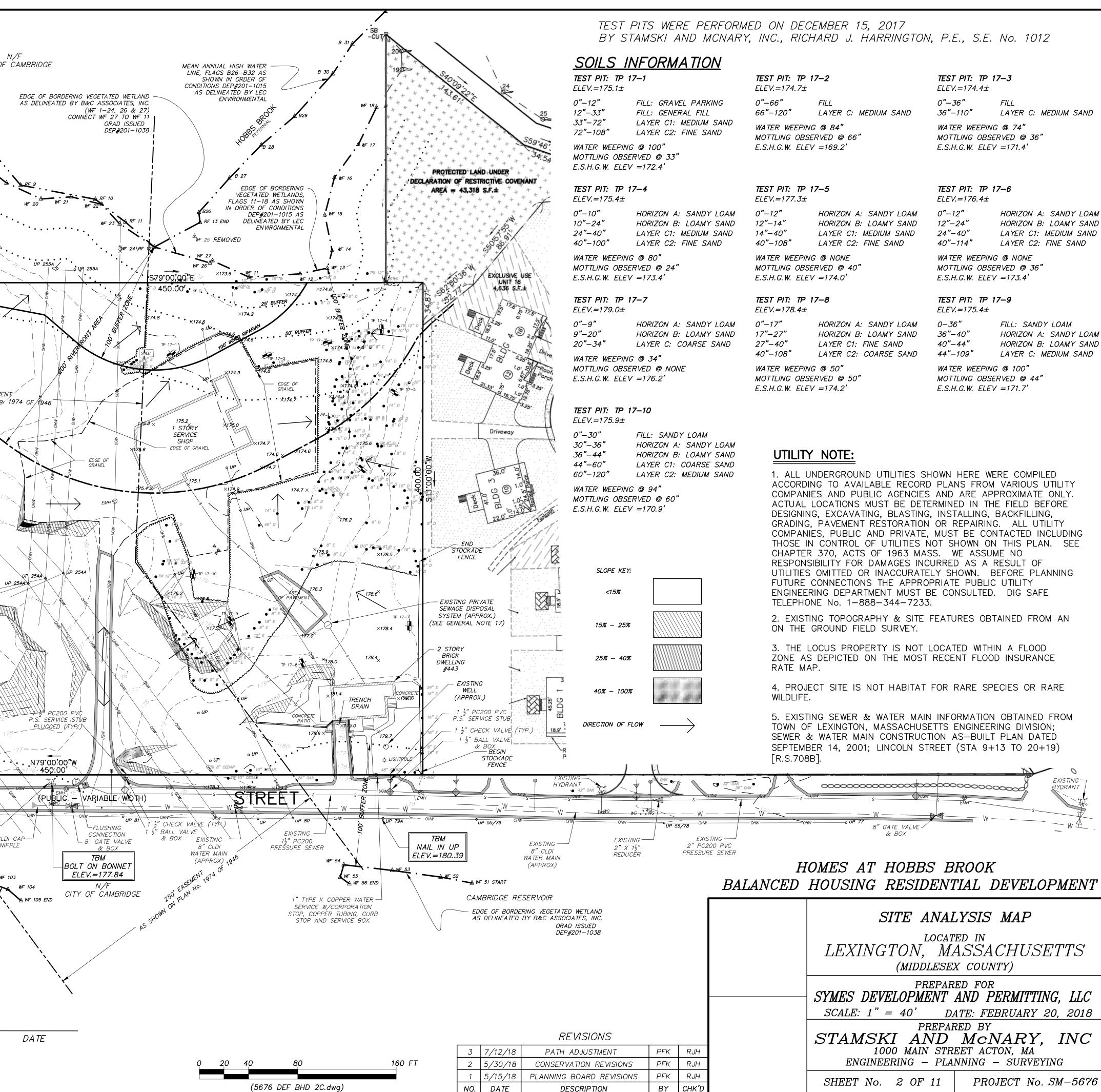
MIDDLESEX REGISTRY OF DEEDS SOUTH DISTRICT DEED BOOK 65347 PAGE 366 PLAN BOOK 239 PLAN 26 ASSESSOR'S MAP 35 PARCEL 2

ZONING DISTRICT

DATUM

N.G.V.D. OF 1929

LEGEND:	
N/F NOW OR FORMERLY OVERHEAD WIRES TREE TREE LINE UP UTILITY POLE GG• GAS GATE	$\begin{array}{c} \text{MEAN ANNUAL HIGH-WATER} \\ \text{ATED BY B&C ASSOCIATES, INC.} \\ \text{ON SEPTEMBER 27, 2016} \\ (RF 1-13) \\ \text{CONNECT RF 13 TO B26} \\ \text{ORAD ISSUED} \\ \text{DEP#201-1038} \\ \text{DEP#201-1038} \\ \text{WF 13} \\ \text{WF 14} \\ \text{WF 15} \\ \text{WF 16} \\ \text{WF 16} \\ \text{WF 17} \\ \text{WF 18} \\ \text{WF 18} \\ \text{WF 19} \\ \text{WF 10} \\ $
EDGE OF BORDERING VEGETATED WETLAND AS DELINEATED BY B&C ASSOCIATES, INC. ON SEPTEMBER 27, 2016 ORAD ISSUED DEP#201-1038 MEAN ANNUAL HIGH-WATER AS DELINEATED BY B&C ASSOCIATES, INC. ON SEPTEMBER 27, 2016 ORAD ISSUED RF 4	MHO MHO MHO MHO MHO MHO MHO MHO
DEP#201-1038	HO HO HO HO HO HO HO HO HO HO
RF 3 WF 4	-175- OHW OHW OHW OHW OHW OHW OHW OHW OHW OHW
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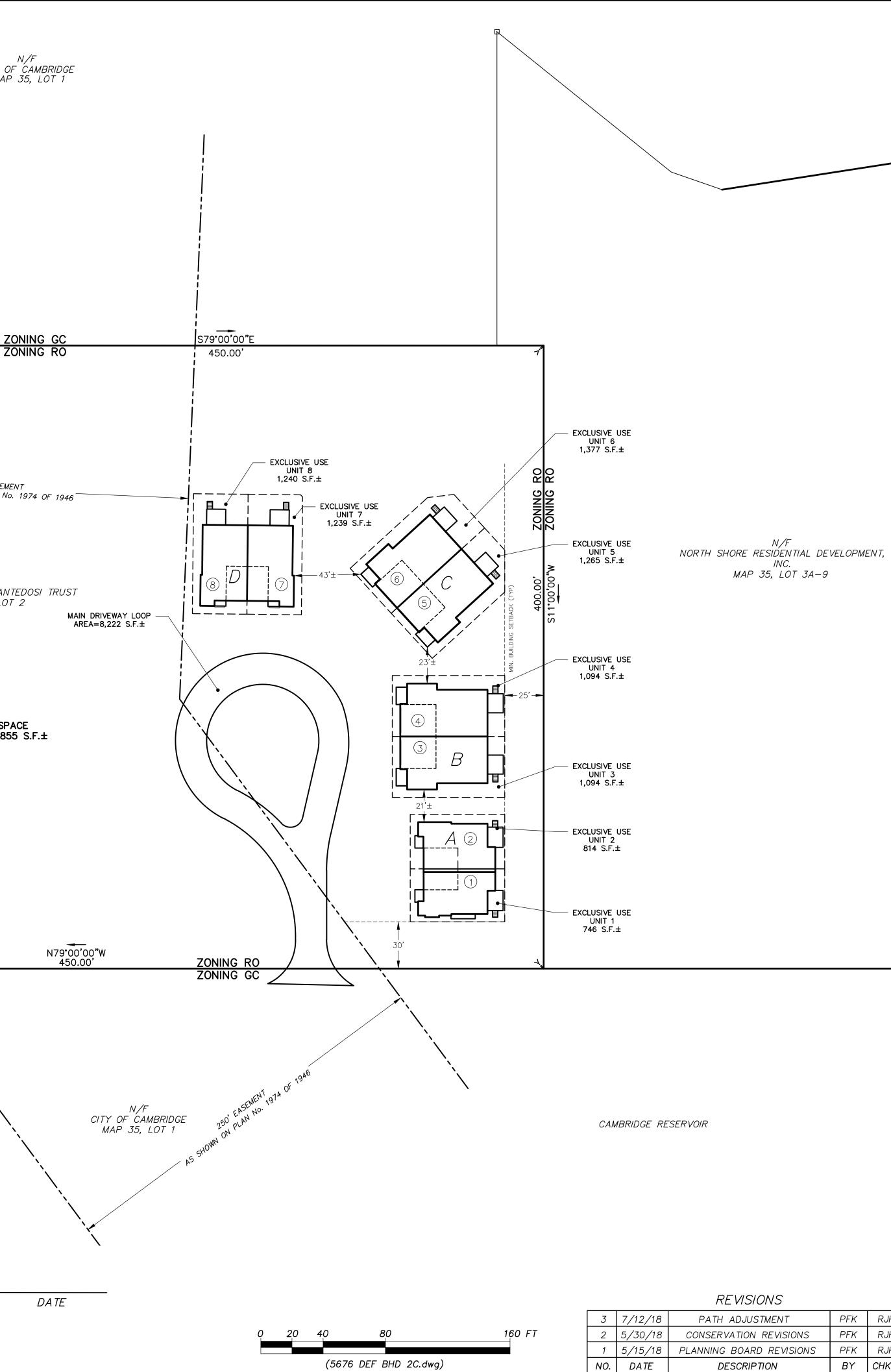


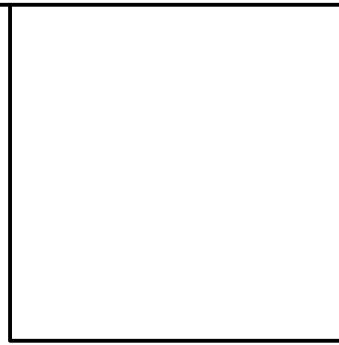
FILL: SANDY LOAM
HORIZON A: SANDY LOAN
HORIZON B: LOAMY SANI
LAYER C1: COARSE SANL
LAYER C2: MEDIUM SAND
'ING @ 94"
3SERVED @ 60"

TEST PIT: TP ELEV.=177.3±	17–5
0"–12" 12"–14" 14"–40" 40"–108"	HORIZON A: SANDY LOAM HORIZON B: LOAMY SAND LAYER C1: MEDIUM SAND LAYER C2: FINE SAND
WATER WEEPIN MOTTLING OBS E.S.H.G.W. ELE	ERVED @ 40"

0"—12"	HORIZON A: SANDY LOAM
12"—24"	HORIZON B: LOAMY SAND
24"-40"	LAYER C1: MEDIUM SAND
40"—114"	LAYER C2: FINE SAND
WATER WEEPING	
MOTTLING OBSER	₹ <i>VED @ 36"</i>
	177 1

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	Z Z Z AS SHOWN ON PLAN NG
	N/F THE GERTRUDE M. PIAN MAP 35, LOT SITE 180,000 S.F.±. 4.1322 AC.± OPEN SP AREA=135,85
"THIS PLAN IS SUBJECT TO A COVENANT DATED" "THIS PLAN IS SUBJECT TO A CERTIFICATE OF ACTION DATED"	CAMBRIDGE RESERVOIR
"THIS PLAN IS SUBJECT TO A SPECIAL PERMIT DATED" I,, CLERK OF THE TOWN OF LEXINGTON, MASSACHUSETTS HEREBY CERTIFY THAT THE NOTICE OF APPROVAL OF THIS PLAN BY THE LEXINGTON PLANNING BOARD HAS BEEN RECEIVED AND RECORDED AT THIS OFFICE AND NO NOTICE OF APPEAL WAS RECEIVED DURING THE TWENTY DAYS NEXT AFTER SUCH RECEIPT AND RECORDING OF SAID NOTICE. TOWN CLERK DATE	LEXINGTON PLANNING BOARD





FOR REGISTRY OF DEEDS USE ONLY

I DECLARE, TO THE BEST OF MY PROFESSIONAL KNOWLEDGE, INFORMATION, AND BELIEF, THAT THIS PLAN WAS PREPARED IN ACCORDANCE WITH THE RULES AND REGULATIONS OF THE REGISTERS OF DEEDS.

JOSEPH MARCH, PLS

DATE

LEGEND:

N/F	NOW OR FORMERLY
——он <i>w</i> ——	OVERHEAD WIRES
٢٠	TREE
	TREE LINE
UP	UTILITY POLE
GG •	GAS GATE
G	GAS SERVICE (BURIED)
WG•	WATER GATE
— <i>w</i> ——	WATER SERVICE (BURIED)
	DRAIN MANHOLE
<i>D</i>	SUB-SURFACE DRAIN LINE
99	EXISTING CONTOUR
— <i>— 95</i> — — –	EXISTING CONTOUR
¢	LIGHTPOLE
\triangle	WETLAND FLAG
99X9	SPOT ELEVATION
00000	STONE WALL
	EDGE OF PAVEMENT
	PROPOSED PERVIOUS PAVEMENT

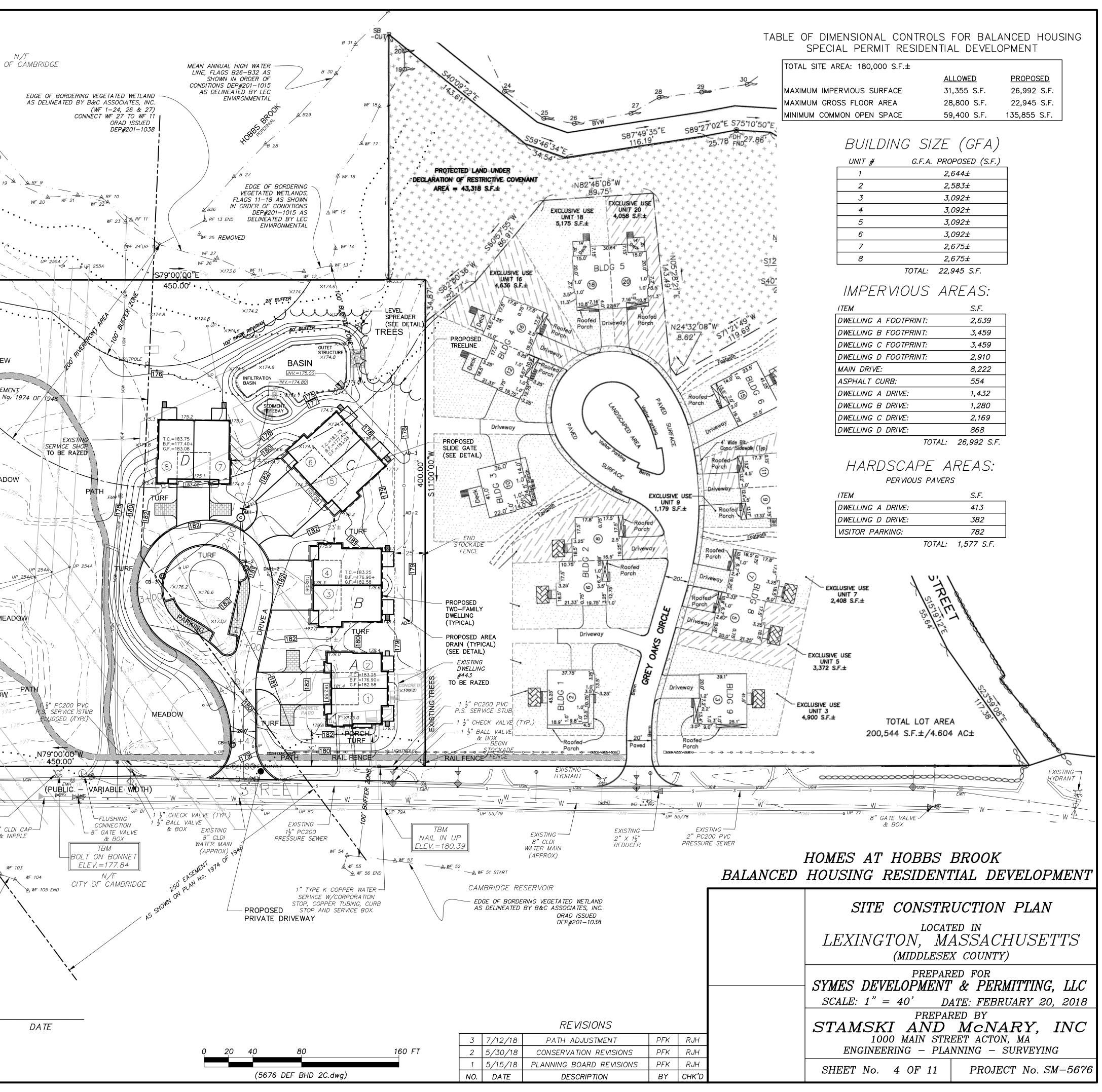
NOTE:

OPEN SPACE EXCLUDES BUILDINGS, EXCLUSIVE USE AREAS, AND THE MAIN DRIVEWAY LOOP.

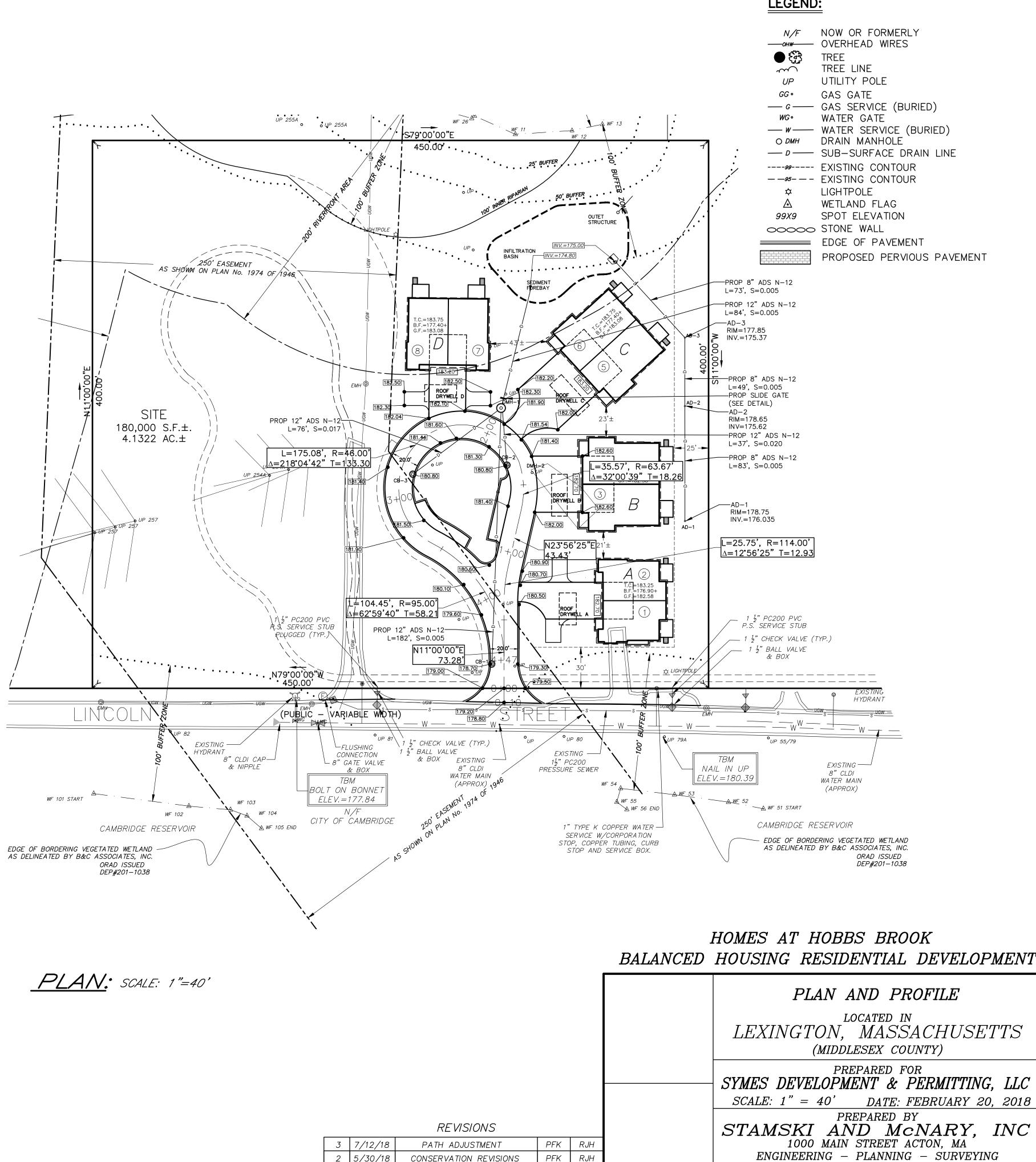
HOMES AT HOBBS BROOK BALANCED HOUSING RESIDENTIAL DEVELOPMENT

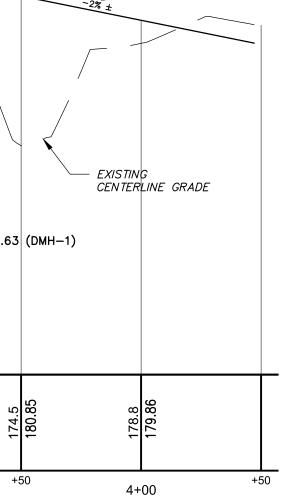
			PROPERTY RIGHTS PLAN OF LAND Located in LEXINGTON, MASSACHUSETTS (MIDDLESEX COUNTY)
		,	PREPARED FOR SYMES DEVELOPMENT & PERMITTING, LLC SCALE: 1" = 40' DATE: FEBRUARY 20, 2018 PREPARED BY
PFK PFK	RJH RJH		STAMSKI AND MCNARY, INC 1000 main street acton, ma engineering – planning – surveying
PFK BY	RJH CHK'D		SHEET No. 3 OF 11 PROJECT No. SM-5676

LEGEND:	
N/F NOW OR FORMERLY — онw—— OVERHEAD WIRES	MEAN ANNUAL HIGH-WATER AS DELINEATED BY B&C ASSOCIATES, INC.
TREE INE	AS DELINEATED BY B&C ASSOCIATES, INC. ON SEPTEMBER 27, 2016 (RF 1–13) CONNECT RF 13 TO B26
UP UTILITY POLE	ORAD ISSUED DEP#201-1038
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99X9 SPOT ELEVATION	
OOOOO STONE WALL EDGE OF PAVEMENT	
PROPOSED PERVIOUS PAVEMENT	
↓ /	
EDGE OF BORDERING VEGETATED WETLAND / / AS DELINEATED BY B&C ASSOCIATES, INC.	
ON SEPTEMBER 27, 2016 ORAD ISSUED DEP#201–1038	
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	VISTA V
	AS SHOWN ON PLAN
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DEP#201-1038	
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	EDGE OF BORDERING VEGETATED WETLAND AS DELINEATED BY B&C ASSOCIATES, INC.
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THE NOTICE OF APPROVAL OF THIS PLAN BY THE LEXINGTON PLANNING BOARD HAS BEEN RECEIVED AND RECORDED AT	
THIS OFFICE AND NO NOTICE OF APPEAL WAS RECEIVED DURING THE TWENTY DAYS NEXT AFTER SUCH RECEIPT AND RECORDING OF SAID NOTICE.	



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2	181.4	179.9	178.4	178.2	179.48	217.43	37.96	2	184.33	183.25	182.58	176.
3	176.3	178.6	178.4	177.0	177.58	213.60	36.03	3	184.33	183.25	182.58	176
4	176.3	178.6	178.5	175.9	177.33	213.60	36.28	4	184.33	183.25	182.58	176
5	174.7	175.6	177.7	174.2	176.05	214.10	38.05	5	184.83	183.75	183.08	177
6	174.7	175.6	174.3	174.6	174.80	214.10	39.30	6	184.83	183.75	183.08	177
7	175.1	175.2	175.1	174.9	175.08	214.68	39.61	7	184.83	183.75	183.08	177
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RE	VISIC	DNS

3	7/12/18	PATH ADJUSTMENT
2	5/30/18	CONSERVATION REVISIO
1	5/15/18	PLANNING BOARD REVIS
NO.	DATE	DESCRIPTION

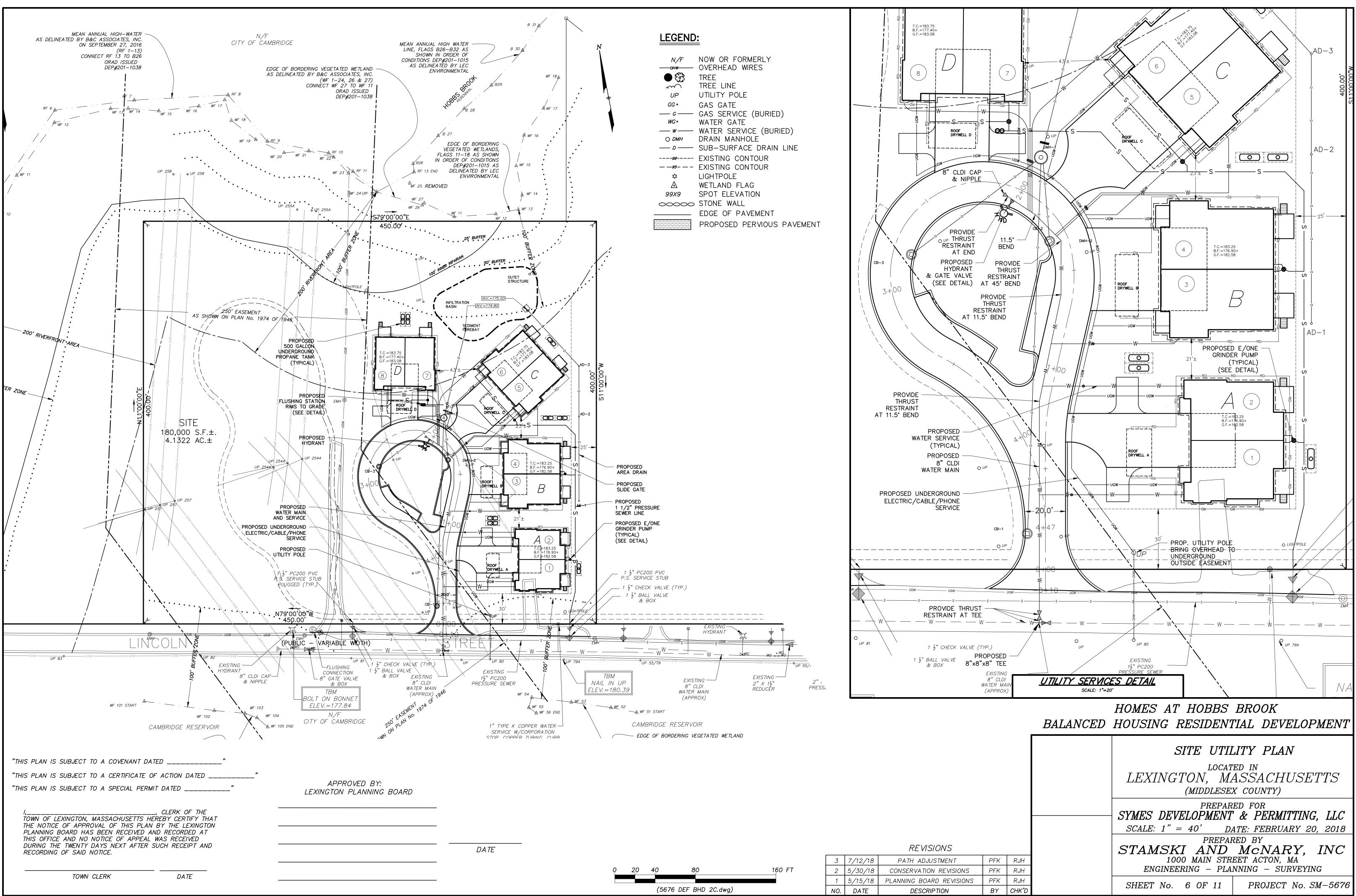
(5676 DEF BHD 2C.dwg)

LEGEND:

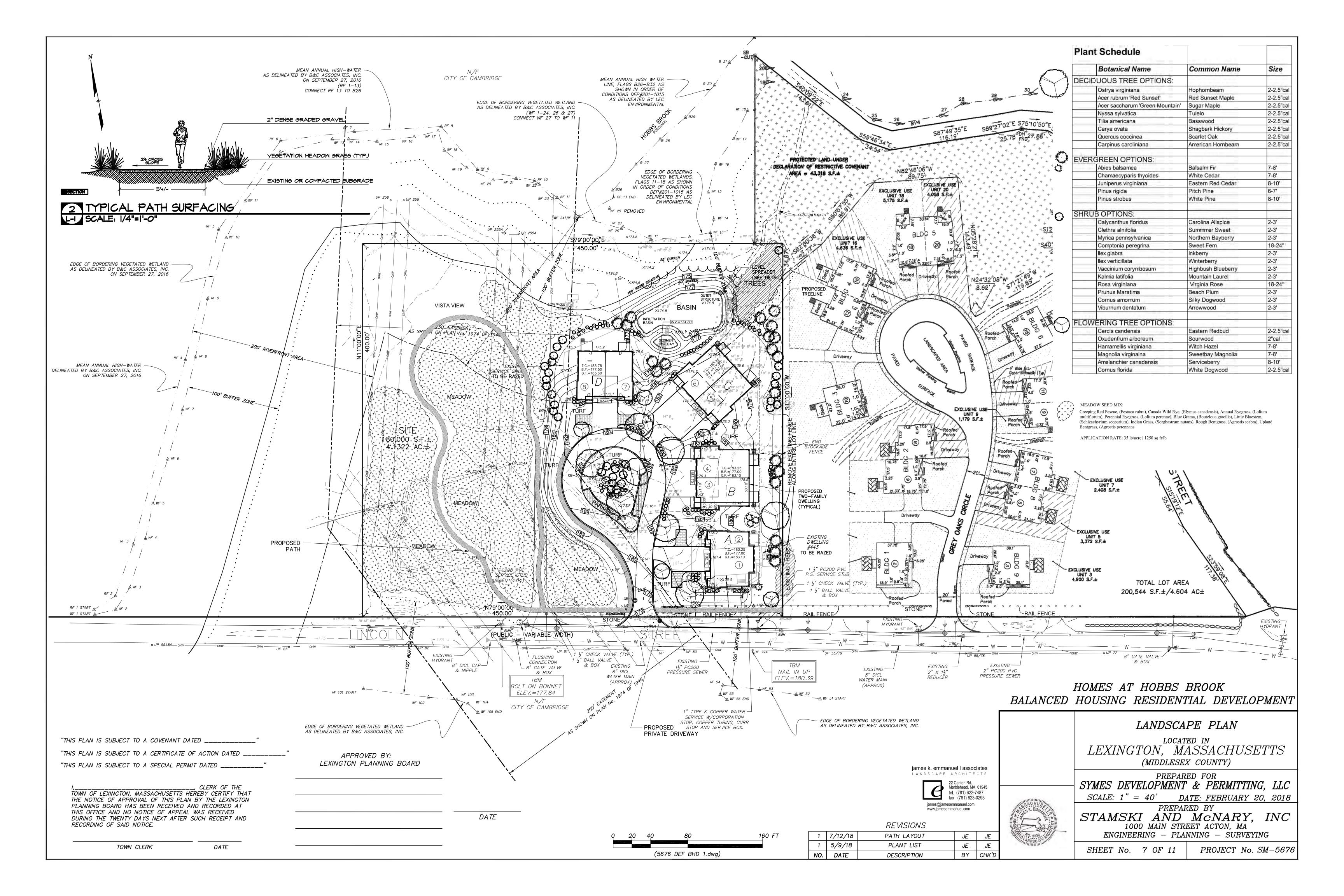
SHEET No. 5 OF 11

PROJECT No. SM-5676

-	PFK	RJH	
IONS	PFK	RJH	
SIONS	PFK	RJH	
	BY	СНК'Д	



					REVISIONS
			3	7/12/18	PATH ADJUSTMENT
0 20 40	80	160 FT	2	5/30/18	CONSERVATION REVISION
			1	5/15/18	PLANNING BOARD REVISIO
(5	676 DEF BHD 2C.dwg)		NO.	DATE	DESCRIPTION



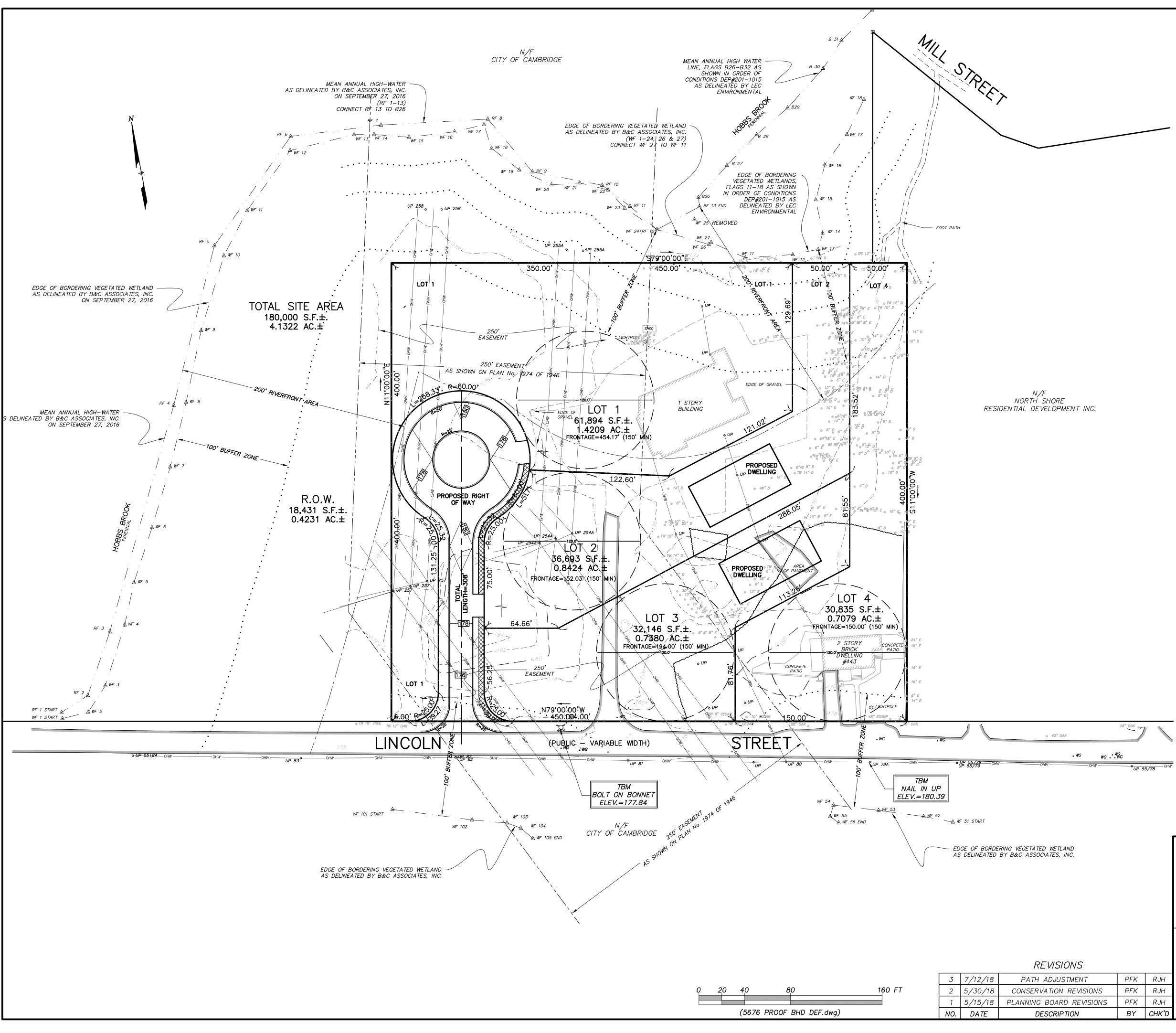


TABLE OF DEVELOPMENT DATA - BALANCED HOUSING DEVELOPMENT TOTAL LAND AREA: 180,000 S.F. \pm TOTAL LAND AREA FOR 4 LOTS: 161,569 S.F. \pm TOTAL LAND AREA WITHIN PROP RIGHT OF WAY (ROW): 18,431 S.F.± AREA OF IMPERVIOUS SURFACES WITHIN ROW: 11,967 S.F.+ MAX. GROSS FLOOR AREA (4 LOTS X 7,200 S.F.): 28,800 S.F. MAX. AREA OF IMPERVIOUS SURFACE: 31,355 S.F.± 4 LOTS; AREA 161,569 S.F. X 0.12 = 19,388 S.F.± IMPERVIOUS SURFACE WITHIN ROW = 11,967 S.F.± NUMBER OF DWELLINGS - NO LIMIT SITE COVERAGE – NO LIMIT MINIMUM COMMON OPEN SPACE: 59,400 S.F.± (TOTAL LAND AREA X 33%) EACH DWELLING TO BE PROVIDED WITH A CRAWL SPACE WITH A FLOOR TO CEILING HEIGHT LESS THAN SEVEN FEET.

: 6,067 S.F.

ON-SITE RIVERFRONT AREA: 60,666 S.F.

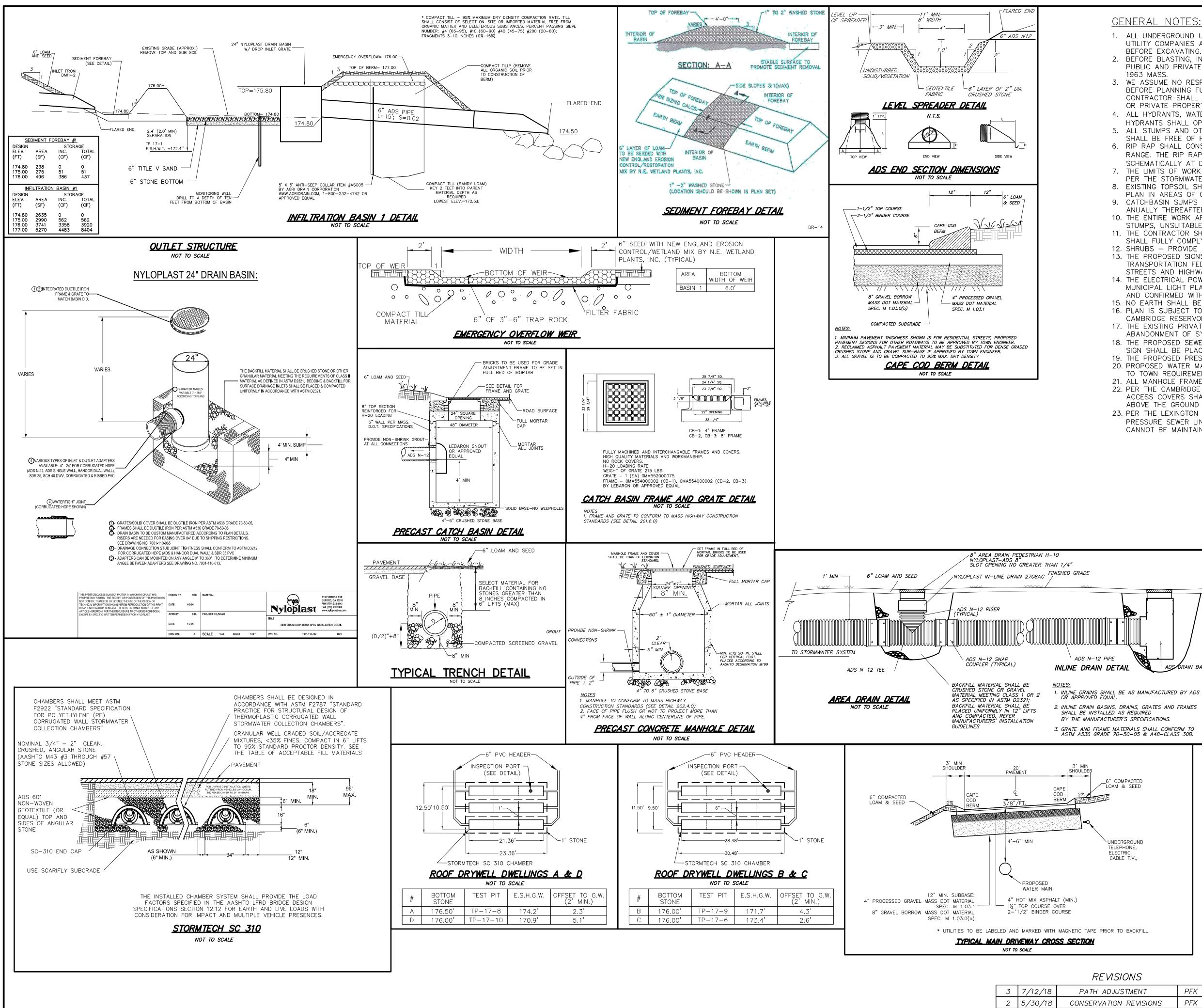
LEGEND:

10% MAX

N/F 	NOW OR FORMERLY OVERHEAD WIRES TREE TREE LINE UTILITY POLE
GG •	
	GAS GATE
— G ——	GAS SERVICE (BURIED)
WG•	WATER GATE
— <i>w</i> ——	WATER SERVICE (BURIED)
O DMH	DRAIN MANHOLE
D	SUB-SURFACE DRAIN LINE
99	EXISTING CONTOUR
— <i>— 95</i> — — –	EXISTING CONTOUR
¢	LIGHTPOLE
\bigtriangleup	WETLAND FLAG
99X9	SPOT ELEVATION
00000	STONE WALL
	EDGE OF PAVEMENT

HOMES AT HOBBS BROOK BALANCED HOUSING RESIDENTIAL DEVELOPMENT

			CONVENTIONAL SUBDIVISION PROOF PLAN Located in LEXINGTON, MASSACHUSETTS (MIDDLESEX COUNTY)
			PREPARED FOR SYMES DEVELOPMENT AND PERMITTING, LLC SCALE: 1" = 40' DATE: FEBRUARY 20, 2018 PREPARED BY STAMSKI AND MCNARY, INC
	PFK PFK	RJH RJH	1000 MAIN STREET ACTON, MA ENGINEERING – PLANNING – SURVEYING
S	PFK PFK BY	RJH CHK'D	SHEET No. 8 OF 11 PROJECT No. SM-5676



GENERAL NOTES:

1. ALL UNDERGROUND UTILITIES SHOWN HERE WERE COMPILED ACCORDING TO AVAILABLE RECORD PLANS FROM VARIOUS UTILITY COMPANIES AND PUBLIC AGENCIES AND ARE APPROXIMATE ONLY. ACTUAL LOCATIONS MUST BE DETERMINED BEFORE EXCAVATING.

2. BEFORE BLASTING, INSTALLING, BACKFILLING, GRADING, OR PAVEMENT RESTORATION OR REPAIR, ALL UTILITY COMPANIES, PUBLIC AND PRIVATE, MUST BE CONTACTED, INCLUDING THOSE IN CONTROL OF UTILITIES. SEE CHAPTER 370, ACTS OF 1963 MASS.

3. WE ASSUME NO RESPONSIBILITY FOR DAMAGES INCURRED AS A RESULT OF UTILITIES OMITTED OR INACCURATELY SHOWN. BEFORE PLANNING FUTURE CONNECTIONS, THE APPROPRIATE UTILITY ENGINEERING DEPT. MUST BE CONSULTED. THE CONTRACTOR SHALL NOTIFY PUBLIC UTILITY COMPANIES AT LEAST 72 HOUSE PRIO TO DIGGING OR EXCAVATING ON PUBLIC OR PRIVATE PROPERTY. DIG SAFE TEL. NO. 1-888-344-7233.

4. ALL HYDRANTS, WATER VALVES, VALVE BOXES, ETC SHALL BE AMERICAN MADE; VALVES SHALL OPEN RIGHT (CLOCKWISE), HYDRANTS SHALL OPEN RIGHT (CLOCKWISE), PER TOWN OF LEXINGTON REQUIREMENTS. 5. ALL STUMPS AND OTHER CONSTRUCTION DEBRIS SHALL BE PROPERLY REMOVED FROM THE SITE. ANY FILL MATERIAL USED SHALL BE FREE OF HAZARDOUS MATERIALS, WASTE, AND CONSTRUCTION DEBRIS.

6. RIP RAP SHALL CONSIST OF HARD DURABLE STONE, ANGULAR IN SHAPE, THAT IS WELL GRADED WITHIN THE 25# TO 125# RANGE. THE RIP RAP SHALL BE PLACED OVER A 12" BASE OF COARSE BANK RUN GRAVEL. RIP RAP SHOWN SCHEMATICALLY AT DRAINAGE OUTFALLS SHALL BE PLACED FOR A 3' WIDTH AND 6' LENGTH UNLESS OTHERWISE SPECIFIED.

7. THE LIMITS OF WORK SHALL BE CLEARLY MARKED IN THE FIELD PRIOR TO THE START OF CONSTRUCTION OR SITE CLEARING PER THE STORMWATER POLLUTION PREVENTION PLAN. 8. EXISTING TOPSOIL SHALL BE STRIPPED, STOCKPILEDM SCREENED AND SPREAD TO REQUIRED DEPTHS AS SHOWN ON THE PLAN IN AREAS OF GENERAL LOAM AND SEED.

9. CATCHBASIN SUMPS AND STORM WATER BASINS SHALL BE CLEANED FOLLOWING COMPLETION OF CONSTRUCTION AND ANUALLY THEREAFTER PER O&M.

10. THE ENTIRE WORK AREA SHALL BE CLEARED OF BUILDINGS TO BE RAZED, PAVEMENT, DEBRIS, BOULDERS, BRUSH, TREES, STUMPS, UNSUITABLE MATERIAL AND LIKE MATERIALS. 11. THE CONTRACTOR SHALL MAINTAIN THE SITE IN A SAFE CONDITION THROUGHOUT THE CONTRACT PERIOD. THE CONTRACTOR SHALL FULLY COMPLY WITH ALL STATE, FEDERAL, AND LOCAL REGULATIONS PERTAINING TO SAFETY.

12. SHRUBS - PROVIDE PER LANDSCAPE PLAN SPECIFICAITONS. 13. THE PROPOSED SIGNS SHALL BE DESIGNED AND INSTALLED IN CONFORMANCE WITH THE U.S. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES 2009 EDITION FOR STREETS AND HIGHWAYS OR AS MOST RECENTLY AMENDED. EXISTING SIGNS TO BE RELOCATED WHERE NECESSARY. 14. THE ELECTRICAL POWER DISTRIBUTION SHALL BE INSTALLED IN ACCORDANCE WITH THE SPECIFICATIONS OF THE LEXINGTON MUNICIPAL LIGHT PLANT IN EFFECT AT THE TIME. ELECTRICAL REQUIREMENTS AND LOCATION TO BE DETERMINED BY OTHER AND CONFIRMED WITH OWNER.

15. NO EARTH SHALL BE REMOVED FROM THE SITE. 16. PLAN IS SUBJECT TO REVIEW AND COMMENT BY THE CITY OF CAMBRIDGE WATER DEPARTMENT, DUE TO LOCATION OF CAMBRIDGE RESERVOIR IN PROXIMITY TO THE SITE. 17. THE EXISTING PRIVATE ON-SITE SEWAGE DISPOSAL SYSTEM SHALL BE ABANDONED IN ACCORDANCE WITH 310 CMR 15.354:

ABANDONMENT OF SYSTEMS. 18. THE PROPOSED SEWER PUMPING SYSTEM SHALL BE PRIVATELY OWNED AND MAINTAINED BY THE APPLICANT'S DESIGNEE. A SIGN SHALL BE PLACED ON EACH PUMPING UNIT INCLUDING EMERGENCY CONTACT INFORMATION IN THE EVENT OF FAILURE.

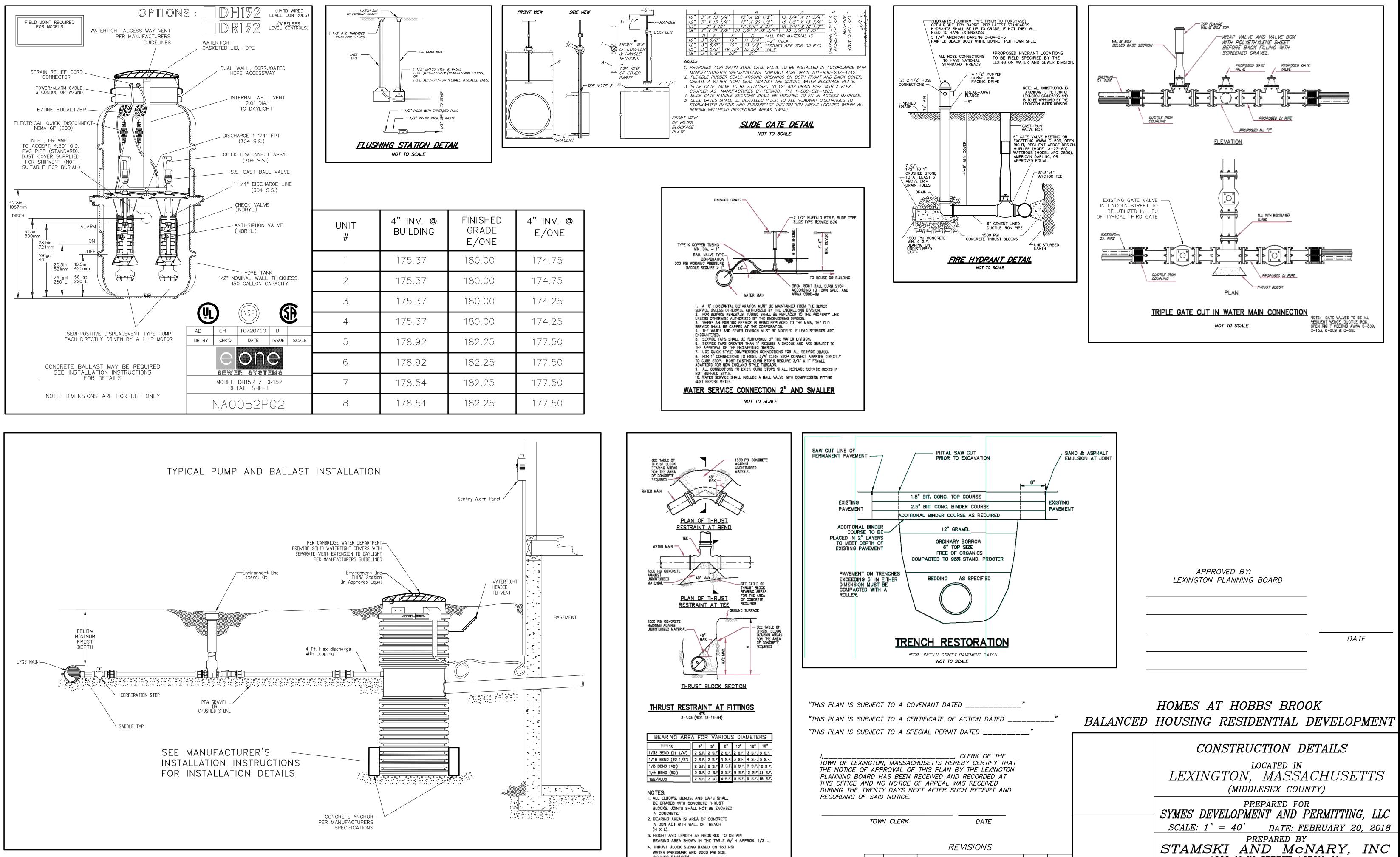
19. THE PROPOSED PRESSURE SEWER PIPE SHALL BE OF TYPE SDR 21 PVC. 20. PROPOSED WATER MAIN PIPE SHALL BE CEMENT LINED DUCTILE IRON THICKNESS CLASS 52. INSTALLATION SHALL CONFORM TO TOWN REQUIREMENTS. 21. ALL MANHOLE FRAMES AND COVERS SHALL CONFORM TO TOWN OF LEXINGTON STANDARDS

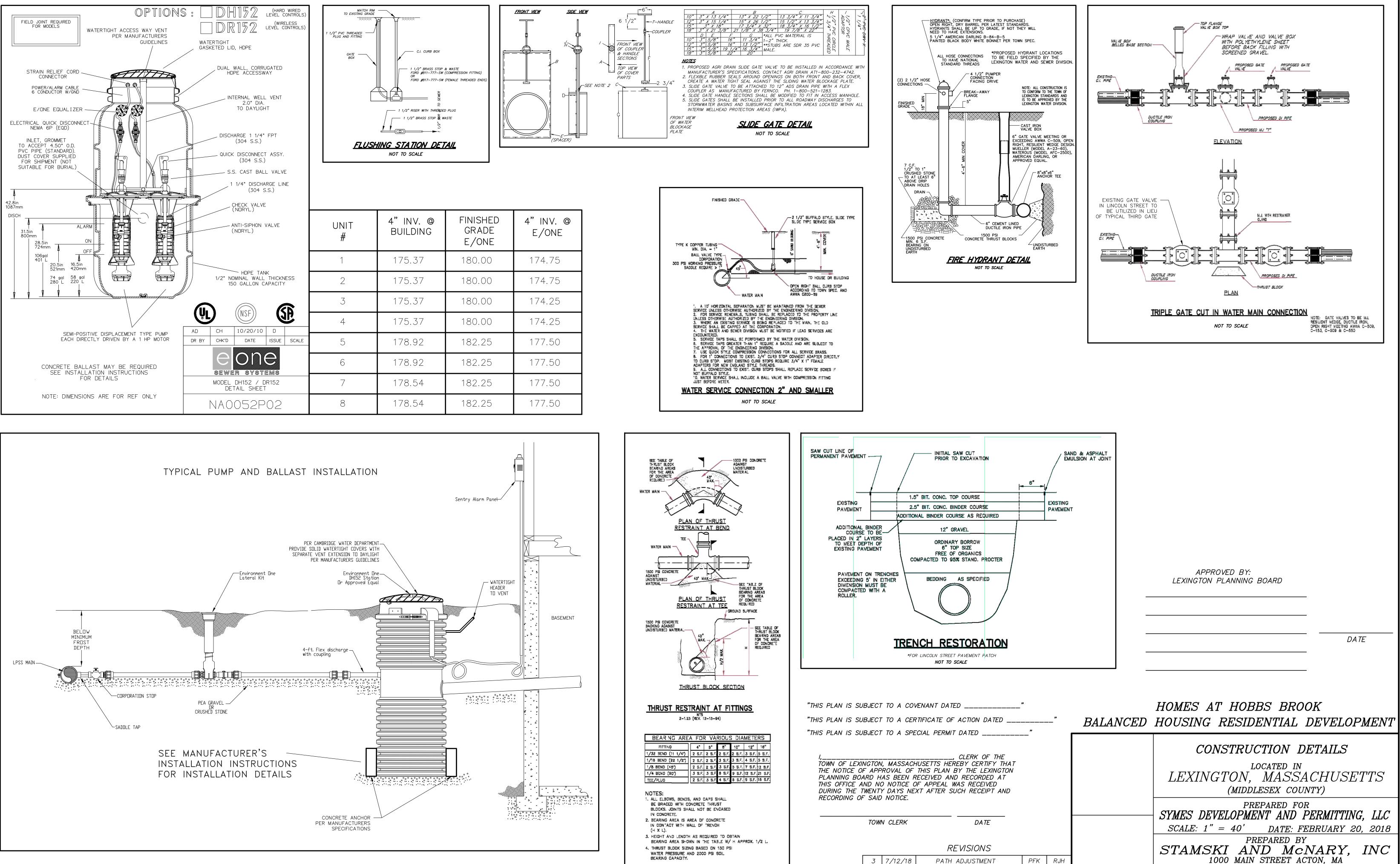
22. PER THE CAMBRIDGE WATER DEPARTMENT, THE PROPOSED SEWER LINES, FLUSHING STATION, GRINDER PUMP STATIONS, AND ACCESS COVERS SHALL BE WATER TIGHT. A VENT PIPE EXTENSION WILL BE USED TO ELEVATE THE PUMP TANK VENT ABOVE THE GROUND SURFACE.

"THIS PLAN IS SUBJECT TO A COVENANT DATED _____

23. PER THE LEXINGTON ENGINEERING DIVISION, MAINTAIN A MINIMUM OF 18" VERTICAL SEPARATION BETWEEN THE CROWN OF PRESSURE SEWER LINES AND THE INVERT OF WATER LINES WHEN LINES MUST CROSS OR A 10' HORIZONTAL SEPARATION CANNOT BE MAINTAINED.

"THIS PLAN IS SUBJECT TO A CERTIFICATE OF ACTION DATED _____ "THIS PLAN IS SUBJECT TO A SPECIAL PERMIT DATED ______ CLERK OF THE TOWN OF LEXINGTON, MASSACHUSETTS HEREBY CERTIFY THAT THE NOTICE OF APPROVAL OF THIS PLAN BY THE LEXINGTON PLANNING BOARD HAS BEEN RECEIVED AND RECORDED AT THIS OFFICE AND NO NOTICE OF APPEAL WAS RECEIVED DURING THE TWENTY DAYS NEXT AFTER SUCH RECEIPT AND RECORDING OF SAID NOTICE. TOWN CLERK DATE APPROVED BY: ÓRAIN BASIN LEXINGTON PLANNING BOARD DATE HOMES AT HOBBS BROOK BALANCED HOUSING RESIDENTIAL DEVELOPMENT CONSTRUCTION DETAILS LOCATED IN LEXINGTON, MASSACHUSETTS (MIDDLESEX COUNTY) PREPARED FOR SYMES DEVELOPMENT AND PERMITTING, LLC SCALE: 1" = 40' DATE: FEBRUARY 20, 2018 PREPARED BY STAMSKI AND MCNARY, INC 1000 MAIN STREET ACTON, MA PFK RJH ENGINEERING - PLANNING - SURVEYING PFK RJH PFK RJH PROJECT No. SM-5676 SHEET No. 9 OF 11 BY CHK'D





2 5/30/18

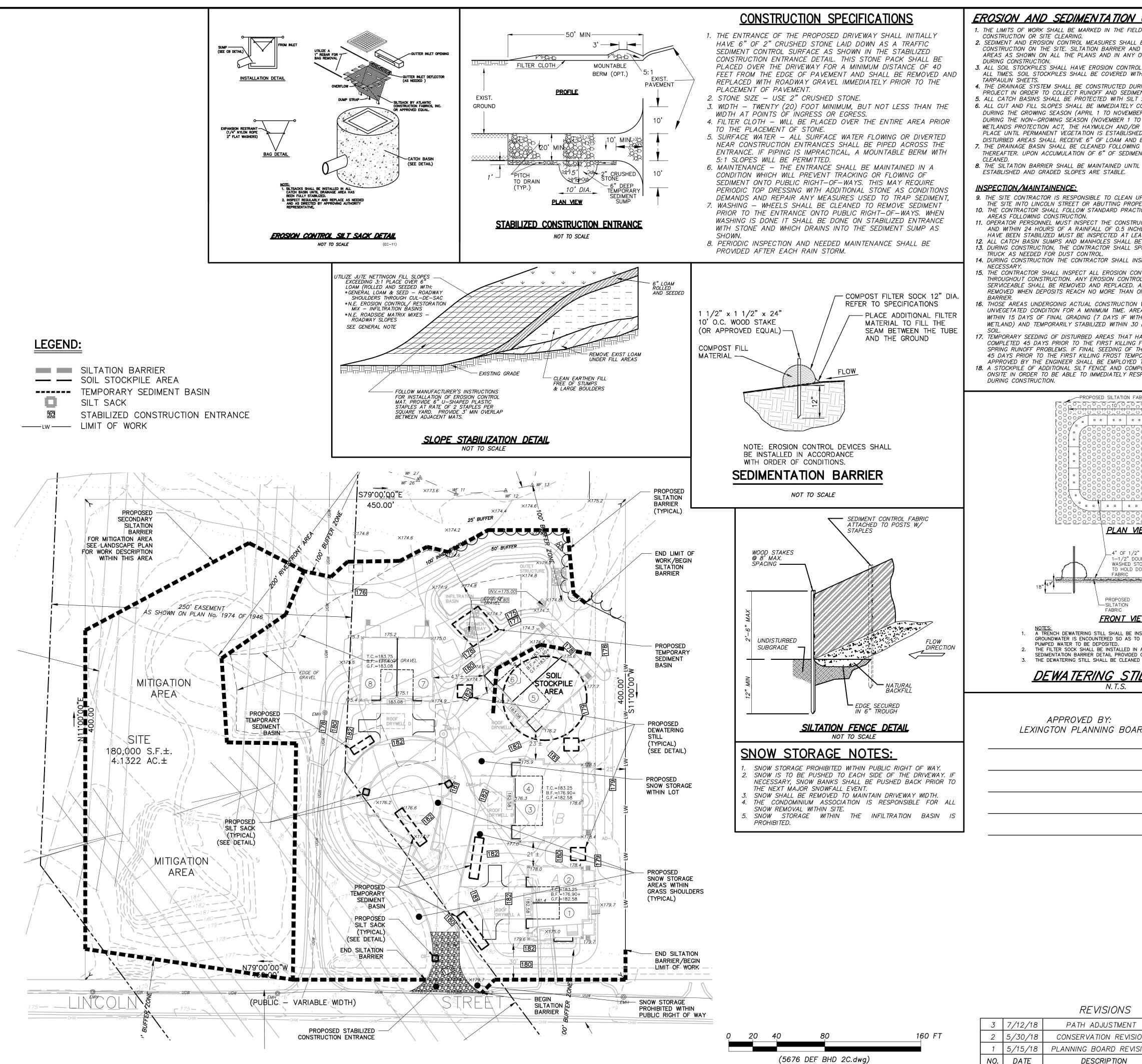
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PLANNING BOARD

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REVISIONS				PREPARED BY STAMSKI AND MCNARY, INC
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NING BOARD REVISIONS	PFK	RJH		SHEET No. 10 OF 11 PROJECT No. SM-5676
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<u>I CONTROL NOTES</u>	LONG TERM POLLUTION PREVENTION AND
ELD PRIOR TO THE START OF	DRAINAGE SYSTEM OPERATION AND MAINTENANCE PLAN
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DURING THE EARLIEST STAGES OF THE	RESPONSIBILITY OF THE SITE CONTRACTOR DURING CONSTRUCTION.
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OR REQUIRED MEASURES SHALL REMAIN IN HED. UNLESS OTHERWISE INDICATED, ALL ID BE SEEDED TO PREVENT EROSION	PARTIES RESPONSIBLE FOR LONG TERM OPERATION/MAINTENANCE: CONDOMINIUM ASSOCIATION
ID BE SEEDED TO PREVENT EROSION. NG CONSTRUCTION AND ANNUALLY MENT, THE DRAINAGE BASIN SHALL BE	SCHEDULE FOR INSPECTION AND MAINTENANCE:
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	TO IS RECOMMENDED THAT THE PAVEMENT SHALL BE PROPERLY SWEPT TWICE A YEAR, WITH CONCENTRATIONS IN THE SPRING AND THE FALL. DEEP SUMP AND HOODED CATCH BASINS
UP ANY SEDIMENT WHICH ERODES FROM	DURING CONSTRUCTION, CATCH BASIN GRATES SHALL BE WRAPPED WITH FILTER FABRIC. CATCH BASINS SHALL BE CLEANED UPON THE COMPLETION OF CONSTRUCTION. AFTER CONSTRUCTION,
OPERTY IMMEDIATELY UPON DISCOVERY. CTICE AND LOAM AND SEED ALL DISTURBED	THE DEEP SUMPS FOR ALL CATCH BASINS AND DRAIN MANHOLES SHALL BE INSPECTED FOUR TIMES A YEAR AND CLEANED FOUR TIMES A YEAR. SEDIMENT REMOVED SHALL BE DISPOSED OF IN
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LEAST ONCE PER MONTH. BE CLEANED OUT AFTER CONSTRUCTION. SPRAY DOWN THE SITE WITH A WATER	DETERMINED BY PROBING WITH A STICK. IF THE STICK HITS THE BOTTOM WITHIN 30 INCHES OF THE WATER LEVEL, MORE THAN 18 INCHES OF SEDIMENT HAS ACCUMULATED
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CONTROL STRUCTURES AND DEVICES ROL DEVICES FOUND TO NO LONGER TO BE	INFILTRATION BASINS
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WITH 100 FEET OF A STREAM, POND OR 30 DAYS OF INITIAL DISTURBANCE OF THE	ONCE ONLINE, THE BASINS SHALL BE INSPECTED AFTER EVERY MAJOR STORM EVENT, FOR THE FIRST FEW MONTHS. THEREAFTER, THE BASIN SHOULD BE INSPECTED AT LEAST TWICE PER
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THE DISTURBED AREAS IS NOT COMPLETED	ACCUMULATION AND THE HEALTH OF THE TURF.
D TO PROTECT THE SITE. MPOST FILTER SOCKS SHALL BE KEPT PESPOND TO ISSUES WHICH MIGHT DEVELOP	AT LEAST TWICE A YEAR, THE BUFFER AREA, SIDE SLOPES AND BASIN BOTTOM SHOULD BE MOWED. GRASS CLIPPINGS AND ACCUMULATED ORGANIC MATTER SHOULD BE REMOVED TO PREVENT THE FORMATION OF AN IMPERVIOUS ORGANIC MAT. TRASH AND DEBRIS SHOULD ALSO
	BE REMOVED AT THIS TIME.
FABRIC	SEDIMENT SHOULD BE REMOVED FROM THE BASIN AS NECESSARY. REMOVAL PROCEDURES SHOULD NOT TAKE PLACE UNTIL THE FLOOR OF THE BASIN IS THOROUGHLY DRY. PRETREATMENT DEVISES ASSOCIATED WITH BASINS SHOULD BE INSPECTED AND CLEANED AT
	PRETREATMENT DEVISES ASSOCIATED WITH BASINS SHOULD BE INSPECTED AND CLEANED AT LEAST TWICE A YEAR AND IDEALLY EVERY OTHER MONTH.
STAKED COMPOST FILTER SOCKS	DRYWELLS: INSPECT THE DRYWELL AFTER EVERY MAJOR STORM FOR THE FIRST FEW MONTHS TO ENSURE PROPER
	STABILIZATION AND FUNCTION. THEREAFTER, INSPECT AND CLEAN IT AT LEAST ONCE PER YEAR. WATER LEVELS SHOULD BE RECORDED OVER SEVERAL DAYS TO CHECK THE DRYWELL DRAINAGE.
	<u>DEICING AND SNOW STORAGE</u> THE USE OF SODIUM–BASED DEICING AGENTS IS PROHIBITED AND USE OF CHLORIDE–CONTAINING
	DEICERS SHALL BE LIMITED. ACCEPTABLE DEICING CHEMICALS INCLUDE A MIX OF 80% SAND AND NOT MORE THAN 20% SODIUM-FREE DEICING AGENT (SUCH AS $C_{a}CI_{2}$). USE OF THE 80% SAND MIX MAY
	RESULT IN A NEED FOR MORE FREQUENT CLEANING OF CATCH BASINS. OTHER LOW SODIUM OPTIONS COULD BE USED IF FIRST APPROVED BY THE CAMBRIDGE WATER DEPARTMENT.
BOODE WASHED STONE TO HOLD DOWN FABRIC	UNDER NO CIRCUMSTANCES SHALL SNOW BE STORED WITHIN THE INFILTRATION BASIN. SNOW SHALL BE STORED WITHIN THE AREA MARKED ON THIS PLAN.
<u>vew</u>	LANDSCAPING AND LAWN MAINTENANCE
(o" TO 1	USE OF HERBICIDES AND PESTICIDES IS PROHIBITED UNLESS PERMITTED BY THE CAMBRIDGE WATER DEPARTMENT. FERTILIZER USE SHOULD CONFORM TO THE REQUIREMENTS OF 330 CMR 31.00.
	EMERGENCY CONTACTS: IN THE EVENT OF A HAZARDOUS MATERIALS SPILL ON THE SITE THE FOLLOWING PARTIES SHALL
	BE CONTACTED: FIRE DEPARTMENT: PH: 781-862-0272
Ų	<u>RECORDS:</u> THE OWNER SHALL MAINTAIN AN INSPECTION LOG OF ALL ELEMENTS OF THE STORM WATER MANAGEMENT PLAN. THE OWNER SHALL MAINTAIN A MAINTENANCE LOG DOCUMENTING THE
	INSPECTION AND MAINTENANCE OF THE DRAINAGE STRUCTURES UNDER HIS CONTROL. A COPY OF THE EROSION CONTROL AND STORM WATER MAINTENANCE PLAN AND INSPECTION LOGS
	SHALL BE KEPT ONSITE AT ALL TIMES.
INSTALLED WHEREVER TO PROVIDE AN AREA FOR	
IN ACCORDANCE WITH THE ED ON THIS PLAN. NED OF SILT AS NECESSARY.	
TILL DETAIL	
	"THIS PLAN IS SUBJECT TO A COVENANT DATED"
	"THIS PLAN IS SUBJECT TO A CERTIFICATE OF ACTION DATED"
	"THIS PLAN IS SUBJECT TO A SPECIAL PERMIT DATED"
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	I,, CLERK OF THE TOWN OF LEXINGTON, MASSACHUSETTS HEREBY CERTIFY THAT
	THE NOTICE OF APPROVAL OF THIS PLAN BY THE LEXINGTON PLANNING BOARD HAS BEEN RECEIVED AND RECORDED AT
	THIS OFFICE AND NO NOTICE OF APPEAL WAS RECEIVED DURING THE TWENTY DAYS NEXT AFTER SUCH RECEIPT AND
DATE	RECORDING OF SAID NOTICE.
	TOWN CLERK DATE
	HOMES AT HOBBS BROOK
BAL	ANCED HOUSING RESIDENTIAL DEVELOPMENT
	EROSION AND SEDIMENTATION
	CONTROL PLAN
	LOCATED IN
	LEXINGTON, MASSACHUSETTS
	(MIDDLESEX COUNTY)
	PREPARED FOR
	SYMES DEVELOPMENT & PERMITTING, LLC
	SCALE: $1'' = 40'$ DATE: FEBRUARY 20, 2018
	PREPARED BY
	STAMSKI AND MCNARY, INC
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ISIONS PFK RJH	SHEET No. 11 OF 11 PROJECT No. SM-5676
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LEXINGTON PLANNING BOARD

AGENDA ITEM TITLE:

8 Adams Street: Definitive Site Sensitive Development (Public Hearing)

PRESENTER:

<u>ITEM</u> <u>NUMBER:</u>

Gary Larson

SUMMARY:

Planning Board will open a public hearing to discuss the application of Randall and Elaine Hiller for approval of a special permit for a Site Sensitive Development under Section 135-6.9.3, of the Code of Lexington. The property, 8 Adams Street (Map 63, Lot 77A), is located in the RS Residential Zoning District. The project proposes maintaining the existing single family dwelling unit and constructing a second unit on the lot.

Type

SUGGESTED MOTION:

FOLLOW-UP:

DATE AND APPROXIMATE TIME ON AGENDA:

7/19/2018

ATTACHMENTS:

D	•	
Desc	rin	tion
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D	8 Adams Plan Set	Backup Material
D	Staff Report	Backup Material
D	Board of Health Comments	Backup Material
D	Abutter letter from 1 Adams	Backup Material
D	Abutter letter from 10 Adams	Backup Material
D	Attorney Memo	Backup Material
D	Stormwater Analysis and Calculations	Backup Material

Architectural Rendering

Backup Material



1. THE INFORMATION DEPICTED ON THIS PLAN HAS BEEN COMPILED FROM THE TOWN OF LEXINGTON GEOGRAPHIC INFORMATION SYSTEM.

2. LAND USE WITHIN 500 FEET OF THE SUBJECT PROPERTY IS PRIMARILY SINGLE FAMILY

8 ADAMS STREET (ASSESSOR'S MAP 63 - LOT 77A) DEFINITIVE SITE SENSITIVE SUBDIVISION PLAN SET

PLANNING BOARD DEVELOPMENT REGULATIONS

REVISED: JULY 12, 2018

RECORD OWNERS/ APPLICANTS:

8 ADAMS STREET

DEEDS.



LANDSCAPE ARCHITECT

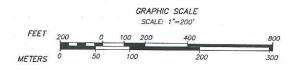
GARY LARSON RLA 6 WADMAN CRICLE LEXIGNTON MA 02420

PATRICIA NELSON

SHEET 1	COVER S
SHEET 2	RECORD
SHEET 3	SITE AN
SHEET 4	PROPERT
SHEET 5	SITE CO.
SHEET 6	SITE UT
SHEET 7	SITE LAI
SHEET 8	SITE DE
SHEET 9	SITE DE.
SHEET 10	PROOF P



LOCUS CONTEXT MAP:



IN ACCORDANCE WITH SECTION 175-6.0 OF THE LEXINGTON

LOCATED IN LEXINGTON, MASSACHUSETTS DATE: MAY 24, 2018.

> RANDALL S. & ELAINE H. HILLER LEXINGTON, MASSACHUSETTS 02420 -DEED BOOK 26502, PAGE 3 *

*DENOTES DOCUMENTS RECORDED AT THE MIDDLESEX SOUTH REGISTRY OF

PREPARED BY:

MERIDIAN ASSOCIATES ENTER SUITE 5950 69 MILK STREET, SUITE 30 ACHUSETTS 01915 WESTBOROUGH, MASSACHUSET

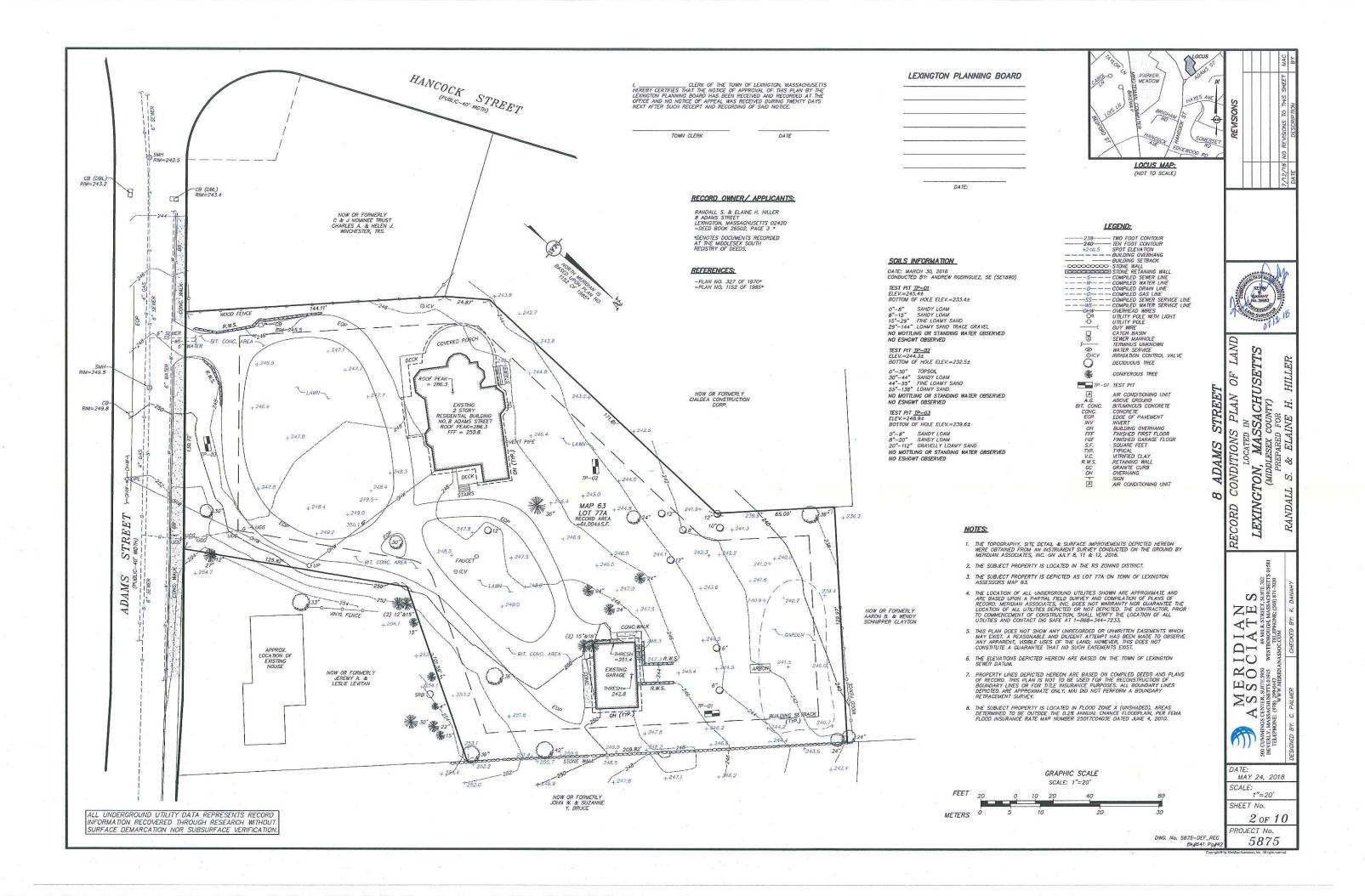
ATTORNEY

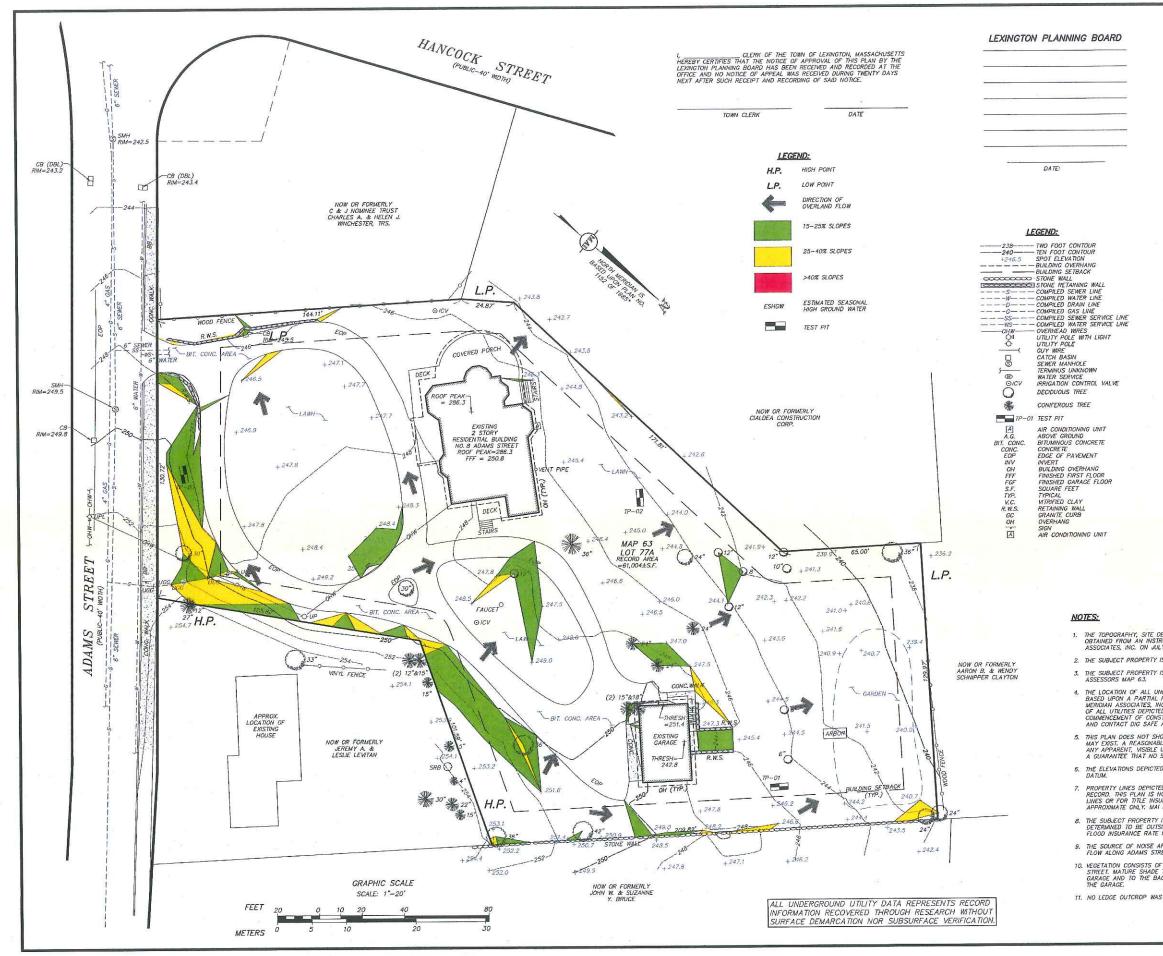
7 HARTWELL AVENUE LEXINGTON, MA 02421

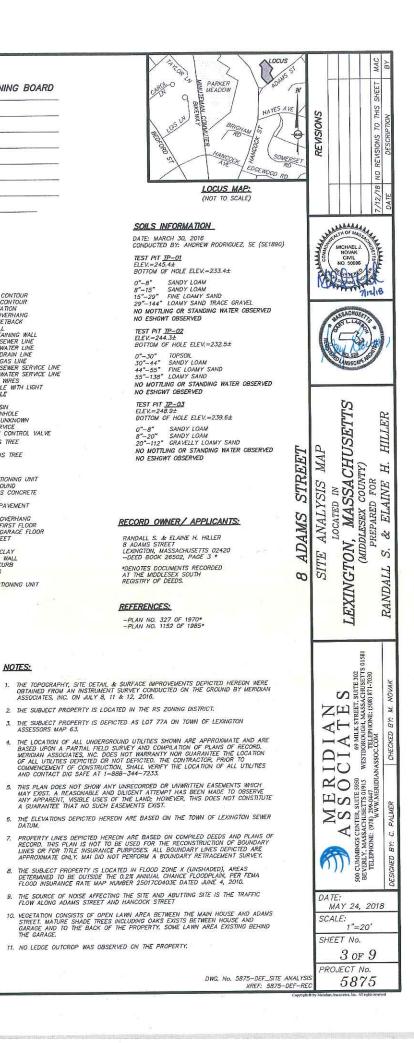
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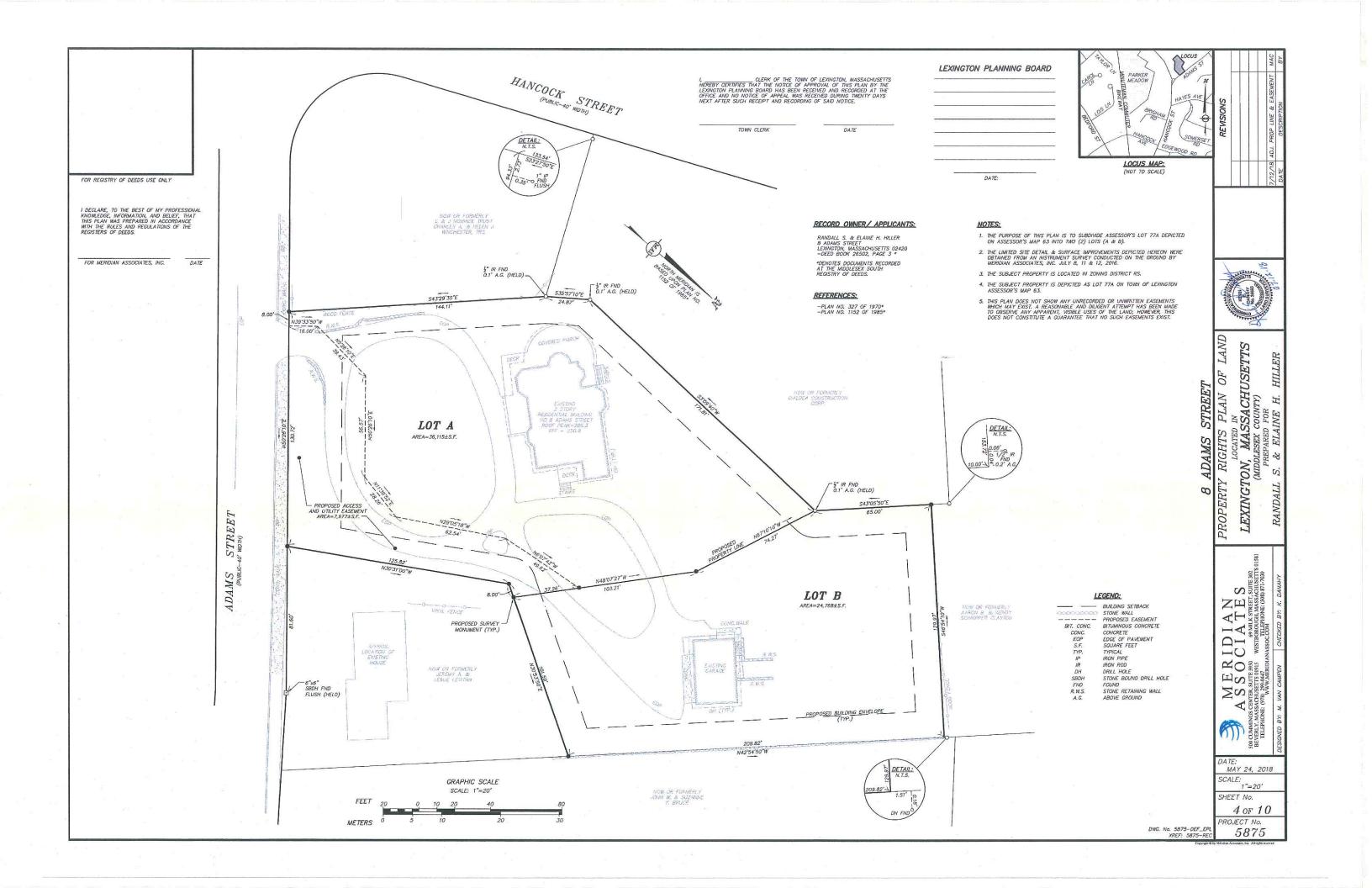
SHEET & LOCUS CONTEXT MAP CONDITIONS ALYSIS MAP TY RIGHTS PLAN OF LAND NSTRUCTION/LANDSCAPE PLAN TILITY PLAN NDSCAPE PLAN TAILS TAILS PLAN

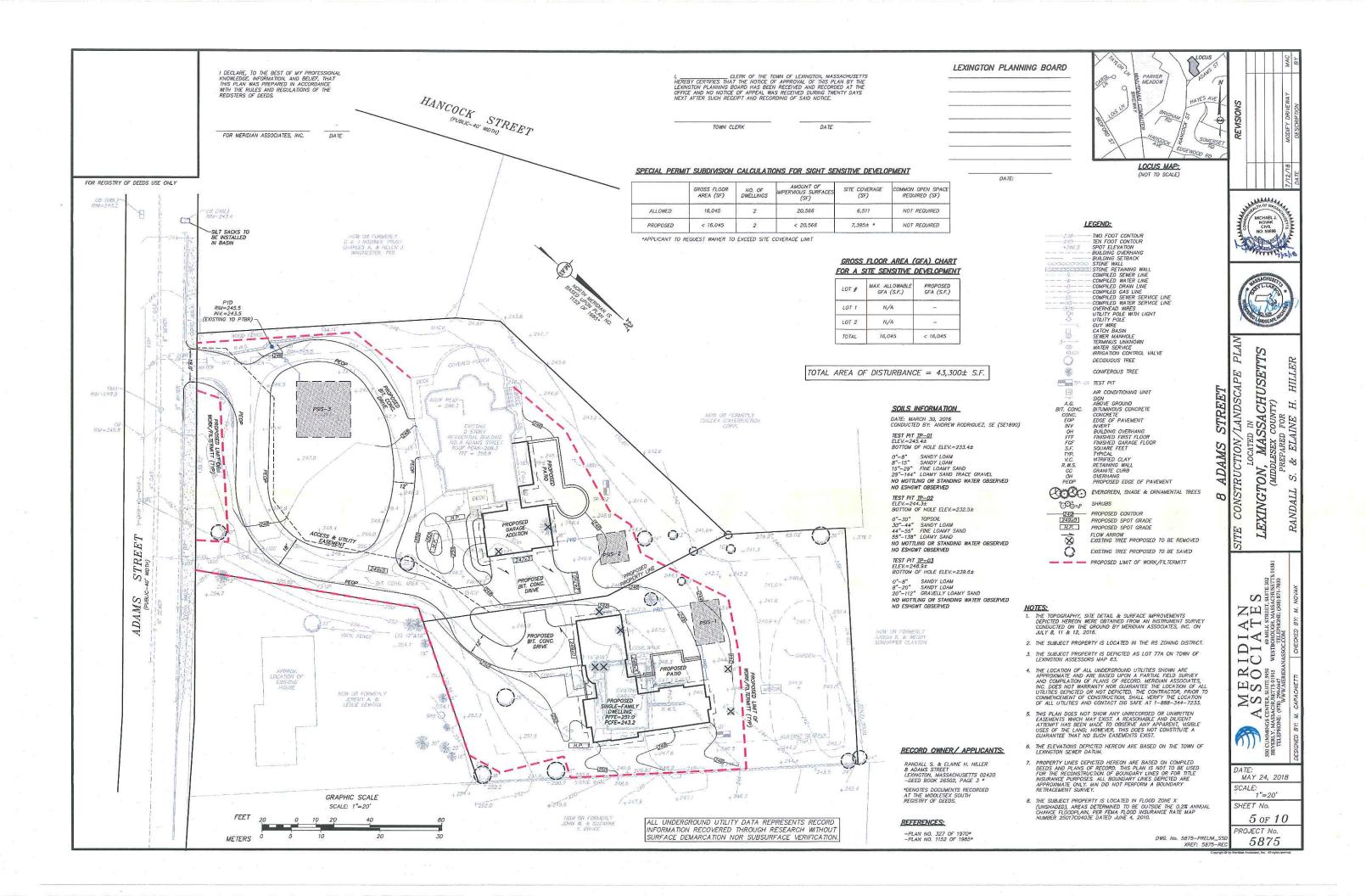


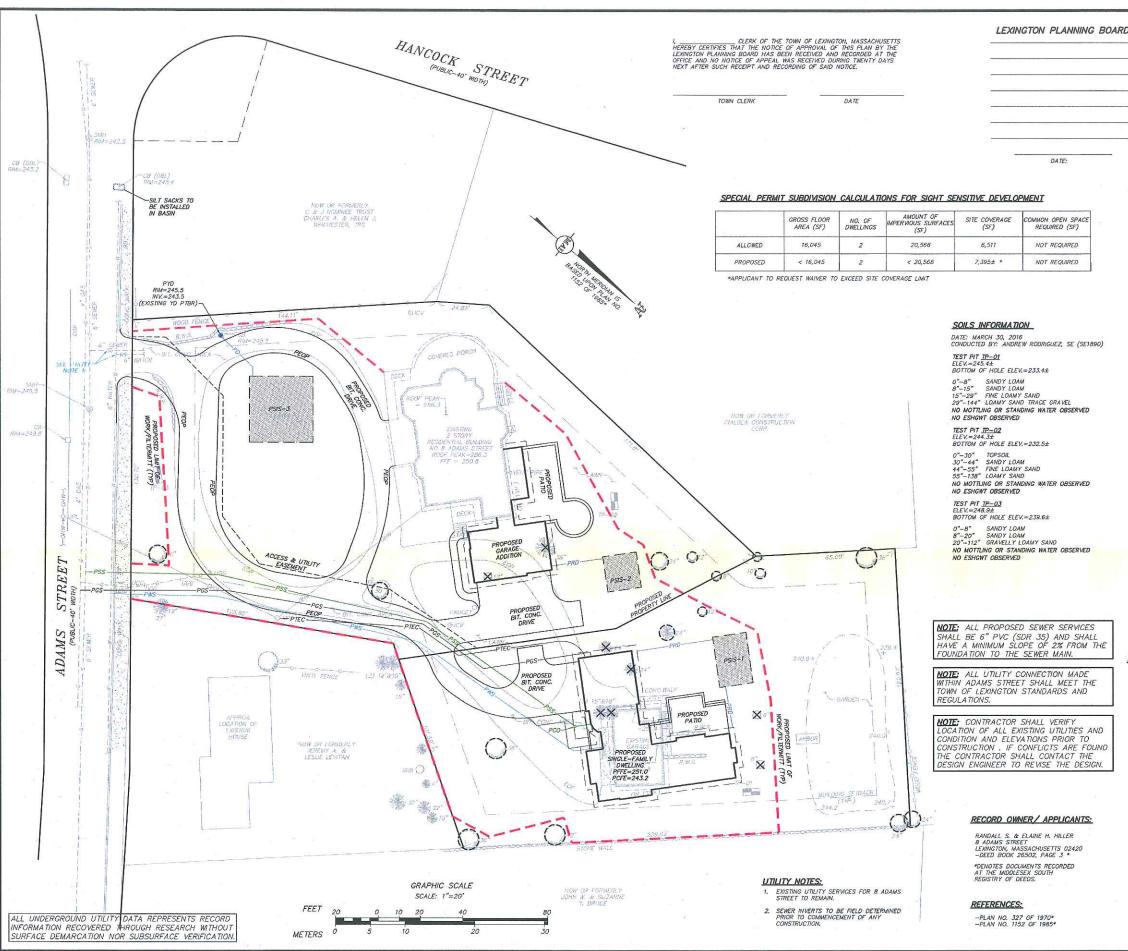




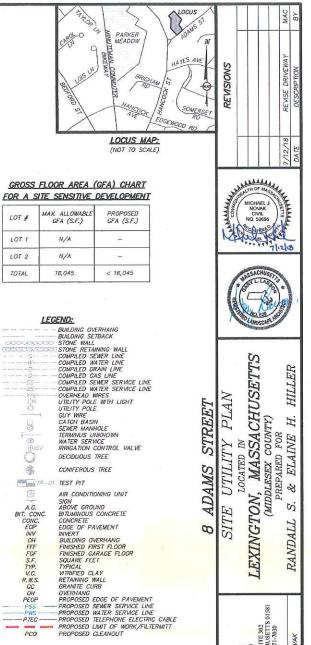








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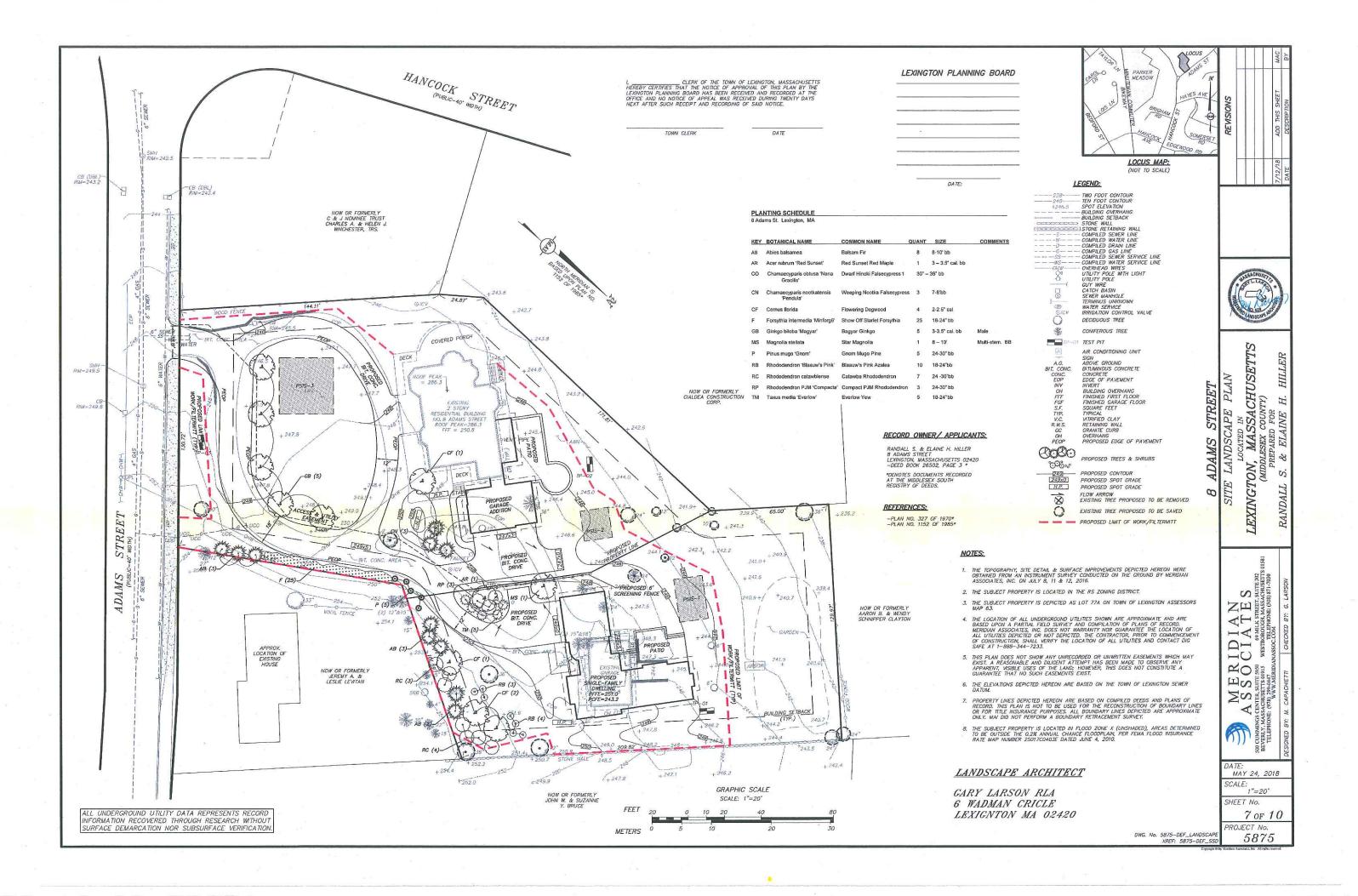
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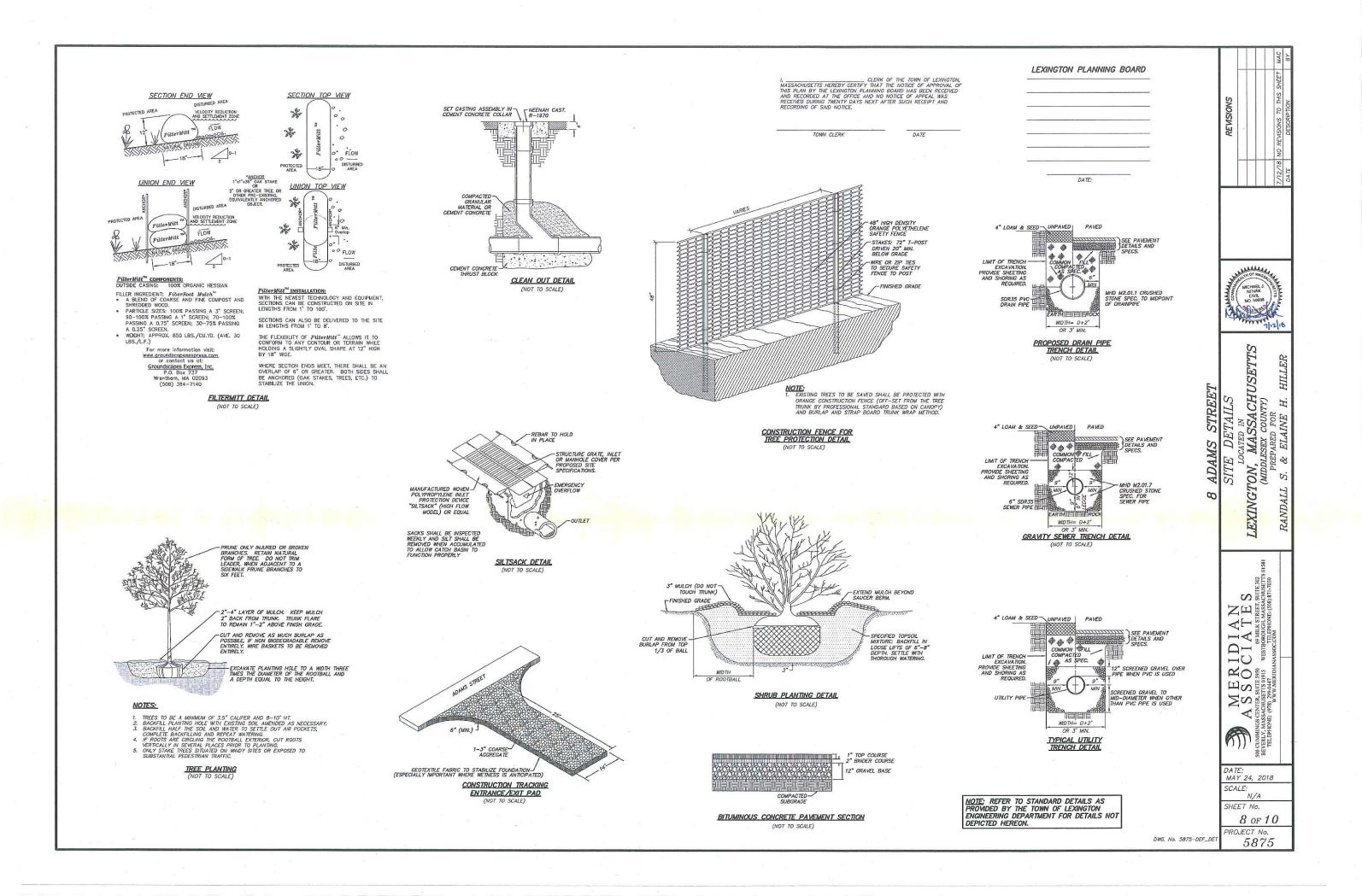
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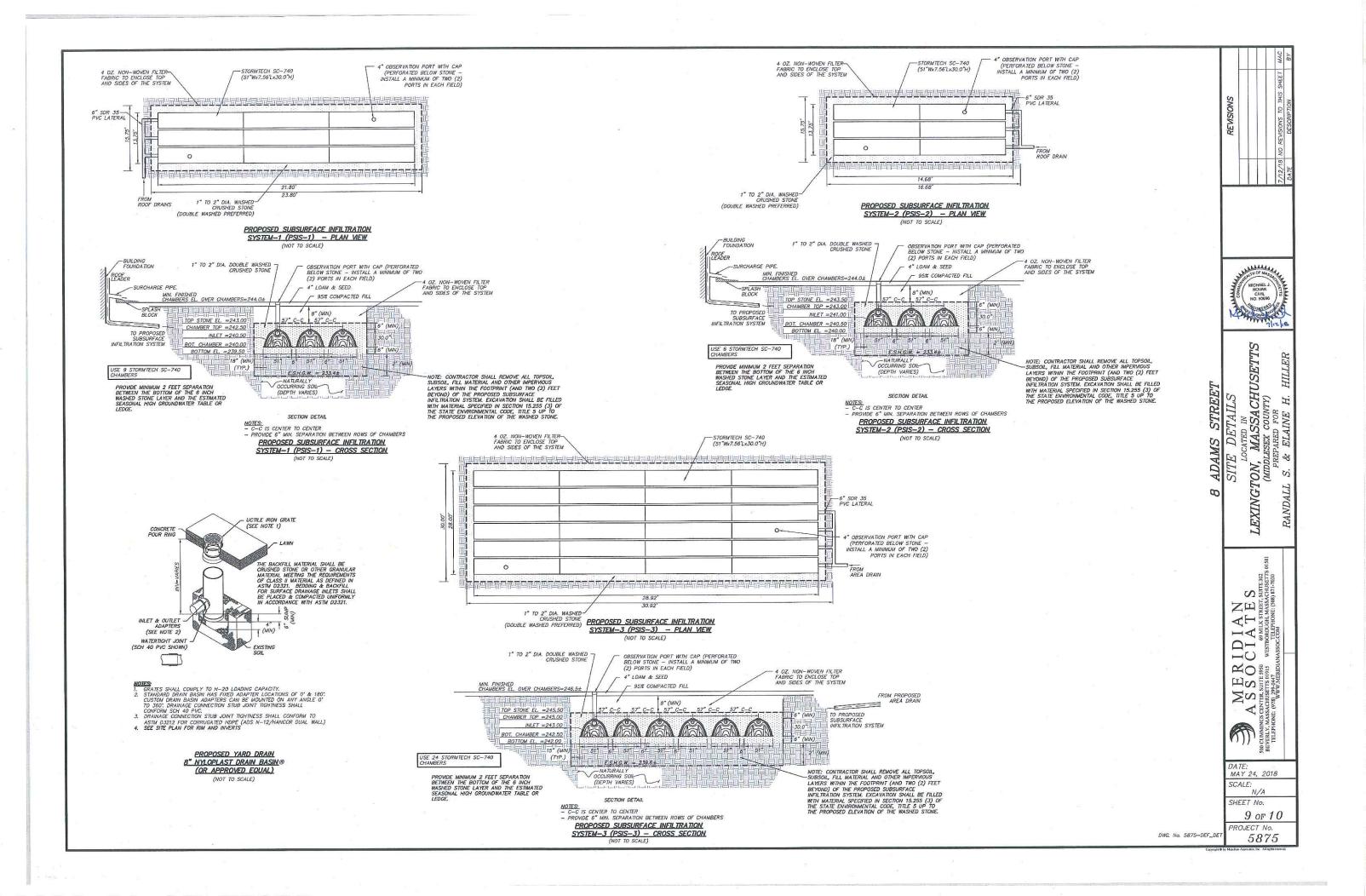
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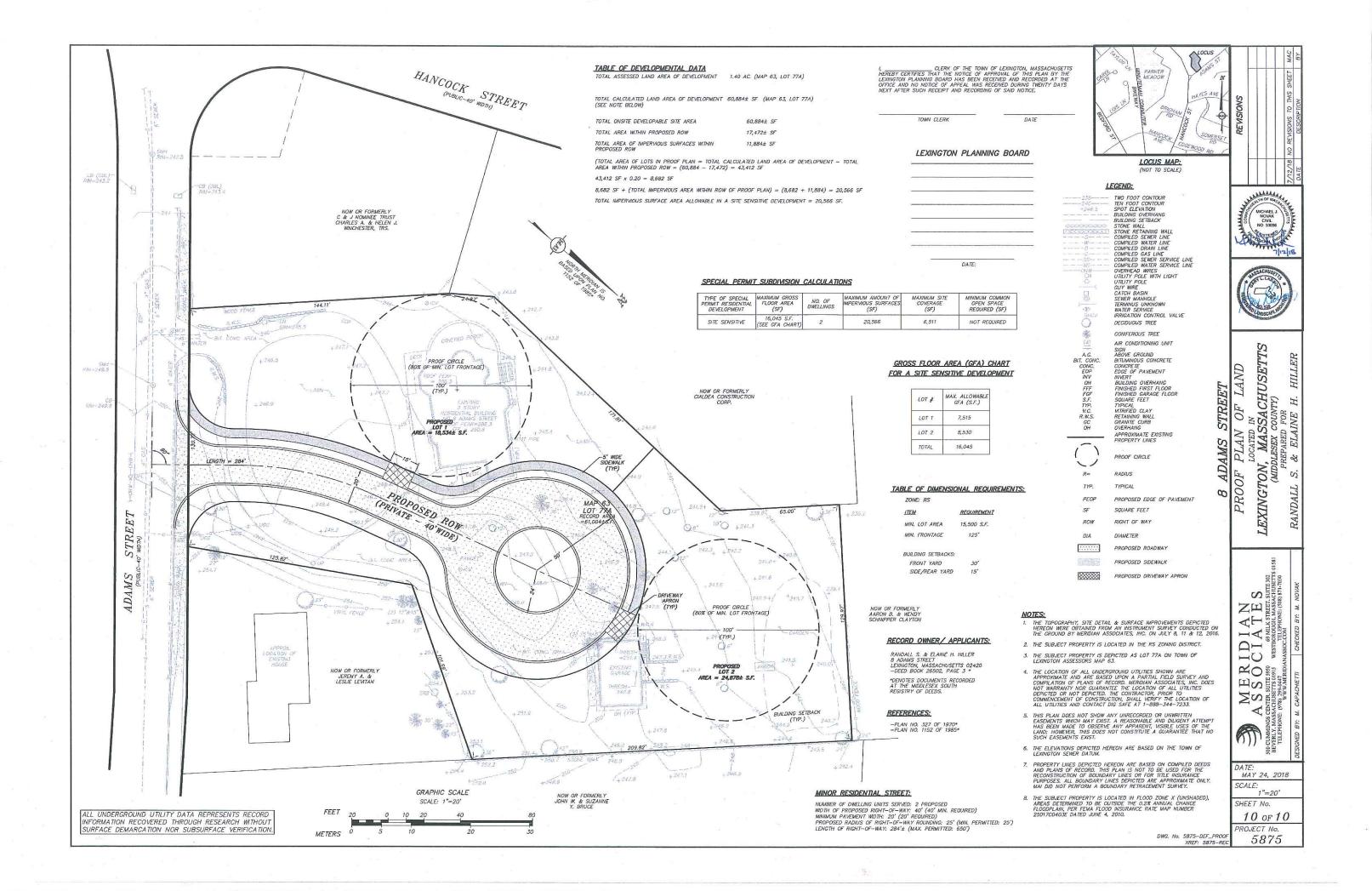
- THE TOPOGRAPHY, SITE DETAIL & SURFACE IMPROVEMENTS DEPICIED HEREON WERE OBTAINED FROM AN INSTRUMENT SURVEY CONDUCTED ON THE GROUND BY MERIDIAN ASSOCIATES, INC. ON JULY 8, 11 & 12, 2016.
- 2. THE SUBJECT PROPERTY IS LOCATED IN THE RS ZONING DISTRICT. 3. THE SUBJECT PROPERTY IS DEPICTED AS LOT 77A ON TOWN OF LEXINGTON ASSESSORS MAP 63.
- 4. THE LOCATION OF ALL UNDERGROUND UTILITIES SHOWN ARE APPROXIMATE AND ARE BASED UPON A PARTIAL FIELD SUPPEY AND COMPLATION OF PLANS OF RECORD. MERDIAN ASSOCIATES, INC. DOES NOT WARRANTY NOR GUARANTEE THE LOCATION OF ALL UTILITIES DEPICTED OR NOT DEPICTED. THE CONTRACTOR, PRIOR TO COMMENCEMENT OF CONSTRUCTION, SHALL VERITY THE LOCATION OF ALL UTILITIES AND CONTACT DIG SAFE AT 1-888-344-7233.
- 5. THIS PLAN DOES NOT SHOW ANY UNRECORDED OR UNIWRITTEN EASEMENTS WHICH MAY EXIST. A REASONABLE AND DUIGENT ATTEMPT HAS BEEN MORE TO OBSERVE ANY APARENT, VISIBLE USES OF THE LAND: HOWEVER, THIS DOES NOT CONSTITUTE A GUARANTEE THAT NO SUCH EASEMENTS EXIST.
- 6. THE ELEVATIONS DEPICTED HEREON ARE BASED ON THE TOWN OF LEXINGTON SEWER DATUM.
- PROPERTY LINES DEPICTED HEREON ARE BASED ON COMPILED DEEDS AND PLANS OF RECORD. THIS PLAN IS NOT TO BE USED FOR THE RECONSTRUCTION OF BOLINDARY LINES OR FOR TITLE NISURANCE PURPOSES. ALL BOUNDARY LINES DEPICTED ARE APPROXIMATE ONLY. MAI DO NOT PERFORM A BOUNDARY RETRACEMENT SURVEY.
- 8. THE SUBJECT PROPERTY IS LOCATED IN FLOOD ZONE X (UNSHADED), AREAS DETERMINED TO BE OUTSIDE THE 0.2% ANNUAL CHAINCE FLOODPLAIN, PER FEMA FLOOD INSURANCE RATE MAP NUMBER ZSOT7CO403E DATED JUNE 4, 2010.

DWG. No. 5875-DEF_SSD XREF: 5875-REC











Lexington Planning Office Memorandum

То:	Planning Board
From:	David Fields, Planner
Date:	July 16, 2018
Subject:	Site Sensitive Development Plan for 8 Adams Street

GENERAL INFORMATION

Owner / Applicant:	Randall & Elaine Hiller
Designers:	Gary Larson, RLA; and Meridian Associates, Inc.;
Submission Materials:	Special permit application for a Site Sensitive Development.
Location:	8 Adams Street, Assessor's Map 63, Parcel 77A
Assessed Area:	$1.4 \pm acres$
Zoning:	RS, One Family (15,500 S.F. lot, 125 ft. frontage)
Current Land Use:	Single Family Residence
Surrounding Land Use:	The property at 8 Adams Street is surrounded by single family homes and is located off of Hancock Street, roughly ½ mile from Lexington Center.
Topography/Land Cover:	The site is flat with a small portion of 25-40% slope on the southeast portion of the lot fronting Adams Street.
	Soils on the site consist Charlton-Urban Land-Hollis Complex fine sandy loam and Merrimac-Urban Land Complex fine sandy loamy over very gravely sand.
Wetlands/Flood Zone:	There are no known wetlands on site. The property is not located in any FEMA Flood Zone determined to be in the 1% and 0.2% annual chance floodplains.
Historic Status:	The existing structure is not located in a Historic District, however, the structure is a historically significant building.
Other Board, Commission & Department Status:	This plan has been reviewed by the Development Review Team.

DEVELOPMENT DATA

Compliance with Zoning:

The lot has roughly 130 feet of frontage on Adams Street, a total area of $1.4 \pm$ acres which meets the requirements for residential developments in Section 135-4.0 of the Lexington Zoning Bylaw.

Development Data	Conventional	Proposed SSD
Dwelling Units (DU)	2	2
Density	1.42 DU/AC	1.42 DU/AC
Maximum Site Coverage (SF)	N/A	7,875
Total GFA	16,045 for total site	<16, 045 for total site
Impervious Surface (SF)	Allowed 20,566 for total site	<17,500 for total site

SUMMARY OF THE PLAN

The plan for 8 Adams Street has been submitted under §135-6.9 *Special Permit Residential Developments* of Lexington's Zoning Bylaw, specifically the provision defined in §135-6.9.3. The proof plan shows a single minor residential street terminating in a cul-de-sac, retaining no existing features of the site. As shown, all lots on the proof plan comply with conventional dimensional requirements.

The proposed Site Sensitive Development shows the retention of the existing home, however, the detached out building will be demolished. The proposal shows an addition on the rear of the home to be retained. The applicant should discuss the proposal with the Lexington Historical Commission regarding alterations to the structures and may have done so already; clarification should be sought by the Board as to the status of these conversations, if they have taken place. Furthermore, as the existing home is built in to the sideyard setback, the height of any addition may be subject to the height limit adopted during the 2016 Town Meeting season, or the height of the existing nonconforming structure; whichever is greater.

The applicant should be prepared to discuss any conversations conducted with the Lexington Fire Department as to the status of fire suppression required for the proposed new dwelling unit.

The proposed additional structure to the rear of the existing home at 8 Adams Street is designed to be a 1.5 story structure to accommodate buyers in all potential age ranges. While this is commendable, this design also creates a more sprawling building. As such the applicant will require a waiver for site coverage if this project moves forward as is. While the additional height that would come with shrinking the building footprint is not a particularly great compromise, site coverage could be reduced by:

- 1. Not adding on to the existing home
- 2. Not designing three car garages for the existing home (5 bays in total on site for two homes)

It will be for the Board to decide whether to grant a waiver for site coverage if the plan moves forward.

With regard to the proposed common driveway serving both homes, the width should be a uniform 18 feet. This was confirmed through discussion with the Lexington Fire Department. The 18 foot minimum can be used on the portions of the common drive serving both homes. The individual drives that are not to be common use can remain as less than 18 feet in width as they serve only one unit.



Town of Lexington

Land Use, Health and Development Department Office of Public Health 1625 Massachusetts Avenue Lexington, MA 02420 (781)-698-4533 Fax (781)-861-2780

Gerard F. Cody, R.E.H.S./R.S. Health Director x 84503

Board of Health

Kathy P. Fox, R.E.H.S. /R.S., C.H.O., CP-FS Environmental Health Agent x 84507

David Neylon, B, S.N., R.N. Public Health Nurse x 84509 Wendy Heiger-Bernays, PhD, Chair Sharon Mackenzie, R.N., CCM Burt M. Perlmutter, M.D. David S. Geller, M.D. John J. Flynn, J.D.

June 15, 2018

To: David Fields, Planner, Planning Office | Land Use, Health and Development

From: Gerard F. Cody, R.E.H.S./R.S.

Re: Comments on 8 Adams Street

The Office of Public Health received a definitive Subdivision Plan for "8 Adams Street." The applicant asked for comments from the Office of Public Health about this project. New Construction can sometimes create unintentional nuisance conditions by creating harborage conditions for both mosquitoes, rodents and other pests. The Office of Public Health would like to share with the developer some "best practices" to help avoid mosquito and pest harborage nuisance conditions during new construction and to help avoid them in the future once the project is completed.

Mosquito Population Reduction through storm water runoff design

During periods of several rain events and the when the ground water is high within a 10 day period, mosquito populations will increase. Below, you will find some general best practices to help reduce the mosquito population at this location:

- Ensure that stormwater structures such as dry wells, rain gardens and detention basins are designed to infiltrate water within 48 hours of a rain event to help reduce mosquito populations. Dry wells and detention ponds should be located, if possible, at elevations that are more than 2 feet above the seasonal ground water mark.
- Any outflow pipes/ drainage ditches that take water from dry wells, detention basins and • catchbasins should be directed to upland areas, if possible, and if not into existing waterways. They should not be directed into a wetland because the inflow of water could cause increased water levels that is sufficient to allow immature mosquitoes in their larval and pupal stages to complete their development.
- Designing detention basins that are sloped and have low flow channels that are designed 0 to prevent water from stagnating is beneficial. The low flow channels need to be maintained periodically to eliminate sand and sediment from obstructing the channels.
- As previously mentioned infiltrating stormwater is preferred to directing runoff into 6 wetlands. If developers could install catchbasins with porous bottoms or even porous

pavement in some locations, those designs would be beneficial from a mosquito control perspective.

Rodent Population Reduction

New Construction, demolition or renovation projects, can displace rodents from their natural habitat. Rodents may seek shelter or harborage in storm drains on residential and commercial properties. The Lexington Office of Public Health would like to provide you with the following information to help ensure that rodents do not take shelter permanently in this area or cause a nuisance condition for the general public.

- Maintain or Rodent Proof the outside structure
- Seal cracks and openings in building foundations, openings for pipes, electric wires, drain spouts, and vents. Do not leave holes any larger than 1/4 inch unsealed.
- If gnawing is suspected to be a problem plug holes and gaps with sheet metal, coarse steel wool or wire screening.
- Most rodents are excellent climbers so do not focus just on the ground level, check the roof as well. Make sure internal screens on roof and in attic air vents are in good repair.
- Keep side doors and garage doors tightly closed.
- Make sure that all windows that can be opened have screens that are in good condition.
- Cover crawl space with a tight fitting cover.
- Cover chimneys with a spark arrester.
- Make sure all exterior doors are tight fitting and weatherproofed at the bottom.
- Remember that pet doors in the house or garage also provide and easy entrance for rodents.
- Sanitation is a very important part of rodent control. Without proper sanitation other steps to eliminate and prevent rodents will not work.
- Keep the areas around your work zone "clutter free" to reduce hiding spaces for rodents.
- Store rubbish and garbage properly in air tight cans with tight fitting lids. All rubbish and garbage should be in cans, do not have bagged or loose rubbish and garbage on the ground.
- Article XI Dumpsters states in part that "It shall be the responsibility of the property owner or agent being serviced to maintain the dumpster free of odors, scattered debris, overflow and all other nuisances. It shall also be the responsibility of the property owner or agent being serviced to maintain the dumpster area free from any condition that may be considered an attraction for rodents or other pests".

cc: Board of Health

1 Adams Street

Lexington, MA 02420

Planning Board

Town Office Building 1625 Massachusetts Avenue Lexington, MA 02420

June 7, 2018

Dear Chairman Johnson,

My family lives at 1 Adams Street, across from the proposed site sensitive development currently under consideration at 8 Adams Street. Our home overlooks the current historical house. Our neighbor, Randy Hiller, have been transparent and forthcoming with information regarding their desire to preserve their current home while building an additional home on their lot.

I have reviewed the plans prepared by Colin Smith and Gary Larsen and submitted by Randy to the Planning Board. We are supportive of the project and particularly the character of the lower profile (though higher site coverage) new house proposed. We fear the destruction of the existing historical home at 8 Adams Street, and hope that an expiditious planning board approval of the Hiller development plans will mitigate this risk.

Sincerely,

Herin Kegan

Alison Ryan

Cc:

Randy Hiller

Phil Posner Patricia Nelson

10 Adams Street Lexington, MA 02420

Planning Board Town Office Building 1625 Massachusetts Avenue Lexington, MA 02420

June 11, 2018

Dear Chairwoman Johnson,

We live at 10 Adams Street, adjacent to the proposed site sensitive development currently under consideration at 8 Adams Street. We still favor a low-profile house design (initially presented to the Planning Board in December 2016 and as indicated in our letter to the Board dated December 27, 2016). Recently, Randy Hiller showed us updated plans and we believe this design will have the least impact on our family's home while maintaining appropriate scale for the lot. We continue to ask that the Board incorporate substantial ground cover and trees as screening as conditions of any permit you may issue.

Sincerely,

Jeremy Levitan

Cc: Randy Hiller Patricia Nelson

Patricia S. Nelson

Attorney At Law 19 Muzzey Street, Suite 207 Lexington, Massachusetts 02421

Telephone: 781-863-8688 Fax: 781-863-2201 E-Mail: <u>psnelson@masslaw.us</u>

July 12, 2018

MEMORANDUM TO:	Ginna Johnson, Chair Lexington Planning Board Town Hall, 1625 Massachusetts Avenue Lexington MA, 02420
RE:	Definitive Site Plan Application, Site Sensitive Plan
PROPERTY:	8 Adams Street, Lexington MA
OWNERS:	Randall Hiller and Elaine Hiller

The following is a Memorandum in support of the Definitive Site Plan Application filed with the Planning Board on May 25, 2018 for a Site Sensitive Development on the Property creating two lots and preserving the existing 1903 home.

BACKGROUND

The current house ("Historic House") was built on the foundation of an earlier Queen Anne house (built 1888) which burned in December of 1902. (Report of Nancy Seasholes to the Historical Commission dated January 1998 ("Seasholes Report"), Form B, copy attached). The existing house at 8 Adams Street was built in 1903, designed by noted local architect Willard D. Brown and is sited on a 61,004 square foot lot, of sufficient size, shape and frontage to support a two lot subdivision if both the house and garage were removed. (See Proof Plan previously submitted.)

The Historical Commission approved the Demolition of the existing garage in October of 2016 on the grounds that the building was not structurally sound.

The Hillers presented a sketch plan to the Planning Board for its hearing on January 5, 2017, which involved demolition of two or more walls of the Historic House, demolition of the garage and construction of a new two plus story home with a footprint of 3142 square feet and a GFA of 5907 square feet.

As noted in the letter of Owner Randall Hiller, attached, the response of the Planning Board was generally positive.

In response to the comments of the Planning Board, the input of the abutter at 10 Adams Street, and the Owners personal concerns for historic preservation, the current plan:

a) Limits exterior alteration of the Historic House to removal of only one (1) wall at the rear of the property;

b) Reduces the height of the new home by one story, with a profile of 1.5 stories;

c) Reduces the footprint of the new building from 3142 sq ft to 2595 sq ft.

d) Reduces the GFA of the new building from 5907 sq ft to 4950 sq ft.

COMPLIANCE WITH REQUIREMENTS OF Chapter 135 §6.9

The proposed project serves the following purposes of Chapter 135 §6.9 as a site sensitive development. A site sensitive development (SSD) is the development of a parcel with configurations of lots allowing flexibility and creativity in residential development through reductions in minimum lot area and frontage requirements in order to minimize site disturbance, preserve historic and sensitive natural resources, and allow for efficient patterns of construction to lower development cost.

1. The Proposed Plans show a "developmentdesigned with sensitivity to the characteristics of the site that otherwise might be limited by application of uniform, largely geometric standards". In this case, a "by right" development is feasible but would entail the destruction of the Historic George O. Whiting/Gilmore House.

2. The proposal preserves historical and architectural features of the existing Historic House and setting.

3. By grouping the Historic House and the new house in the middle of the property (front to back) where the current structures are roughly located, both the set back with circular drive from the street and the significant amount of open space at the rear of the property are preserved.

4. The proposed designs are in keeping with the existing structures and with the livability, scale, character and economic value of the existing neighborhood as follows:

a) The Historic House will remain in its current location set "far back" from Adams Street as noted in the Seasholes Report;

b) The proposed designs retain the semi-circular carriage drive leading up to the front porch and entrance;

c) The changes to the exterior of the Historic House will take place at the rear of the house.

d) The new structure will be located in the approximate location of the current garage, (also set well back from Adams Street) and will be approximately the same height (within two feet) as the current garage.

e) In deference to the request of the abutter most affected by the new construction (owners of 10 Adams Street), the new house will be reduced by one story, keeping a low profile from the viewpoint of the abutters and Adams street.

DOCUMENTS SUBMITTED

The Owners application includes the following submittals:

- Completed Application and Cover Letter
- Drainage Report and Engineering Calculations
- Cover Sheet & Locus Context Plan
- Record Conditions Plan
- Site Analysis Plan
- Property Rights Plan of Land
- Site Construction Plan
- Landscape Plan
- Site Utilities Plan
- Site Details
- Proof Plan
- Completed Application and Cover Letter
- Drainage Report and Engineering Calculations
- Cover Sheet & Locus Context Plan
- Record Conditions Plan
- Site Analysis Plan
- Property Rights Plan of Land
- Site Construction Plan
- Landscape Plan
- Site Utilities Plan
- Site Details
- Proof Plan

- Form W and Addendum
- Owner Letter

WAIVERS

The Owners request a waiver from the site coverage requirements as noted on Form W, attached, with explanations as noted therein.

CONCLUSION

For the reason stated herein and as presented in the Application and supporting documents, the Owners request that the Planning Board approve the plans for a site sensitive development be approved as submitted.

Randall Hiller Elaine Hiller By Their Attorney

10

Patricia S. Nelson 19 Muzzey Street, Suite 207 Lexington MA 02421 781-863-8688 psnelson@masslaw.us



Town of Lexington Planning Office

Land Use, Health and Development Department 1625 Massachusetts Avenue Lexington, MA 02420

Tel: (781) 698-4560

FORM W APPLICATION FOR WAIVERS

Applicant: Randall Hiller and Elaine Hiller

Description of Land: 8 Adams Street, Lexington MA 02420

Type of Development: Site Sensitive Development

Item #	Section of Development Regulations	From (the required standard): To (the proposed alternative):
1	c 135 Section 9.9.	From 6511 square feet To 7395 square feet
		- -

This form is to be submitted with the application for development.

In addition, §176-3.4 of the Zoning Regulations and/or §175-3.5 of the Subdivision Regulations requires:

- 1.a plan showing how the site would be developed if the plan complied with that provision of these Regulations and no waiver is granted; and
 - 2.a narrative statement that explains how granting the waiver would be in the public interest and not inconsistent with the intent and purpose of the Subdivision Control Law. (Please use a separate sheet of paper.)

1625 MASSACHUSETTS AVENUE • LEXINGTON, MASSACHUSETTS 02420

8 ADAMS STREET - DEFINITIVE SITE SENSITIVE PLAN

FORM W - ADDENDUM

Item #1 – The Applicants Randall and Elaine Hiller request a waiver from c. 135 section 6.9.9 on the following grounds:

1. The existing 1903 arts and crafts style home was constructed in a style that features "strong horizontal lines" and includes a "large semi-circular [covered] porch at the south end". Because the porch is covered, it technically is included in the site coverage calculations. Were the cover to be removed, the development as a whole would meet current site coverage requirements. A photo of the porch is part of the report of Nancy Seasholes to the Lexington Historical Commission, Form B, a copy of which is submitted with Applicants' materials. The waiver would avoid penalizing the Owners for keeping this historic feature intact.

2 A new home could be constructed with an additional story on a smaller footprint that would comply with site coverage requirements (see materials submitted herewith). Compared with the taller building, the proposed lower profile building would be more in keeping with the "strong horizontal lines" of the existing building and would present a lower profile as seen from Adams Street and the home of the abutters at 10 Adams Street.

Randy Hiller 8 Adams Street Lexington, MA 02420

July 11, 2018

Town of Lexington Planning Board 1625 Massachusetts Ave. Lexington, MA 02420

To whom it may concern,

I am the current owner/developer of 8 Adams Street. I have lived in the beautiful historic house on the property since 1995, and have lived in Lexington since 1988. I wanted to provide some context for my application for a Site Sensitive permit to develop a new house sharing a driveway with the existing #8 Adams.

A few years ago, in conversation with Lester Savage, it became clear to me that the size of the lot at 8 Adams could potentially endanger the preservation of the beautiful historic Willard Brown 1902 house currently on the site. The large lot has remained undeveloped in the past because the road frontage on Adams Street is insufficient to allow a second house. Lester showed me how a developer could, by removing the existing house, put a cul-de-sac on the property and create two buildable lots. The pressure to build new houses in Lexington would increasingly jeopardize the preservation of the existing historic house. I love this historic house. My father wrote a wonderful historic retrospective of the property, a copy of which currently resides at the Lexington Historical Society.

In response to this threat, I, in conjunction with Gary Larson, put together a Site Sensitive development plan to create a second lot on the property without the need to destroy the existing house by utilizing a shared driveway. In our preliminary hearing, Planning Board member Ginna Johnson said that the plan we had submitted was the first Site Sensitive Development Plan she had seen that adhered to what the Site Sensitive development code was truly written for. I was encouraged to move forward.

At the subsequent Planning Board meeting, I presented a proposed low profile house that my immediate neighbor at 10 Adams Street strongly supported. My neighbor was worried that the site coverage limitations would require us to build a 2.5 story house, which would be both less sensitive to the existing site and would obstruct his view more. After spending the past year trying to locate a developer who would carry the development plan to fruition, it became clear to me that most developers were interested in maximizing the size of the new house with very little sensitivity to my prior agreement with my neighbor or with blending with the existing house at 8 Adams Street. Hence, I have decided to develop the property myself with the help of local businesses, Colin Smith Architecture and Sramowicz General Contractors.

In this final version of our Site Sensitive Development plan, Colin Smith Architecture has created a stunning low-profile home that fits with the existing historic home on the property. He has reduced the footprint, and added architectural features that link the new home to the architectural style of the existing home designed by Willard Brown. While we have reduced the footprint of the new home from what we originally proposed, we still ask you to give us a variance on the site coverage limitations. We feel this is appropriate for three reasons: 1) our most impacted neighbor (at 10 Adams Street) has strongly requested that we limit the height of the new house. 2) Both houses (existing #8 and the proposed new low profile house) fall well within the 15% site coverage limitations on their respective properties for our zoning district. 3) our calculations of site coverage include the covered porch of the existing house... we feel it is important to maintain the historic character of the house and not to remove the covering roof of the existing porch in order to get under the site coverage limitations. Without the covered porch, we are well within the site sensitive site coverage guidelines.

The plan we have submitted maintains the historical character of the site with a beautiful custom home designed by local architect Colin Smith and built by local builders, Michael and Paul Sramowicz. Colin Smith's team has put together a exquisite design that adheres to the character of the existing Willard Brown house while maintaining the appeal of a a low profile carriage house. This enables us to utilize the additional land on this one and one half acre lot without destroying the existing historical house.

I sincerely hope that you see the value of the Site Sensitive proposal we have submitted, and that you grant us the requested site coverage waiver. Thank so much for your time and commitment to the Town of Lexington.

Sincerely

Randall Hiller Owner, 8 Adams Street

STORMWATER ANALYSIS AND CALCULATIONS

for

8 ADAMS STREET LEXINGTON, MASSACHUSETTS

Prepared for:

Randall S. & Elaine H. Hiller 8 Adams Street Lexington, Massachusetts 02421

Prepared by:

Meridian Associates, Inc. 500 Cummings Center, Suite 5950 Beverly, Massachusetts 01915 (978) 299-0447

SSOCIA



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Appendix:

- * Pre-Development Drainage Plan
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CALCULATION METHODS

- TR 20 SCS Unit Hydrograph Procedure
- Runoff Curve Numbers
- Time of Concentration by TR55 Methodology
- Reach and Pond Rating by the Dynamic Storage-Indication Method
- Manning Equation

SOURCE OF DATA

- Technical Report No. 20
- Technical Report No. 55
- Technical Paper No. 40
- Field Survey and Soil Testing by Meridian Associates, Inc.
- Massachusetts Stormwater Handbook February 2008

REPORT SUMMARY:

This project proposes to create a residential development through the process outlined in Chapter 175, Section 11F of the Lexington Development Regulations.

Calculation Objective

The purpose of this drainage analysis is to design a stormwater management system that maintains and/or reduces the peak rates and volumes of stormwater runoff from pre development conditions in the post development conditions for the 1, 2, 10 and 100-year design storm events

The proposed stormwater management system designed for this project will consist of the installation of three (3) subsurface infiltration systems. These systems will collect stormwater runoff from roof area, driveways, walkways and grassed areas via the use of an area drain or gutters and downspouts. The installation of the three (3) subsurface infiltration systems will allow the development to not have an increase in stormwater runoff (rate or volume) from the site during the 1, 2, 10 and 100-year design storms

Classification of Soils:

Existing soil conditions within the limits of the watershed analyzed for this study have been categorized as:

- Merrimac-Urban land complex, 0-8% Slopes, Hydrologic Group A.
- Charlton-Urban land-Hollis complex, 3-15% Slopes, Hydrologic Group A.

The classification is based upon the Natural Resource Conservation Service Maps dated May 1984. A copy of this soil map is contained in the Appendix of this report. Onsite soil testing was conducted by Meridian Associates Inc. on March 30, 2016 in the areas depicted on the attached plan. This testing revealed a loamy sand parent material with no groundwater observed at depths varying from 112" to 144".

Selection of Storm Events

The storm event frequencies and intensities have been selected based upon the Massachusetts Stormwater Guidelines requirements. The storm event rainfall data has been compiled from the Soil Conservation Service Technical Report No. 55 and the U.S. Department of Commerce Technical Paper No. 40.. Rainfall frequency data has been provided as follows:

Frequency	Rainfall [24 hour event(inch)]
1 year	2.5
2 year	3.1
10 year	4.6
100 year	6.6

Existing Site Overview

The site is a single family lot consisting of a single-family home, detached garage, bituminous concrete driveway, associated walkways, decks, porches and grassed/landscaped areas.

- Subcatchment SC1 This subcatchment area consists of portions of the existing house, driveway and grassed areas. Stormwater runoff generated in this subcatchment flows southerly across the lot into an existing area drain (DP1).
- Subcatchment SC2 This subcatchment area consists of portions of the existing house, a retaining wall and grassed areas. Stormwater runoff generated in this subcatchment flows southerly across the lot towards an abutters property. (DP2).
- Subcatchment SC3 This subcatchment area consists of portions of the existing house, driveway and grassed areas. Stormwater runoff generated in this subcatchment flows westerly across the lot towards an abutters property (DP3).
- Subcatchment SC4 This subcatchment area consists of portions of the existing house, retaining walls, concrete and grassed areas. Stormwater runoff generated in this subcatchment flows northwesterly across the lot towards an abutters property. (DP4).

Proposed Site Overview

The proposed project is comprised of the redevelopment of the existing residential property into a residential subdivision. The proposed development includes the creation of a second single family dwelling. This proposed development will include an attached garage addition to the existing dwelling, razing the existing detached garage and replacing it with a new single family dwelling. Additionally associated driveways, walkways and patios are proposed for both dwellings.

This project will not be subject to the Massachusetts Stormwater Management Standards as all the disturbance will occur beyond any wetland resource areas or their associated buffers and this is a project defined as a "housing development comprised of detached single-family dwellings on four or fewer lots that does not contain a stormwater discharge that may affect a critical area". It is also not subject to the Town of Lexington Stomrwater Bylaw as it does not alter more than one (1) acre of land.

However, a formal drainage system has been designed in order to manage stormwater runoff in an appropriate and responsible manner. The proposed project has been developed with the intent of maintaining the existing drainage patterns of the site to the maximum extent practicable.

In order to not increase runoff from the subject property portions of the runoff from the proposed site improvements will be directed to subsurface infiltration systems to mitigate for any increases in rate and volume of runoff to the selected Design Points during the designated storm rainfall events. The six (6) subcatchments in the post construction scenario are as follows:

- Subcatchment SC101 This subcatchment area consists of existing roof area, proposed driveway and grassed. Stormwater runoff generated in this subcatchment flows southerly across the lot into an area drain (DP1) which will outlet to a proposed subsurface infiltration system (PSIS-3).
- Subcatchment SC201 This subcatchment area consists of portions of the existing house, a retaining wall and grassed areas. Stormwater runoff generated in this subcatchment flows southerly across the lot towards an abutters property. (DP2).
- Subcatchment SC301 This subcatchment area consists of portions of the existing house, proposed driveway, proposed patio and grassed areas. Stormwater runoff generated in this subcatchment flows westerly across the lot towards an abutters property (DP3).
- Subcatchment SC401 This subcatchment area consists of portions of the proposed patio and grassed areas. Stormwater runoff generated in this subcatchment flows northwesterly across the lot towards an abutters property. (DP4).
- Subcatchment SC501 This subcatchment area consists of the entire roof area of the proposed single family dwelling. Stormwater runoff generated in this subcatchment is captured by gutters and downspouts and directed to a proposed subsurface infiltration system (PSIS-1).
- Subcatchment SC601 This subcatchment area consists of the entire roof area of the proposed attached garage addition, along with a portion

of the existing roof. Stormwater runoff generated in this subcatchment is captured by gutters and downspouts and directed to a proposed subsurface infiltration system (**PSIS-2**).

Summary of Flows at the Design Point

Design Point 1 (DP1)

Peak Rates (CFS)

DP1	1-year Storm	2-Year Storm	10-Year Storm	100-Year Storm
Existing	0.02	0.06	0.35	0.91
Proposed	0.00	0.00	0.00	0.00

Peak Volumes (CF)

DP1	1-Inch Storm	2-Year Storm	10-Year Storm	100-Year Storm
Existing	188	483	1,348	3,020
Proposed	0	0	0	0

Design Point 2 (DP2)

Peak Rates (CFS)

DP2	1-Inch Storm	2-Year Storm	10-Year Storm	100-Year Storm
Existing	ting 0.00 0.0	0.00	0.03	0.09
Proposed	0.00	0.00	0.03	0.09

Peak Volumes (CF)

DP2	1-Inch Storm	2-Year Storm	10-Year Storm	100-Year Storm
Existing	11	33	124	301
Proposed	11	33	124	301

Design Point 3 (DP3)

Peak Rates (CFS)

DP3	1-year Storm	2-Year Storm	10-Year Storm	100-Year Storm
Existing	0.02	0.07	0.48	1.29
Proposed	0.00	0.03	0.29	0.89

Peak Volumes (CF)

DP3	1-Inch Storm	2-Year Storm	10-Year Storm	100-Year Storm
Existing	242 583	583	1,889	4,312
Proposed	117	339	1,268	3,084

Design Point 4 (DP4)

Peak Rates (CFS)

DP4	1-Inch Storm	2-Year Storm	10-Year Storm	100-Year Storm
Existing	0.00 0	0.00	0.03	0.24
Proposed	0.00	0.00	0.01	0.14

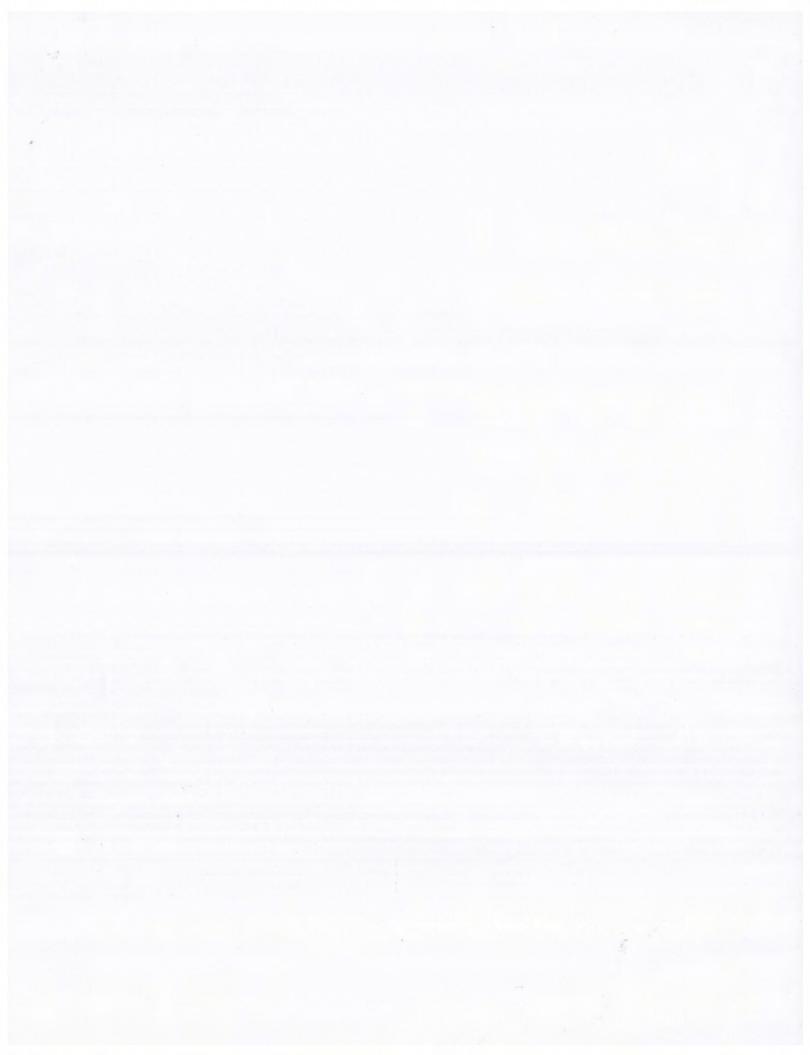
Peak Volumes (CF)

DP4	1-Inch Storm	2-Year Storm	10-Year Storm	100-Year Storm
Existing	disting 0	20	348	1,263
Proposed	0	4	211	875

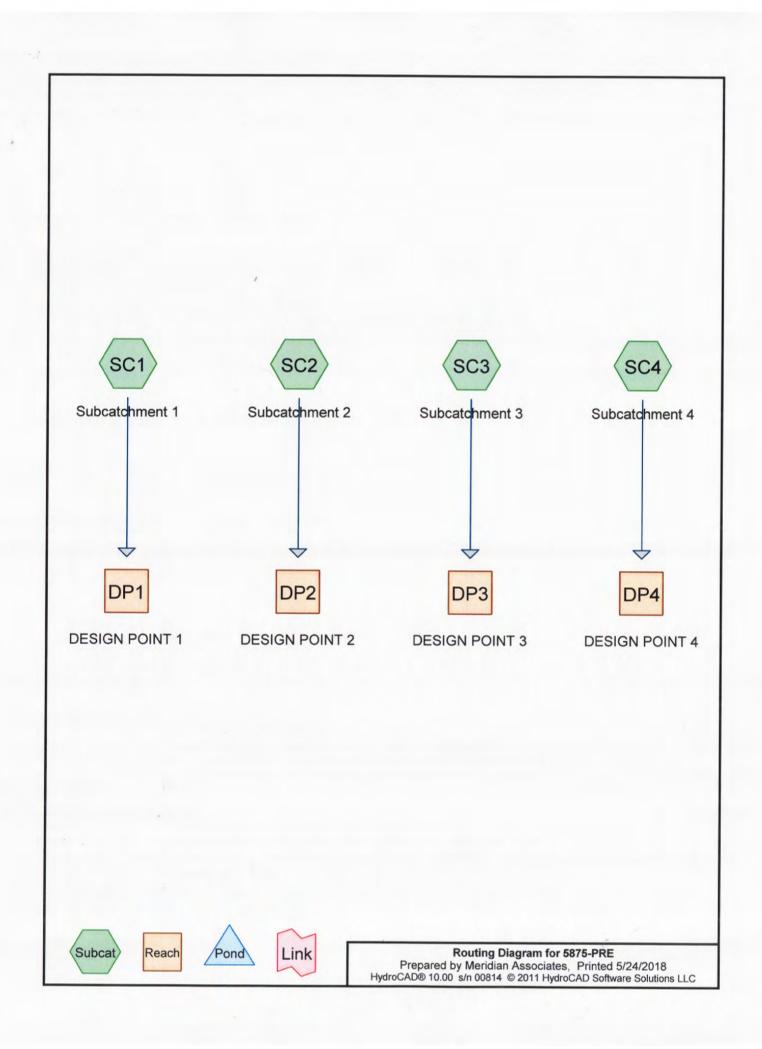
Conclusion

The calculations for each of the selected Design Points demonstrate that proposed site improvements will not result in an increase in the peak rate or volume of stormwater runoff for the 1-year, 2-year, 10-year or 100-year 24-hour storm events at the design point with the proposed stormwater mitigation system improvements.

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EXISTING CONDITIONS WATERSHED ROUTING DIAGRAM



8 Adams St, Lexington Ma

5875-PRE

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Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
46,208	39	
9,050	98	>75% Grass cover, Good, HSG A (SC1, SC2, SC3, SC4) Paved parking, HSG A (SC1, SC3)
1,158	98	ROOF (SC1)
3,958	98	Roofs, HSG A (SC2, SC3, SC4)
90	98	Wall, HSG A (SC2)
420	98	Walls and Concrete (SC4)
60,884	53	TOTAL AREA

EXISTING CONDITIONS 1-YEAR DESIGN

 5875-PRE
 Type III 24-hr 1-Year Design Storm Rainfall=2.50"

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 Printed 5/24/2018

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Summary for Subcatchment SC1: Subcatchment 1

Runoff	=	0.02 cfs @	12.41 hrs,	Volume=	188 cf, Depth= 0.13"
--------	---	------------	------------	---------	----------------------

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1-Year Design Storm Rainfall=2.50"

-	Area (sf)	CN	Description	1	
	11,593	39	>75% Gras	s cover, Go	bod, HSG A
	4,170	98	Paved park	king, HSG A	
*	1,158	98	ROOF	-	
	16,921	58	Weighted A	verage	
	11,593		68.51% Pe		
	5,328		31.49% Im	pervious Ar	ea
(m	Tc Length iin) (feet)	and the second se		Capacity (cfs)	Description
(6.0				Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC2: Subcatchment 2

Runoff =	0.00 cfs @	14.59 hrs,	Volume=	11 cf.	Depth= 0.07"
----------	------------	------------	---------	--------	--------------

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1-Year Design Storm Rainfall=2.50"

A	rea (sf)	CN	Description		
	415	98	Roofs, HSC	ĞΑ	CALL AND A C
	1,514	39	>75% Gras	s cover, Go	bod, HSG A
۲	90		Wall, HSG		
	2,019 1,514 505		Weighted A 74.99% Pei 25.01% Imp	rvious Area	
Tc (min)	Length (feet)	Slope (ft/ft)	· · · · · · · · · · · · · · · · · · ·	Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC3: Subcatchment 3

Runoff = 0.02 cfs @ 12.45 hrs, Volume= 242 cf, Depth=	0.12"
---	-------

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1-Year Design Storm Rainfall=2.50" 8 Adams St, Lexington Ma "Type III 24-hr 1-Year Design Storm Rainfall=2.50 Printed 5/24/2018

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A	rea (sf)	CN	Description					
	2,689	98	Roofs, HSG A					
	17,656	39	>75% Grass cover, Good, HSG A					
	4,880	98	Paved parking, HSG A					
	25,225	57	Weighted A	verage				
	17,656	69.99% Pervious Area						
	7,569		30.01% Imp	pervious Ar	ea			
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
6.0					Direct Entry, Min. Standard Engineering Practice			

Summary for Subcatchment SC4: Subcatchment 4

Runoff	=	0.00 cfs @	0.00 hrs,	Volume=	0 cf, Depth= 0.00"
--------	---	------------	-----------	---------	--------------------

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1-Year Design Storm Rainfall=2.50"

	Area (sf)	CN	Description		the standard to be a second				
	15,445	39	>75% Gras	s cover, Go	ood, HSG A				
	420	98	Walls and Concrete						
	854	98	Roofs, HSC	GΑ					
	16,719	43	Weighted A	Weighted Average					
	15,445		92.38% Pe						
	1,274		7.62% Impe	ervious Are	a				
Тс	Length	Slope	e Velocity	Capacity	Description				
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					

6.0

Direct Entry, Min. Standard Engineering Practice

Summary for Reach DP1: DESIGN POINT 1

Inflow Are	ea =	16,921 sf, 31.49% Impervious	, Inflow Depth = 0.13"	for 1-Year Design Storm event
Inflow	=	0.02 cfs @ 12.41 hrs, Volume=		9
Outflow	=	0.02 cfs @ 12.41 hrs, Volume=	188 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP2: DESIGN POINT 2

Inflow Are	ea =	2,019 sf, 2	25.01% Impervious,	Inflow Depth = 0.07"	for 1-Year Design Storm event
Inflow	=		4.59 hrs, Volume=		•
Outflow	=	0.00 cfs @ 14	4.59 hrs, Volume=	11 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

5875-PRE

 5875-PRE
 Type III 24-hr
 1-Year Design Storm Rainfall=2.50"

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Summary for Reach DP3: DESIGN POINT 3

 Inflow Area =
 25,225 sf, 30.01% Impervious, Inflow Depth =
 0.12" for 1-Year Design Storm event

 Inflow =
 0.02 cfs @
 12.45 hrs, Volume=
 242 cf

 Outflow =
 0.02 cfs @
 12.45 hrs, Volume=
 242 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP4: DESIGN POINT 4

Inflow Are	ea =	16,719 sf,	7.62% Impervious,	Inflow Depth = 0.00"	for 1-Year Design Storm event
Inflow	=		0.00 hrs, Volume=		
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



EXISTING CONDITIONS 2-YEAR DESIGN

 5875-PRE
 Type III 24-hr 2-Year Design Storm Rainfall=3.10"

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Summary for Subcatchment SC1: Subcatchment 1

Runoff	=	0.06 cfs @	12.26 hrs,	Volume=	433 cf, Depth= 0.31"
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.10"

A	rea (sf)	CN	Description		
	11,593	39	>75% Gras	s cover, Go	bod, HSG A
	4,170	98	Paved park	ing, HSG A	
	1,158	98	ROOF		
	16,921	58	Weighted A	verage	
	11,593			rvious Area	
	5,328		31.49% lmp	pervious Ar	ea
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC2: Subcatchment 2

Runoff = 0.00 cfs @ 12.38 hrs, Volume= 33 cf, Depth= 0.20	Runoff	=	0.00 cfs @	12.38 hrs.	Volume=	33 cf.	Depth= 0.20"
---	--------	---	------------	------------	---------	--------	--------------

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.10"

A	rea (sf)	CN	Description				
	415	98	Roofs, HSC	ΞA			
	1,514	39	>75% Gras	s cover, Go	ood, HSG A		
	90		Wall, HSG				
	2,019	54	Weighted A	verage			
	1,514		74.99% Pervious Area				
	505		25.01% Impervious Area				
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description		
6.0					Direct Entry, Min. Standard Engineering Practice		

Summary for Subcatchment SC3: Subcatchment 3

Runoff = 0.07 cfs @ 12.30 hrs, Volume= 58	33 cf,	Depth=	0.28"
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.10" 8 Adams St, Lexington Ma Type III 24-hr 2-Year Design Storm Rainfall=3.10" Printed 5/24/2018

5875-PRE

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A	rea (sf)	CN	Description			
	2,689	98	Roofs, HSC	6 A	the second	
	17,656	39	>75% Gras	s cover, Go	ood, HSG A	
	4,880		Paved park	the second se		
	25,225	57	Weighted A	verage		
	17,656		69.99% Pe			
	7,569		30.01% Imp	pervious Ar	ea	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description	
6.0				100000	Direct Entry, Min. Standard	Engineering Practice

Summary for Subcatchment SC4: Subcatchment 4

Runoff = 0.00 cfs @ 21.24 hrs, Volume= 20 cf, Depth= 0.01"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.10"

	Area (sf)	CN	Description		the second s				
	15,445	39	>75% Gras	s cover, Go	ood, HSG A				
*	420	98		Valls and Concrete					
	854	98	Roofs, HSC	A					
	16,719	43	Weighted Average						
	15,445		92.38% Per						
	1,274		7.62% Impe	ervious Are	a				
Тс	Length	Slop	e Velocity	Capacity	Description				
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)					

6.0

Direct Entry, Min. Standard Engineering Practice

Summary for Reach DP1: DESIGN POINT 1

Inflow Are	a =	16,921 sf, 31.4	9% Impervious,	Inflow Depth = 0).31" fc	or 2-Year Design Storm event
Inflow	=	0.06 cfs @ 12.26		433 cf		•
Outflow	=	0.06 cfs @ 12.26	6 hrs, Volume=	433 cf,	Atten=	0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP2: DESIGN POINT 2

Inflow Are	a =	2,019 sf, 25.01% Impervious,	Inflow Depth = 0.20" for 2-Year Design Storm event
Inflow	=	0.00 cfs @ 12.38 hrs, Volume=	
Outflow	=	0.00 cfs @ 12.38 hrs, Volume=	33 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

 8 Adams St, Lexington Ma

 5875-PRE
 Type III 24-hr 2-Year Design Storm Rainfall=3.10"

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Summary for Reach DP3: DESIGN POINT 3

 Inflow Area =
 25,225 sf, 30.01% Impervious, Inflow Depth =
 0.28" for 2-Year Design Storm event

 Inflow =
 0.07 cfs @
 12.30 hrs, Volume=
 583 cf

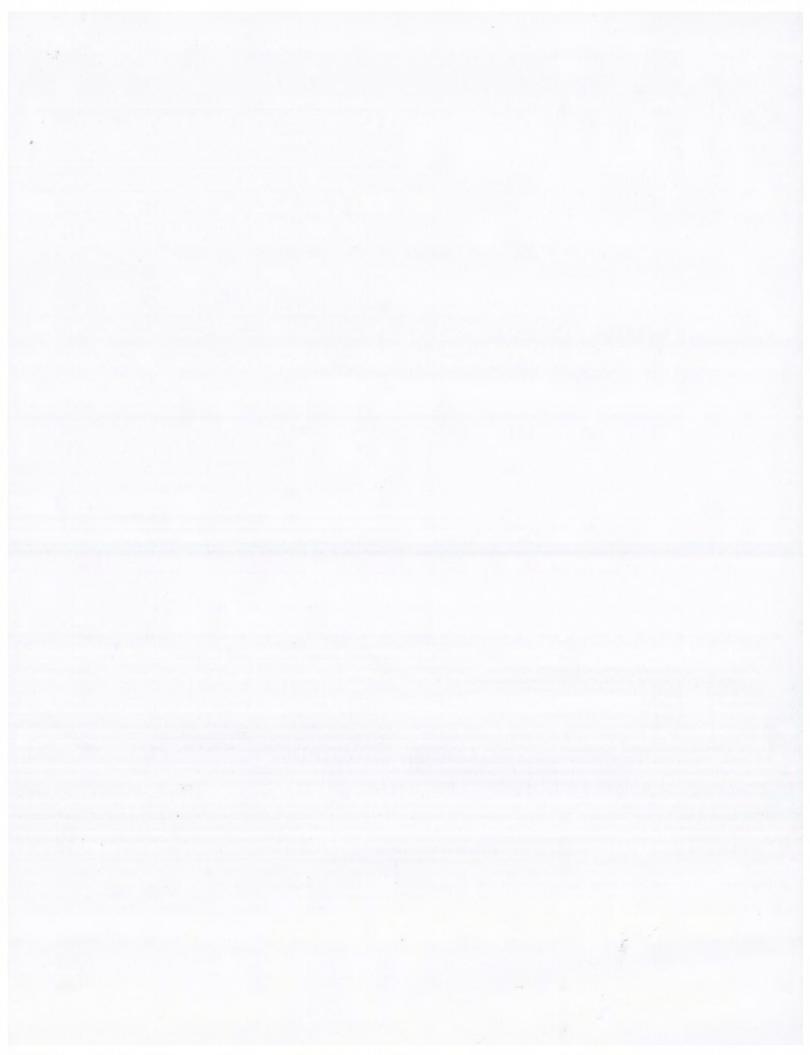
 Outflow =
 0.07 cfs @
 12.30 hrs, Volume=
 583 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP4: DESIGN POINT 4

Inflow Are	a =	16,719 sf, 7.62% Impervious	Inflow Depth = 0.01" for 2-Year Design Storm event
Inflow	=	0.00 cfs @ 21.24 hrs, Volume=	20 cf
Outflow	=	0.00 cfs @ 21.24 hrs, Volume=	20 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



EXISTING CONDITIONS 10-YEAR DESIGN STORM

 5875-PRE
 Type III 24-hr
 10-Year Design Storm Rainfall=4.60"

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Summary for Subcatchment SC1: Subcatchment 1

Runoff	=	0.35 cfs @	12.11 hrs, Volume=	1,348 cf, Depth= 0.96"
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=4.60"

A	rea (sf)	CN	Description		
	11,593	39	>75% Gras	s cover, Go	bod, HSG A
	4,170	98	Paved park	ing, HSG A	
	1,158	98	ROOF		
	16,921	58	Weighted A	verage	
	11,593			vious Area	
	5,328		31.49% Imp	pervious Ar	ea
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC2: Subcatchment 2

Runoff	=	0.03 cfs @	12.12 hrs,	Volume=	124 cf.	Depth= 0.73"
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=4.60"

A	rea (sf)	CN	Description			
	415	98	Roofs, HSC	ΞA	STATES AND A STATES	
	1,514	39	>75% Gras	s cover, Go	bod, HSG A	
k	90	98	Wall, HSG	A		
	2,019 1,514 505		Weighted Average 74.99% Pervious Area 25.01% Impervious Area			
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description	
6.0					Direct Entry, Min. Standard Engineering Practice	

Summary for Subcatchment SC3: Subcatchment 3

Runoff = 0.48 cfs @ 12.11 hrs, Volume= 1,889 cf, Depth= 0.90"	Runoff	=	0.48 cfs @	12.11 hrs,	Volume=	1,889 cf, Depth= 0.90"
---	--------	---	------------	------------	---------	------------------------

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=4.60" 8 Adams St, Lexington Ma Type III 24-hr 10-Year Design Storm Rainfall=4.60" Printed 5/24/2018

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A	rea (sf)	CN	Description					
	2,689	98	Roofs, HSC	6 A				
	17,656	39	>75% Grass cover, Good, HSG A					
4,880 98 Paved parking, HSG A								
25,225 57 Weighted Average 17,656 69.99% Pervious Area 7,569 30.01% Impervious Area				vious Area				
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
6.0			1.00000		Direct Entry, Min. Standard Engineering Practice			

Summary for Subcatchment SC4: Subcatchment 4

Runoff = 0.03 cfs @ 12.41 hrs, Volume= 348 cf, Depth= 0.25"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=4.60"

	Area (sf)	CN	Description					
	15,445	39	>75% Gras	s cover, Go	ood, HSG A			
ł.	420	98	Walls and Concrete					
	854	98	Roofs, HSC	3 A				
	16,719	43	Weighted A	verage				
	15,445		92.38% Per					
	1,274		7.62% Impe	ervious Area	a			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				

6.0

Direct Entry, Min. Standard Engineering Practice

Summary for Reach DP1: DESIGN POINT 1

Inflow Are	a =	16,921 sf, 31.49% Impervious,	Inflow Depth = 0.96" for 10-Year Design Storm event
Inflow	=	0.35 cfs @ 12.11 hrs, Volume=	1,348 cf
Outflow	=	0.35 cfs @ 12.11 hrs, Volume=	1,348 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP2: DESIGN POINT 2

Inflow Are	ea =	2,019 sf, 25.01% Impervious.	Inflow Depth = 0.73" for 10-Year Design Storm event
Inflow	=	0.03 cfs @ 12.12 hrs, Volume=	124 cf
Outflow	=	0.03 cfs @ 12.12 hrs, Volume=	124 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

5875-PRE

 5875-PRE
 Type III 24-hr
 10-Year Design Storm Rainfall=4.60"

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Summary for Reach DP3: DESIGN POINT 3

 Inflow Area =
 25,225 sf, 30.01% Impervious, Inflow Depth =
 0.90" for 10-Year Design Storm event

 Inflow =
 0.48 cfs @
 12.11 hrs, Volume=
 1,889 cf

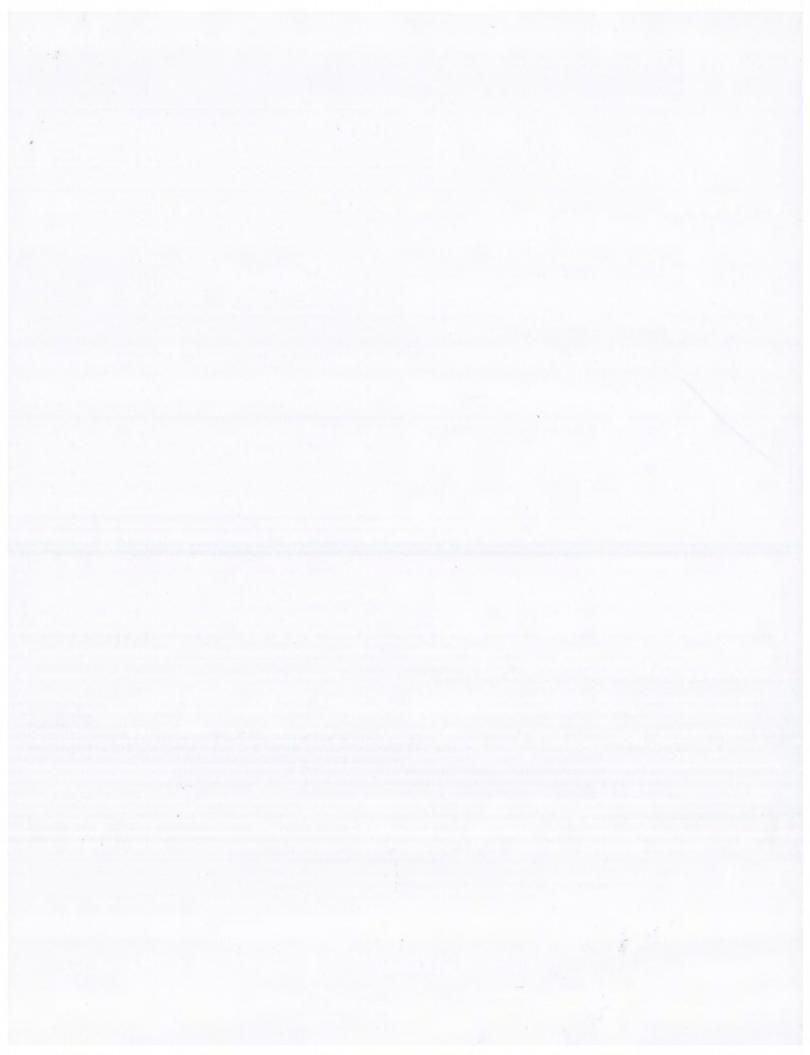
 Outflow =
 0.48 cfs @
 12.11 hrs, Volume=
 1,889 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP4: DESIGN POINT 4

Inflow Are	a =	16,719 sf, 7.62% Impervious	, Inflow Depth = 0.25" for 10-Year Design Storm event
Inflow	=	0.03 cfs @ 12.41 hrs, Volume=	348 cf
Outflow	=	0.03 cfs @ 12.41 hrs, Volume=	348 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



EXISTING CONDITIONS 100-YEAR DESIGN STORM

5875-PRE Type III 24-hr 100-Year Design Storm Rainfall=6.60" Prepared by Meridian Associates HydroCAD® 10.00 s/n 00814 © 2011 HydroCAD Software Solutions LLC

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Summary for Subcatchment SC1: Subcatchment 1

Runoff	=	0.91 cfs @	12.10 hrs, Volume=	3,020 cf, Depth= 2.14"
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=6.60"

	A	rea (sf)	CN	Description	É.	
1		11,593	39	>75% Gras	s cover, Go	bod, HSG A
		4,170	98	Paved park	ing, HSG A	
*		1,158	98	ROOF		
		16,921	58	Weighted A	verage	
		11,593		68.51% Pe		
		5,328		31.49% Imp		
	Tc (min)	Length (feet)	Slop (ft/ft		Capacity (cfs)	Description
	6.0	-				Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC2: Subcatchment 2

Runoff	=	0.09 cfs @	12.10 hrs,	Volume=	301 cf, Depth	= 1.79"
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=6.60"

_	A	rea (sf)	CN	Description	haven	
		415	98	Roofs, HSC	θA	
		1,514	39	>75% Gras	s cover, Go	bod, HSG A
*		90	98	Wall, HSG	A	
-		2,019	54	Weighted A	verage	
		1,514		74.99% Pe		
		505		25.01% Imp	pervious Ar	ea
	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
	6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC3: Subcatchment 3

Runoff	=	1.29 cfs @	12.10 hrs,	Volume=	4,312 cf, Depth= 2	2.05"
--------	---	------------	------------	---------	--------------------	-------

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=6.60"

5875-PRE

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8 Adams St, Lexington Ma Type III 24-hr 100-Year Design Storm Rainfall=6.60" Printed 5/24/2018 Page 13

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A	rea (sf)	CN	Description	_	
	2,689	98	Roofs, HSC	6 A	COLANDO
	17,656	39	>75% Gras	s cover, Go	bod, HSG A
	4,880		Paved park		
25,225 57 Weigh 17,656 69.99%			Weighted A 69.99% Per 30.01% Imp	vious Area	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC4: Subcatchment 4

Runoff 0.24 cfs @ 12.13 hrs, Volume= 1,263 cf, Depth= 0.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=6.60"

	Area (sf)	CN	Description	6			
	15,445	39	>75% Gras	s cover, Go	ood, HSG A		
*	420	98	Walls and Concrete				
-	854	98	Roofs, HSG A				
-	16,719	43	Weighted A	verage			
	15,445						
	1,274						
	Tc Length			Capacity	Description		
(1	min) (feet) (ft/	ft) (ft/sec)	(cfs)			

6.0

Direct Entry, Min. Standard Engineering Practice

Summary for Reach DP1: DESIGN POINT 1

Inflow Are	ea =	16,921 sf, 31.49% Impervious, Inflov	v Depth = 2.14" for 100-Year Design Storm event
Inflow	=	0.91 cfs @ 12.10 hrs, Volume=	3,020 cf
Outflow	=	0.91 cfs @ 12.10 hrs, Volume=	3,020 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP2: DESIGN POINT 2

Inflow Are	a =	2,019 sf, 25.01% Impervious,	Inflow Depth = 1.79" for 100-Year Design Storm event
Inflow	=	0.09 cfs @ 12.10 hrs, Volume=	301 cf
Outflow	=	0.09 cfs @ 12.10 hrs, Volume=	301 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

 5875-PRE
 Type III 24-hr
 100-Year Design Storm Rainfall=6.60"

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Summary for Reach DP3: DESIGN POINT 3

 Inflow Area =
 25,225 sf, 30.01% Impervious, Inflow Depth =
 2.05" for 100-Year Design Storm event

 Inflow =
 1.29 cfs @
 12.10 hrs, Volume=
 4,312 cf

 Outflow =
 1.29 cfs @
 12.10 hrs, Volume=
 4,312 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

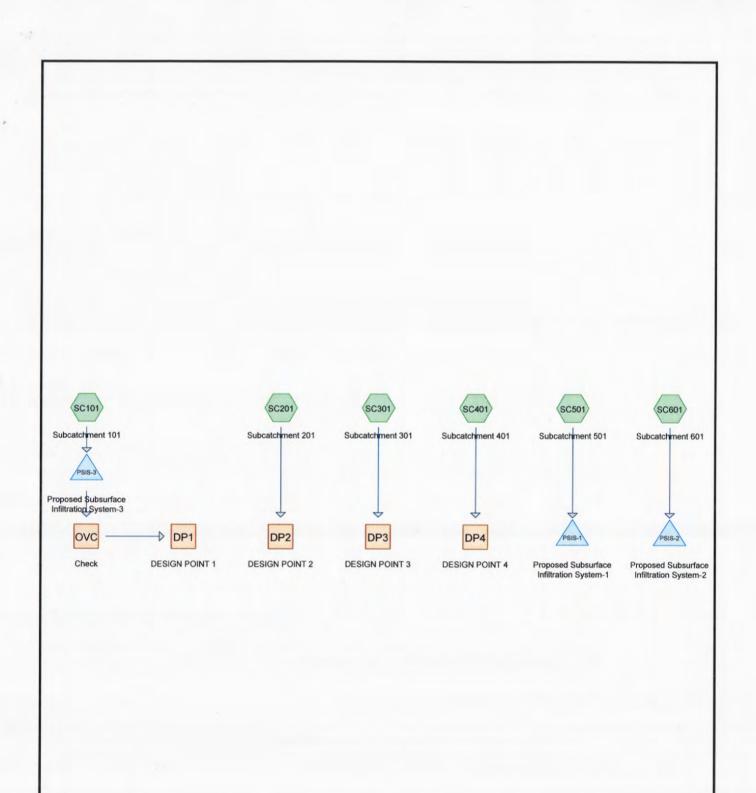
Summary for Reach DP4: DESIGN POINT 4

Inflow Are	a =	16,719 sf, 7.62% Impervious,	Inflow Depth = 0.91" for 100-Year Design Storm event
Inflow	=	0.24 cfs @ 12.13 hrs, Volume=	
Outflow	=	0.24 cfs @ 12.13 hrs, Volume=	1,263 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



PROPOSED CONDITIONS WATERSHED ROUTING DIAGRAM



Link

Pond

Reach

Subcat

Routing Diagram for 5875-POST Prepared by Meridian Associates, Printed 5/24/2018 HydroCAD® 10.00 s/n 00814 © 2011 HydroCAD Software Solutions LLC

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5875-POST

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Area Listing (all nodes)

Area	CN	Description
 (sq-ft)		(subcatchment-numbers)
42,087	39	>75% Grass cover, Good, HSG A (SC101, SC201, SC301, SC401)
5,422	98	PROPOSED DRIVEWAY (SC101)
3,152	98	PROPOSED DRIVEWAY/WALKS (SC301)
1,435	98	PROPOSED PATIO (SC301, SC401)
3,321	98	PROPOSED ROOF (SC501)
3,686	98	ROOF (SC101, SC601)
1,691	98	Roofs, HSG A (SC201, SC301)
90	98	Wall (SC201)
60,884	57	TOTAL AREA

PROPOSED CONDITIONS 1-YEAR DESIGN STORM

 5875-POST
 Type III 24-hr
 1-Year Design Storm Rainfall=2.50"

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Summary for Subcatchment SC101: Subcatchment 101

Runoff = 0.03 cfs @ 12.36 hrs, Volume= 271 cf, Depth= 0.17"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1-Year Design Storm Rainfall=2.50"

*			Descripti					
*	1,290	98	ROOF					
	5,422	98	PROPOS	ED DRI	VEW	/AY		
	11,999	39	>75% Gr	ass cove	er, Go	ood, HSG A		
	18,711	60	Weighter					
	11,999		64.13% I		10.07 (D)(T)			
	6,712		35.87%	mperviou	us Ar	ea		
Tc (min)	Length (feet)	Slop (ft/ft			acity (cfs)	Description		
6.0						Direct Entry, I	Min. Standard Engineering Practice	
Runoff	-		cfs @ 14				11 cf, Depth= 0.07"	
Runoff b Type III	by SCS TF 24-hr 1-Y	0.00 (R-20 me ′ear De	cfs @ 14 ethod, UH sign Storr	.59 hrs, =SCS, T n Rainfal	Volu ime \$	ume= Span= 0.00-72.0		
Runoff b Type III	by SCS TF 24-hr 1-Y area (sf)	0.00 o R-20 me ′ear De <u>CN</u>	cfs @ 14 ethod, UH sign Storr Descripti	.59 hrs, =SCS, T n Rainfal on	Volu ime \$	ume= Span= 0.00-72.0	11 cf, Depth= 0.07"	
Runoff b Type III	by SCS TF 24-hr 1-Y Area (sf) 416	0.00 0 R-20 me ′ear De <u>CN</u> 98	cfs @ 14 ethod, UH sign Storr <u>Descripti</u> Roofs, H	.59 hrs, =SCS, T n Rainfal on SG A	Volu ime \$ II=2.5	ume= Span= 0.00-72.0 50''	11 cf, Depth= 0.07"	
Runoff b Type III	by SCS TF 24-hr 1-Y <u>area (sf)</u> 416 1,513	0.00 c R-20 me ′ear De <u>CN</u> 98 39	cfs @ 14 ethod, UH sign Storn <u>Descripti</u> Roofs, H >75% Gr	.59 hrs, =SCS, T n Rainfal on SG A	Volu ime \$ II=2.5	ume= Span= 0.00-72.0	11 cf, Depth= 0.07"	
Runoff b Type III	by SCS TF 24-hr 1-Y area (sf) 416 1,513 90	0.00 (ear De <u>CN</u> 98 39 98	cfs @ 14 ethod, UH sign Storn <u>Descripti</u> Roofs, H >75% Gr Wall	.59 hrs, =SCS, T n Rainfal on SG A ass cove	Volu ime \$ II=2.5 er, Go	ume= Span= 0.00-72.0 50''	11 cf, Depth= 0.07"	
Runoff b Type III	by SCS TF 24-hr 1-Y (rea (sf) 416 1,513 90 2,019	0.00 c R-20 me ′ear De <u>CN</u> 98 39	cfs @ 14 ethod, UH sign Storn <u>Descripti</u> Roofs, H >75% Gr <u>Wall</u> Weighted	.59 hrs, =SCS, T n Rainfal on SG A ass cove	Volu ime S II=2.5 er, Go	ume= Span= 0.00-72.0 50'' bod, HSG A	11 cf, Depth= 0.07"	
Runoff b	DY SCS TR	0.00 (R-20 me	cfs @ 14 ethod, UH	.59 hrs, =SCS, T	Volu ime \$	ume= Span= 0.00-72.0	11 cf, Depth= 0.07"	
Runoff b Type III	by SCS TF 24-hr 1-Y area (sf) 416 1,513 90	0.00 (ear De <u>CN</u> 98 39 98	cfs @ 14 ethod, UH sign Storn <u>Descripti</u> Roofs, H >75% Gr Wall	.59 hrs, =SCS, T n Rainfal on SG A ass cove	Volu ime \$ II=2.5 er, Go	ume= Span= 0.00-72.0 50''	11 cf, Depth= 0.07"	
Runoff b Type III	by SCS TF 24-hr 1-Y area (sf) 416 1,513 90	0.00 (ear De <u>CN</u> 98 39 98	cfs @ 14 ethod, UH sign Storn <u>Descripti</u> Roofs, H >75% Gr Wall	.59 hrs, =SCS, T n Rainfal on SG A ass cove	Volu ime S II=2.5 er, Go	ume= Span= 0.00-72.0 50'' bod, HSG A	11 cf, Depth= 0.07"	

6.0

Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC301: Subcatchment 301

Runoff = 0.00 cfs @ 14.59 hrs, Volume= 117 cf, Depth= 0.07"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1-Year Design Storm Rainfall=2.50"

8 Adams St, Lexington Ma Type III 24-hr 1-Year Design Storm Rainfall=2.50" Prepared by Meridian Associates HydroCAD® 10.00 s/n 00814 © 2011 HydroCAD Software Solutions LLC Printed 5/24/2018

	Area (sf)	CN Description						
	1,275	98 Roofs, HSG A 39 >75% Grass cover, Good, HSG A						
	15,334	>75% Grass cover, Good, HSG A						
*	3,152	98 PROPOSED DRIVEWAY/WALKS						
-	947	98 PROPOSED PATIO						
	20,708	54 Weighted Average						
	15,334 5,374	74.05% Pervious Area 25.95% Impervious Area						
	5,574	25.95% Impervious Area						
Тс	Length	Slope Velocity Capacity Description						
(min)	(feet)	(ft/ft) (ft/sec) (cfs)						
6.0	a second	Direct Entry, Min. Standard Engineering Practice						
		Summary for Subcatchment SC401: Subcatchment 401						
Runoff	=	0.00 cfs @ 0.00 hrs, Volume= 0 cf, Depth= 0.00"						
A	<u>rea (sf)</u> 13,241	CN Description 39 >75% Grass cover, Good, HSG A						
	488	98 PROPOSED PATIO						
	13,729	41 Weighted Average						
	13,241	96.45% Pervious Area						
	488	3.55% Impervious Area						
Тс	Length	Slope Velocity Capacity Description						
	(feet)	(ft/ft) (ft/sec) (cfs)						
(min) 6.0	(feet)	(ft/ft) (ft/sec) (cfs) Direct Entry, Min. Standard Engineering Practice	-					
(min)	(feet)							
<u>(min)</u> 6.0	(feet) =	Direct Entry, Min. Standard Engineering Practice						
(min) 6.0 Runoff Runoff b	= by SCS TR	Direct Entry, Min. Standard Engineering Practice Summary for Subcatchment SC501: Subcatchment 501						
(min) 6.0 Runoff Runoff b Type III	= by SCS TR	Direct Entry, Min. Standard Engineering Practice Summary for Subcatchment SC501: Subcatchment 501 0.18 cfs @ 12.09 hrs, Volume= 628 cf, Depth= 2.27" 20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs						

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A	rea (sf)	CN L	Description		
*	3,321	98 F	PROPOSE	D ROOF	
	3,321	1	100.00% In	npervious A	rea
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

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5875-POST	Type III 24-hr 1-Year Design Storm Rainfall=2.50"
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Summary for Subcatchment SC601: Subcatchment 601

Runoff = 0.13 cfs @ 12.09 hrs, Volume= 453 cf, Depth= 2.27"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 1-Year Design Storm Rainfall=2.50"

A	rea (sf)	CN	Description		
	2,396	98	ROOF		
	2,396		100.00% In	npervious A	rea
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Reach DP1: DESIGN POINT 1

Inflow Are	ea =	18,711 sf,	35.87% Impervious,	Inflow Depth = 0.00"	for 1-Year Design Storm event
Inflow	=		0.00 hrs, Volume=		3
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP2: DESIGN POINT 2

Inflow Are	ea =	2,019 sf, 25.06% Impervious,	Inflow Depth = 0.07" for 1-Year Design Storm event
Inflow	=	0.00 cfs @ 14.59 hrs, Volume=	11 cf
Outflow	=	0.00 cfs @ 14.59 hrs, Volume=	11 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP3: DESIGN POINT 3

Inflow Are	ea =	20,708 sf,	25.95% Impervious,	Inflow Depth = 0.07"	for 1-Year Design Storm event
Inflow	=		14.59 hrs, Volume=	117 cf	
Outflow	=	0.00 cfs @	14.59 hrs, Volume=	117 cf. Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP4: DESIGN POINT 4

Inflow Are	ea =	13,729 sf,	3.55% Impervious,	Inflow Depth = 0.00"	for 1-Year Design Storm event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	3
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atten=	= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

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 Type III 24-hr 1-Year Design Storm Rainfall=2.50"

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Summary for Reach OVC: Check

Inflow Area =18,711 sf, 35.87% Impervious, Inflow Depth = 0.00" for 1-Year Design Storm eventInflow =0.00 cfs @0.00 hrs, Volume=0 cfOutflow =0.00 cfs @0.00 hrs, Volume=0 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs Average Depth at Peak Storage= 0.00' Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 2.31 cfs

6.0" Round Pipe n= 0.010 PVC, smooth interior Length= 1.0' Slope= 0.1000 '/' Inlet Invert= 245.00', Outlet Invert= 244.90'

Summary for Pond PSIS-1: Proposed Subsurface Infiltration System-1

Inflow Area	a =	3,321 sf,100.00% Impervious, Inflow Depth =	2.27" for 1-Year Design Storm event
Inflow	=	0.18 cfs @ 12.09 hrs, Volume= 628 d	· · · · · · · · · · · · · · · · · · ·
Outflow	=	0.02 cfs @ 12.61 hrs, Volume= 628 c	cf, Atten= 86%, Lag= 31.2 min
Discarded	=	0.02 cfs @ 12.61 hrs, Volume= 628 d	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 240.40' @ 12.61 hrs Surf.Area= 375 sf Storage= 194 cf

Plug-Flow detention time= 51.2 min calculated for 628 cf (100% of inflow) Center-of-Mass det. time= 51.2 min (813.1 - 761.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	239.50'	356 cf	15.75'W x 23.80'L x 3.50'H Field A
			1,312 cf Overall - 422 cf Embedded = 890 cf x 40.0% Voids
#2A	240.00'	422 cf	StormTech SC-740 × 9 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		778 of	Total Available Storage

778 cf Total Available Storage

Storage Group A created with Chamber Wizard

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 Type III 24-hr 1-Year Design Storm Rainfall=2.50"

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Device	Routing	Invert	Outlet Devices	
#1	Discarded	239.50'	2.410 in/hr Exfiltration over Wetted area	

Discarded OutFlow Max=0.02 cfs @ 12.61 hrs HW=240.40' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Summary for Pond PSIS-2: Proposed Subsurface Infiltration System-2

Inflow Area	a =	2,396 sf,100.00% Impervious, Inflow Depth = 2.27" for 1-Year Design Storm	n event
Inflow	=	0.13 cfs @ 12.09 hrs, Volume= 453 cf	
Outflow	=	0.02 cfs @ 12.61 hrs, Volume= 453 cf, Atten= 86%, Lag= 31.1 min	
Discarded	=	0.02 cfs @ 12.61 hrs, Volume= 453 cf	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 240.94' @ 12.61 hrs Surf.Area= 263 sf Storage= 140 cf

Plug-Flow detention time= 51.7 min calculated for 453 cf (100% of inflow) Center-of-Mass det. time= 51.7 min (813.6 - 761.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	240.00'	254 cf	15.75'W x 16.68'L x 3.50'H Field A 919 cf Overall - 284 cf Embedded = 635 cf x 40.0% Voids
#2A	240.50'	284 cf	StormTech SC-740 x 6 Inside #1 Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		538 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	240.00'	2.410 in/hr Exfiltration over Wetted area	

Discarded OutFlow Max=0.02 cfs @ 12.61 hrs HW=240.94' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Summary for Pond PSIS-3: Proposed Subsurface Infiltration System-3

Inflow Area	a =	18,711 sf, 35.87% Impervious	, Inflow Depth = 0.17" for 1-Year Design Storm event
Inflow	=	0.03 cfs @ 12.36 hrs, Volume=	
Outflow	=	0.03 cfs @ 12.43 hrs, Volume=	271 cf, Atten= 5%, Lag= 4.3 min
Discarded	=	0.03 cfs @ 12.43 hrs, Volume=	271 cf
Primary	=	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 242.02' @ 12.43 hrs Surf.Area= 928 sf Storage= 7 cf

Plug-Flow detention time= 4.2 min calculated for 271 cf (100% of inflow) Center-of-Mass det. time= 4.2 min (968.8 - 964.7) 8 Adams St, Lexington Ma Type III 24-hr 1-Year Design Storm Rainfall=2.50" Printed 5/24/2018

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Volume	Invert	Avail.Storage	Storage Description
#1A	242.00'	851 cf	30.00'W x 30.92'L x 3.50'H Field A 3,246 cf Overall - 1,120 cf Embedded = 2,127 cf x 40.0% Voids
#2A	242.50'	1,120 cf	StormTech SC-740 x 24 Inside #1 Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 6 rows
		1,970 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	242.00'	2.410 in/hr Exfiltration over Wetted area	_
#2	Primary	245.00'	6.0" Vert. Orifice/Grate C= 0.600	

Discarded OutFlow Max=0.05 cfs @ 12.43 hrs HW=242.02' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=242.00' (Free Discharge)

PROPOSED CONDITIONS 2-YEAR DESIGN STORM

 5875-POST
 Type III 24-hr 2-Year Design Storm Rainfall=3.10"

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Summary for Subcatchment SC101: Subcatchment 101

Runoff = 0.10 cfs @ 12.15 hrs, Volume= 577 cf, Depth= 0.37"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.10"

1	Area (sf)	CN	Description	n		
*	1,290	98	ROOF			
*	5,422	98	PROPOSE	D DRIVEV	VAY	
	11,999	39	>75% Gras	s cover, G	Good, HSG A	
	18,711	60	Weighted /	Average	A REAL PROPERTY OF	
	11,999			rvious Are	а	
	6,712		35.87% Im	pervious A	rea	
Tc (min)		Slope (ft/ft)		Capacity (cfs)		
6.0					Direct Entry	Min. Standard Engineering Practice
		Sum	mary for	Subcatcl	hment SC201	: Subcatchment 201
D		0.00	- 40.0	O has Mal		
Runoff	=	0.00 c	fs @ 12.3	88 hrs, Vol	ume=	33 cf, Depth= 0.20"
Runoff	by SCS TF	R-20 met	thod, UH=		Span= 0.00-72	
Runoff Type III	by SCS TF	R-20 mei ′ear Des	thod, UH=	SCS, Time Rainfall=3.	Span= 0.00-72	33 cf, Depth= 0.20"
Runoff Type III	by SCS TF 24-hr 2-Y	R-20 me l'ear Des <u>CN I</u>	thod, UH=8 ign Storm	SCS, Time Rainfall=3.	Span= 0.00-72	33 cf, Depth= 0.20"
Runoff Type III	by SCS TF 24-hr 2-Y Area (sf)	R-20 me rear Des <u>CN I</u> 98 I	thod, UH=s ign Storm <u>Descriptior</u> Roofs, HS0	SCS, Time Rainfall=3. 1 G A	Span= 0.00-72	33 cf, Depth= 0.20"

	00	00 1	van	and the second se	
	2,019	54 V	Veighted A	verage	
	1,513	7	4.94% Per	vious Area	
	506	2	5.06% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.0			- 10, 20		Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC301: Subcatchment 301

Runoff = 0.03 cfs @ 12.38 hrs, Volume= 339 cf, Depth= 0.20"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.10" 8 Adams St, Lexington Ma Type III 24-hr 2-Year Design Storm Rainfall=3.10" Printed 5/24/2018 Page 10

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A	rea (sf)	CN	Description			
	1,275	98	Roofs, HSG	6 A	Contraction of the	
	15,334	39	>75% Gras			
*	3,152	98			AY/WALKS	
e.	947	98	PROPOSEI	and the second se	No. and the second second	
	20,708	54	Weighted A			
	15,334		74.05% Per			
	5,374		25.95% Imp	pervious Ar	ea	
Tc (min)	Length (feet)	Slope (ft/ft	· · · · · · · · · · · · · · · · · · ·	Capacity (cfs)	Description	
6.0	(1001)	(1011	(10300)	(013)	Direct Entry, Mi	n. Standard Engineering Practice
		Sum	nmary for s	Subcatch	ment SC401: S	ubcatchment 401
Runoff	=	0.00	cfs @ 23.7	7 hrs, Volu	me=	4 cf, Depth= 0.00"
ype III	24-hr 2-Y	ear De	sign Storm F	Dainfall-2 1	011	
			sign otornin	annan-5.	0	
А	rea (sf)	CN	-		0	
A	area (sf) 13,241	<u>CN</u> 39	Description			
A	area (sf) 13,241 488	CN 39 98	-	s cover, Go		
A	13,241	39	Description >75% Grass	s cover, Go D PATIO		
A	13,241 488 13,729 13,241	39 98	Description >75% Grass PROPOSEI Weighted A 96.45% Per	s cover, Go <u>D PATIO</u> verage vious Area	od, HSG A	
A •	13,241 488 13,729	39 98	Description >75% Grass PROPOSEI Weighted A	s cover, Go <u>D PATIO</u> verage vious Area	od, HSG A	
	13,241 488 13,729 13,241 488	39 98 41	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe	s cover, Go D PATIO verage vious Area ervious Area	od, HSG A	
Tc	13,241 488 13,729 13,241 488 Length	39 98 41 Slope	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe	s cover, Go D PATIO verage vious Area ervious Area Capacity	od, HSG A	
Tc (min)	13,241 488 13,729 13,241 488	39 98 41	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe	s cover, Go D PATIO verage vious Area ervious Area	od, HSG A	n. Standard Engineering Practice
Tc	13,241 488 13,729 13,241 488 Length	39 98 41 Slope	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe	s cover, Go D PATIO verage vious Area ervious Area Capacity	od, HSG A	n. Standard Engineering Practice
Tc (min)	13,241 488 13,729 13,241 488 Length	39 98 41 Slope (ft/ft	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe e Velocity (ft/sec)	s cover, Go D PATIO verage vious Area ervious Area Capacity (cfs)	od, HSG A Description Direct Entry, Min	n. Standard Engineering Practice
Tc (min)	13,241 488 13,729 13,241 488 Length	39 98 41 Slope (ft/ft	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe e Velocity (ft/sec)	s cover, Go <u>D PATIO</u> verage vious Area ervious Area Capacity (cfs)	ood, HSG A Description Direct Entry, Min ment SC501: S	
Tc (min) 6.0 Runoff	13,241 488 13,729 13,241 488 Length (feet)	39 98 41 Slope (ft/ft Sum 0.22 o	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe e Velocity (ft/sec)	s cover, Go <u>D PATIO</u> verage vious Area ervious Area Capacity (cfs) Subcatch P hrs, Volu	ood, HSG A Description Direct Entry, Min ment SC501: S me= 7	94 cf, Depth= 2.87"
Tc (min) 6.0 Runoff	13,241 488 13,729 13,241 488 Length (feet) =	39 98 41 Slope (ft/ft Sum 0.22 (Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe e Velocity (ft/sec)	s cover, Go <u>D PATIO</u> verage vious Area ervious Area Capacity (cfs) Subcatch P hrs, Volu CS, Time S	od, HSG A Description Direct Entry, Min ment SC501: S me= 7 Span= 0.00-72.00	94 cf, Depth= 2.87"
Tc (min) 6.0 Runoff Runoff b Type III	13,241 488 13,729 13,241 488 Length (feet) =	39 98 41 Slope (ft/ft Sum 0.22 (Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe e Velocity (ft/sec)	s cover, Go <u>D PATIO</u> verage vious Area ervious Area Capacity (cfs) Subcatch P hrs, Volu CS, Time S	od, HSG A Description Direct Entry, Min ment SC501: S me= 7 Span= 0.00-72.00	94 cf, Depth= 2.87"
Tc (min) 6.0 Runoff Runoff b Type III	13,241 488 13,729 13,241 488 Length (feet) = 24-hr 2-Y	39 98 41 Slope (ft/ft Sum 0.22 d c-20 me ear Des	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe e Velocity (ft/sec) mary for S cfs @ 12.09 ethod, UH=S sign Storm F	s cover, Go <u>D PATIO</u> verage vious Area ervious Area Capacity (cfs) Subcatch 9 hrs, Volu CS, Time S Rainfall=3.1	od, HSG A Description Direct Entry, Min ment SC501: S me= 7 Span= 0.00-72.00	94 cf, Depth= 2.87"
Tc (min) 6.0 Runoff Runoff b Type III	13,241 488 13,729 13,241 488 Length (feet) = by SCS TR 24-hr 2-Y	39 98 41 Slope (ft/ft Sum 0.22 c 2-20 me ear Des CN	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe e Velocity (ft/sec) mary for S cfs @ 12.09 ethod, UH=S sign Storm F Description	s cover, Go D PATIO verage vious Area ervious Area capacity (cfs) Subcatch hrs, Volu CS, Time S Rainfall=3.1	od, HSG A Description Direct Entry, Min ment SC501: S me= 7: Span= 0.00-72.00 0''	94 cf, Depth= 2.87"
Tc (min) 6.0 Runoff Runoff b Type III	13,241 488 13,729 13,241 488 Length (feet) = by SCS TR 24-hr 2-Y rea (sf) 3,321	39 98 41 Slope (ft/ft Sum 0.22 c 2-20 me ear Des CN	Description >75% Grass PROPOSEI Weighted A 96.45% Per 3.55% Impe e Velocity (ft/sec) mary for S cfs @ 12.09 ethod, UH=S sign Storm F Description PROPOSEI 100.00% Im	s cover, Go D PATIO verage vious Area ervious Area capacity (cfs) Subcatch hrs, Volu CS, Time S Rainfall=3.1	od, HSG A Description Direct Entry, Min ment SC501: S me= 7: Span= 0.00-72.00 0''	94 cf, Depth= 2.87"

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5875-POST	Type III 24-hr 2-Year Design Storm Rainfall=3.10"
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Summary for Subcatchment SC601: Subcatchment 601

Runoff = 0.16 cfs @ 12.09 hrs, Volume= 573 cf, Depth= 2.87"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.10"

A	rea (sf)	CN	Description		
k.	2,396	98	ROOF		
	2,396		100.00% In	npervious A	rea
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Reach DP1: DESIGN POINT 1

Inflow Are	ea =	18,711 sf,	35.87% Impervious,	Inflow Depth = 0.00"	for 2-Year Design Storm event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP2: DESIGN POINT 2

Inflow Are	a =	2,019 sf, 25.06% Impervious,	Inflow Depth = 0.20" for 2-Year Design Storm event
Inflow	=	0.00 cfs @ 12.38 hrs, Volume=	33 cf
Outflow	=	0.00 cfs @ 12.38 hrs, Volume=	33 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP3: DESIGN POINT 3

Inflow Are	ea =	20,708 sf, 2	25.95% Impervious,	Inflow Depth = $0.20"$	for 2-Year Design Storm event
Inflow	=	0.03 cfs @ 12	2.38 hrs, Volume=	339 cf	
Outflow	=	0.03 cfs @ 12	2.38 hrs, Volume=	339 cf. Atter	n= 0%. Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP4: DESIGN POINT 4

Inflow Are	ea =	13,729 sf, 3.55% Impervious,	Inflow Depth = 0.00" for 2-Year Design Storm event
Inflow	=	0.00 cfs @ 23.77 hrs, Volume=	4 cf
Outflow	=	0.00 cfs @ 23.77 hrs, Volume=	4 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

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 Type III 24-hr
 2-Year Design Storm Rainfall=3.10"

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Summary for Reach OVC: Check

Inflow Area =18,711 sf, 35.87% Impervious, Inflow Depth = 0.00" for 2-Year Design Storm eventInflow =0.00 cfs @0.00 hrs, Volume=0 cfOutflow =0.00 cfs @0.00 hrs, Volume=0 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs Average Depth at Peak Storage= 0.00' Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 2.31 cfs

6.0" Round Pipe n= 0.010 PVC, smooth interior Length= 1.0' Slope= 0.1000 '/' Inlet Invert= 245.00', Outlet Invert= 244.90'

Summary for Pond PSIS-1: Proposed Subsurface Infiltration System-1

Inflow Area	a =	3,321 sf,100.00% Impervious, Inflow Depth = 2.87" for 2-Year Design Storm event
Inflow	=	0.22 cfs @ 12.09 hrs, Volume= 794 cf
Outflow	=	0.03 cfs @ 12.71 hrs, Volume= 794 cf, Atten= 88%, Lag= 37.1 min
Discarded	=	0.03 cfs @ 12.71 hrs, Volume= 794 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 240.65' @ 12.71 hrs Surf.Area= 375 sf Storage= 264 cf

Plug-Flow detention time= 71.2 min calculated for 793 cf (100% of inflow) Center-of-Mass det. time= 71.2 min (828.3 - 757.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	239.50'	356 cf	15.75'W x 23.80'L x 3.50'H Field A
1			1,312 cf Overall - 422 cf Embedded = 890 cf x 40.0% Voids
#2A	240.00'	422 cf	StormTech SC-740 x 9 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		778 cf	Total Available Storage

778 cf Total Available Storage

Storage Group A created with Chamber Wizard

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 Type III 24-hr 2-Year Design Storm Rainfall=3.10"

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Device	Routing	Invert	Outlet Devices
#1	Discarded	239.50'	2.410 in/hr Exfiltration over Wetted area

Discarded OutFlow Max=0.03 cfs @ 12.71 hrs HW=240.65' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Summary for Pond PSIS-2: Proposed Subsurface Infiltration System-2

Inflow Area	a =	2,396 sf,100.00% Impervious, Inflow Depth = 2.87" for 2-Year Design Storm even	nt
Inflow	=	0.16 cfs @ 12.09 hrs, Volume= 573 cf	
Outflow	=	0.02 cfs @ 12.69 hrs, Volume= 573 cf, Atten= 88%, Lag= 36.5 min	
Discarded	=	0.02 cfs @ 12.69 hrs, Volume= 573 cf	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 241.19' @ 12.69 hrs Surf.Area= 263 sf Storage= 191 cf

Plug-Flow detention time= 71.2 min calculated for 572 cf (100% of inflow) Center-of-Mass det. time= 71.2 min (828.3 - 757.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	240.00'	254 cf	15.75'W x 16.68'L x 3.50'H Field A 919 cf Overall - 284 cf Embedded = 635 cf x 40.0% Voids
#2A	240.50'	284 cf	StormTech SC-740 x 6 Inside #1 Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		538 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	240.00'	2.410 in/hr Exfiltration over Wetted area	
2011.1			A second	

Discarded OutFlow Max=0.02 cfs @ 12.69 hrs HW=241.19' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Summary for Pond PSIS-3: Proposed Subsurface Infiltration System-3

Inflow Area	a =	18,711 sf, 35.87% Impervious,	Inflow Depth = 0.37" for 2-Year Design Storm event
Inflow	=	0.10 cfs @ 12.15 hrs, Volume=	577 cf
Outflow	=	0.05 cfs @ 12.51 hrs, Volume=	577 cf, Atten= 46%, Lag= 21.3 min
Discarded	=	0.05 cfs @ 12.51 hrs, Volume=	577 cf
Primary	=	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 242.14' @ 12.51 hrs Surf.Area= 928 sf Storage= 50 cf

Plug-Flow detention time= 6.3 min calculated for 577 cf (100% of inflow) Center-of-Mass det. time= 6.3 min (931.2 - 924.9)

8 Adams St, Lexington Ma 5875-POST Type III 24-hr 2-Year Design Storm Rainfall=3.10" Prepared by Meridian Associates Printed 5/24/2018 HydroCAD® 10.00 s/n 00814 © 2011 HydroCAD Software Solutions LLC Page 14 Volume Invert Avail.Storage Storage Description #1A 242.00' 30.00'W x 30.92'L x 3.50'H Field A 851 cf 3,246 cf Overall - 1,120 cf Embedded = 2,127 cf x 40.0% Voids #2A 242.50' StormTech SC-740 x 24 Inside #1 1,120 cf Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 6 rows 1,970 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	242.00'	2.410 in/hr Exfiltration over Wetted area
#2	Primary	245.00'	6.0" Vert. Orifice/Grate C= 0.600

Discarded OutFlow Max=0.05 cfs @ 12.51 hrs HW=242.14' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=242.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) **PROPOSED CONDITIONS** 10-YEAR DESIGN STORM

 8 Adams St, Lexington Ma

 5875-POST
 Type III 24-hr 10-Year Design Storm Rainfall=4.60"

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Summary for Subcatchment SC101: Subcatchment 101

Runoff = 0.46 cfs @ 12.11 hrs, Volume= 1,675 cf, Depth= 1.07"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=4.60"

A	rea (sf)	CN	Description	2	
	1,290	98	ROOF		
·	5,422	98	PROPOSE	D DRIVEW	/AY
	11,999	39	>75% Gras	s cover, Go	bod, HSG A
	18,711 11,999 6,712	60	Weighted A 64.13% Per 35.87% Imp	rvious Area	
Tc (min)	Length (feet)	Slope (ft/ft	· · · · · · · · · · · · · · · · · · ·	Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC201: Subcatchment 201

Runoff = 0.03 cfs @ 12.12 hrs, Volume= 124 cf, Depth= 0.	Runoff	=	0.03 cfs @	12.12 hrs,	Volume=	124 cf, Depth= 0.73
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=4.60"

A	rea (sf)	CN	Description		
	416	98	Roofs, HSC	ĞΑ	and the second
	1,513	39	>75% Gras	s cover, Go	ood, HSG A
	90	98	Wall		
	2,019 1,513 506		Weighted A 74.94% Pei 25.06% Imp	rvious Area	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC301: Subcatchment 301

Runoff	=	0.29 cfs @	12.12 hrs,	Volume=	1,268 cf, Depth= 0.73"
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=4.60"

8 Adams St, Lexington Ma Type III 24-hr 10-Year Design Storm Rainfall=4.60" Prepared by Meridian Associates HydroCAD® 10.00 s/n 00814 © 2011 HydroCAD Software Solutions LLC Printed 5/24/2018 Page 16

A	rea (sf)	CN	Description	n		
	1,275	98	Roofs, HSC	GA		
	15,334	39			ood, HSG A	
*	3,152	98			AY/WALKS	
*	947	98	PROPOSE	D PATIO		
	20,708	54	Weighted A			
	15,334			ervious Area		
	5,374		25.95% Im	pervious Ar	ea	
Тс	Length	Slope			Description	
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)		and the second
6.0					Direct Entry	, Min. Standard Engineering Practice
		Sum	mary for	Subcatch	ment SC40	1: Subcatchment 401
Runoff	=	0.01	cfs @ 12.4	8 hrs, Volu	ıme=	211 cf, Depth= 0.18"
Type III :			esign Storm			2.00 hrs, dt= 0.05 hrs
	24-hr 10-	Year D	esign Storm	n Rainfall=4		
	24-hr 10- rea (sf)	Year D CN	esign Storm	n Rainfall=4	.60"	
	24-hr 10- <u>rea (sf)</u> 13,241	Year D <u>CN</u> 39	esign Storm Description >75% Gras	n Rainfall=4 n ss cover, Go		
	24-hr 10- rea (sf) 13,241 488	Year D <u>CN</u> 39 98	esign Storm Description >75% Gras PROPOSE	n Rainfall=4 n ss cover, Go D PATIO	.60"	
	24-hr 10- rea (sf) 13,241 488 13,729	Year D <u>CN</u> 39	esign Storm Description >75% Gras PROPOSE Weighted A	n Rainfall=4 ss cover, Go D PATIO Average	.60" bod, HSG A	
	24-hr 10- rea (sf) 13,241 488	Year D <u>CN</u> 39 98	esign Storm Description >75% Gras PROPOSE Weighted A 96.45% Pe	n Rainfall=4 n ss cover, Go D PATIO	.60" bod, HSG A	
A	24-hr 10- <u>rea (sf)</u> 13,241 <u>488</u> 13,729 13,241 <u>488</u>	Year D <u>CN</u> 39 98 41	esign Storm >75% Gras PROPOSE Weighted A 96.45% Pe 3.55% Impo	n Rainfall=4 ss cover, Go D PATIO Average rvious Area ervious Area	.60" bod, HSG A	
	24-hr 10- rea (sf) 13,241 488 13,729 13,241	Year D <u>CN</u> 39 98	esign Storm >75% Gras PROPOSE Weighted A 96.45% Pe 3.55% Impo	n Rainfall=4 ss cover, Go D PATIO Average rvious Area ervious Area	.60" bod, HSG A	
A * Tc	24-hr 10- rea (sf) 13,241 488 13,729 13,241 488 Length	Year D CN 39 98 41 Slope	esign Storm >75% Gras PROPOSE Weighted A 96.45% Pe 3.55% Impo	n Rainfall=4 ss cover, Go D PATIO Average rvious Area ervious Area Capacity	.60" bod, HSG A a Description	, Min. Standard Engineering Practice
A * Tc (min)	24-hr 10- rea (sf) 13,241 488 13,729 13,241 488 Length	Year D CN 39 98 41 Slope (ft/ft	esign Storm Description >75% Gras PROPOSE Weighted A 96.45% Pe 3.55% Impo Velocity) (ft/sec)	n Rainfall=4 ss cover, Go D PATIO Average rvious Area ervious Area capacity (cfs)	.60" bod, HSG A a Description Direct Entry	
A * Tc (min) 6.0	24-hr 10- rea (sf) 13,241 488 13,729 13,241 488 Length (feet)	Year D CN 39 98 41 Slope (ft/ft	esign Storm Description >75% Gras PROPOSE Weighted A 96.45% Pe 3.55% Impo e Velocity) (ft/sec)	Rainfall=4 ss cover, Go D PATIO Average rvious Area ervious Area Capacity (cfs)	.60" bod, HSG A Description Direct Entry ment SC50	7, Min. Standard Engineering Practice 1: Subcatchment 501
A * Tc (min)	24-hr 10- rea (sf) 13,241 488 13,729 13,241 488 Length	Year D CN 39 98 41 Slope (ft/ft	esign Storm Description >75% Gras PROPOSE Weighted A 96.45% Pe 3.55% Impo Velocity) (ft/sec)	Rainfall=4 ss cover, Go D PATIO Average rvious Area ervious Area Capacity (cfs)	.60" bod, HSG A Description Direct Entry ment SC50	v, Min. Standard Engineering Practice
A Tc (min) 6.0 Runoff	24-hr 10- <u>rea (sf)</u> 13,241 488 13,729 13,241 488 Length (feet) = y SCS TR	Year D <u>CN</u> 39 98 41 Slope (ft/ft Sum 0.33 c 2-20 me	esign Storm Description >75% Gras PROPOSE Weighted A 96.45% Pe 3.55% Impo e Velocity) (ft/sec) mary for solution offs @ 12.0	A Rainfall=4 S cover, Go D PATIO Average rvious Area ervious Area capacity (cfs) Subcatch 9 hrs, Volu SCS, Time S	.60" bod, HSG A Description Direct Entry ment SC50 me= Span= 0.00-72	7, Min. Standard Engineering Practice 1: Subcatchment 501
A Tc (min) 6.0 Runoff Runoff b Type III 2	24-hr 10- rea (sf) 13,241 488 13,729 13,241 488 Length (feet) = y SCS TR 24-hr 10-	Year D CN 39 98 41 Slope (ft/ft Sum 0.33 c 2-20 me Year Do	esign Storm <u>Description</u> >75% Gras <u>PROPOSE</u> Weighted A 96.45% Pe 3.55% Impo e Velocity) (ft/sec) mary for cfs @ 12.0 ethod, UH=S esign Storm	A Rainfall=4 A Rainfall=4 A Society of the second	.60" bod, HSG A Description Direct Entry ment SC50 me= Span= 0.00-72	7, Min. Standard Engineering Practice 1: Subcatchment 501 1,208 cf, Depth= 4.36"
A Tc (min) 6.0 Runoff Runoff b Type III 2	24-hr 10- <u>rea (sf)</u> 13,241 488 13,729 13,241 488 Length (feet) = y SCS TR	Year D CN 39 98 41 Slope (ft/ft Sum 0.33 c 2-20 me Year Do CN	esign Storm <u>Description</u> >75% Gras <u>PROPOSE</u> Weighted A 96.45% Pe 3.55% Impo e Velocity) (ft/sec) mary for s ofs @ 12.0 ethod, UH=S	A Rainfall=4 A Rainfall=4 A scover, Go D PATIO A verage rvious Area ervious Area ervious Area Capacity (cfs) Subcatch 9 hrs, Volu SCS, Time S n Rainfall=4	.60" bod, HSG A Description Direct Entry ment SC50 me= Span= 0.00-72	7, Min. Standard Engineering Practice 1: Subcatchment 501 1,208 cf, Depth= 4.36"

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-	(min)	(feet)	(ft/sec)	Capacity (cfs)	Description	
	6.0				Direct Entry, Min. Standard Engineering Practice	

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5875-POST	Type III 24-hr 10-Year Design Storm Rainfall=4.60"
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Summary for Subcatchment SC601: Subcatchment 601

Runoff = 0.24 cfs @ 12.09 hrs, Volume= 871 cf, Depth= 4.36"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=4.60"

A	rea (sf)	CN	Description		
	2,396	98	ROOF		
	2,396		100.00% In	npervious A	rea
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
6.0		-			Direct Entry, Min. Standard Engineering Practice

Summary for Reach DP1: DESIGN POINT 1

Inflow Are	ea =	18,711 sf,	35.87% Impervious,	Inflow Depth = 0.00"	for 10-Year Design Storm event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP2: DESIGN POINT 2

Inflow Are	ea =	2,019 sf, 25.06% Impervious,	Inflow Depth = 0.73" for 10-Year Design Storm event
Inflow	=	0.03 cfs @ 12.12 hrs, Volume=	124 cf
Outflow	=	0.03 cfs @ 12.12 hrs, Volume=	124 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP3: DESIGN POINT 3

Inflow Are	ea =	20,708 sf, 25.95% Impervious	, Inflow Depth = 0.73" for 10-Year Design Storm event
Inflow	=	0.29 cfs @ 12.12 hrs, Volume=	1,268 cf
Outflow	=	0.29 cfs @ 12.12 hrs, Volume=	1,268 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP4: DESIGN POINT 4

Inflow Are	a =	13,729 sf, 3.55% Impervious	, Inflow Depth = 0.18" for 10-Year Design Storm event
Inflow	=	0.01 cfs @ 12.48 hrs, Volume=	211 cf
Outflow	=	0.01 cfs @ 12.48 hrs, Volume=	211 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

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8 Adams St, Lexington Ma Type III 24-hr 10-Year Design Storm Rainfall=4.60" Printed 5/24/2018 HydroCAD® 10.00 s/n 00814 © 2011 HydroCAD Software Solutions LLC Page 18

Summary for Reach OVC: Check

18,711 sf, 35.87% Impervious, Inflow Depth = 0.00" for 10-Year Design Storm event Inflow Area = Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0 cf Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs Average Depth at Peak Storage= 0.00' Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 2.31 cfs

6.0" Round Pipe n= 0.010 PVC, smooth interior Length= 1.0' Slope= 0.1000 '/' Inlet Invert= 245.00', Outlet Invert= 244.90'

Summary for Pond PSIS-1: Proposed Subsurface Infiltration System-1

Inflow Area	a =	3,321 sf,100.00% Impervious, Inflow Depth = 4.36" for 10-Year Design	n Storm event
Inflow	=	0.33 cfs @ 12.09 hrs, Volume= 1,208 cf	
Outflow	=	0.03 cfs @ 12.99 hrs, Volume= 1,208 cf, Atten= 91%, Lag= 54.2 r	min
Discarded	=	0.03 cfs @ 12.99 hrs, Volume= 1,208 cf	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 241.36' @ 12.99 hrs Surf.Area= 375 sf Storage= 457 cf

Plug-Flow detention time= 124.1 min calculated for 1,207 cf (100% of inflow) Center-of-Mass det. time= 124.0 min (873.5 - 749.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	239.50'	356 cf	15.75'W x 23.80'L x 3.50'H Field A
			1,312 cf Overall - 422 cf Embedded = 890 cf x 40.0% Voids
#2A	240.00'	422 cf	StormTech SC-740 x 9 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
		and the second se	Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		770 -6	Tatal Available Oteran

778 cf Total Available Storage

Storage Group A created with Chamber Wizard

 5875-POST
 Type III 24-hr 10-Year Design Storm Rainfall=4.60"

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Device	Routing	Invert	Outlet Devices	
#1	Discarded	239.50'	2.410 in/hr Exfiltration over Wetted area	

Discarded OutFlow Max=0.03 cfs @ 12.99 hrs HW=241.36' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Summary for Pond PSIS-2: Proposed Subsurface Infiltration System-2

Inflow Area	a =	2,396 sf,100.00% Impervious	, Inflow Depth = 4.36" for 10-Year Design Storm event
Inflow	=	0.24 cfs @ 12.09 hrs, Volume=	871 cf
Outflow	=	0.02 cfs @ 12.96 hrs, Volume=	871 cf, Atten= 91%, Lag= 52.5 min
Discarded	=	0.02 cfs @ 12.96 hrs, Volume=	871 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 241.93' @ 12.96 hrs Surf.Area= 263 sf Storage= 329 cf

Plug-Flow detention time= 121.6 min calculated for 871 cf (100% of inflow) Center-of-Mass det. time= 121.5 min (871.0 - 749.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	240.00'	254 cf	15.75'W x 16.68'L x 3.50'H Field A 919 cf Overall - 284 cf Embedded = 635 cf x 40.0% Voids
#2A	240.50'	284 cf	StormTech SC-740 x 6 Inside #1 Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		538 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	240.00'	2.410 in/hr Exfiltration over Wetted area	

Discarded OutFlow Max=0.02 cfs @ 12.96 hrs HW=241.93' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Summary for Pond PSIS-3: Proposed Subsurface Infiltration System-3

Inflow Area	a =	18,711 sf, 35.87% Impervious, Inflow Depth = 1.07" for 10-Year Design Storm event
Inflow	=	0.46 cfs @ 12.11 hrs, Volume= 1,675 cf
Outflow	=	0.06 cfs @ 13.32 hrs, Volume= 1,675 cf, Atten= 87%, Lag= 73.0 min
Discarded	=	0.06 cfs @ 13.32 hrs, Volume= 1,675 cf
Primary	=	0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 242.96' @ 13.32 hrs Surf.Area= 928 sf Storage= 531 cf

Plug-Flow detention time= 86.4 min calculated for 1,674 cf (100% of inflow) Center-of-Mass det. time= 86.3 min (968.3 - 881.9) 5875-POST

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8 Adams St, Lexington Ma *Type III 24-hr 10-Year Design Storm Rainfall=4.60"* Printed 5/24/2018 Software Solutions LLC Page 20

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Volume	Invert	Avail.Storage	Storage Description
#1A	242.00'	851 cf	30.00'W x 30.92'L x 3.50'H Field A 3,246 cf Overall - 1,120 cf Embedded = 2,127 cf x 40.0% Voids
#2A	242.50'	1,120 cf	StormTech SC-740 x 24 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 6 rows
		1,970 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Dutlet Devices			
#1	Discarded	242.00'	2.410 in/hr Exfiltration over Wetted area			
#2	Primary	245.00'	6.0" Vert. Orifice/Grate C= 0.600			

Discarded OutFlow Max=0.06 cfs @ 13.32 hrs HW=242.96' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.06 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=242.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs) PROPOSED CONDITIONS 100-YEAR DESIGN STORM

 5875-POST
 Type III 24-hr 100-Year Design Storm Rainfall=6.60"

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Summary for Subcatchment SC601: Subcatchment 601

Runoff = 0.35 cfs @ 12.09 hrs, Volume= 1,270 cf, Depth= 6.36"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=6.60"

A	rea (sf)	CN	Description		
	2,396	98	ROOF		
	2,396		100.00% Im	npervious A	rea
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Reach DP1: DESIGN POINT 1

Inflow Are	ea =	18,711 sf,	35.87% Impervious,	Inflow Depth = 0.00" for 100-Year Design Storm event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP2: DESIGN POINT 2

Inflow Are	a =	2,019 sf, 25.06% Impervious, Inflow Depth = 1.79"	for 100-Year Design Storm event
Inflow	=	0.09 cfs @ 12.10 hrs, Volume= 301 cf	
Outflow	=	0.09 cfs @ 12.10 hrs, Volume= 301 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP3: DESIGN POINT 3

Inflow Are	ea =	20,708 sf, 25.95% Impervious,	Inflow Depth = 1.79" for 100-Year Design Storm event
Inflow	=	0.89 cfs @ 12.10 hrs, Volume=	3,084 cf
Outflow	=	0.89 cfs @ 12.10 hrs, Volume=	3,084 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Reach DP4: DESIGN POINT 4

Inflow Are	a =	13,729 sf, 3.55% Impervious,	Inflow Depth = 0.76" for 100-Year Design Storm event
Inflow	=	0.14 cfs @ 12.15 hrs, Volume=	875 cf
Outflow	=	0.14 cfs @ 12.15 hrs, Volume=	875 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

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Summary for Reach OVC: Check

Inflow Area = 18,711 sf, 35.87% Impervious, Inflow Depth = 0.00" for 100-Year Design Storm event Inflow 0.00 hrs, Volume= = 0.00 cfs @ 0 cf 0.00 hrs, Volume= Outflow 0.00 cfs @ = 0 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs Average Depth at Peak Storage= 0.00' Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 2.31 cfs

6.0" Round Pipe n= 0.010 PVC, smooth interior Length= 1.0' Slope= 0.1000 '/' Inlet Invert= 245.00', Outlet Invert= 244.90'

Summary for Pond PSIS-1: Proposed Subsurface Infiltration System-1

Inflow Area	a =	3,321 sf.	100.00% Im	pervious,	Inflow Depth = 6.36" for 100-Yea	ar Design Storm event
Inflow	=	0.48 cfs @	12.09 hrs,	Volume=	1,760 cf	
Outflow	=	0.04 cfs @	13.23 hrs,	Volume=	1,760 cf, Atten= 93%, Lag=	= 68.6 min
Discarded	=	0.04 cfs @	13.23 hrs,	Volume=	1,760 cf	

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 242.77' @ 13.23 hrs Surf.Area= 375 sf Storage= 743 cf

Plug-Flow detention time= 191.2 min calculated for 1,760 cf (100% of inflow) Center-of-Mass det. time= 191.2 min (934.9 - 743.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	239.50'	356 cf	15.75'W x 23.80'L x 3.50'H Field A
#2A	240.00'	422 cf	1,312 cf Overall - 422 cf Embedded = 890 cf x 40.0% Voids StormTech SC-740 x 9 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		770 -6	Tatal Available Otanana

778 cf Total Available Storage

Storage Group A created with Chamber Wizard

 5875-POST
 Type III 24-hr
 100-Year Design Storm Rainfall=6.60"

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Summary for Subcatchment SC101: Subcatchment 101

Runoff = 1.11 cfs @ 12.10 hrs, Volume= 3,624 cf, Depth= 2.32"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=6.60"

A	rea (sf)	CN	Description		
	1,290	98	ROOF	1.00	
	5,422	98	PROPOSE	D DRIVEW	/AY
	11,999	39	>75% Gras	s cover, Go	bod, HSG A
	18,711 11,999 6,712		Weighted A 64.13% Pe 35.87% Imp	rvious Area	
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC201: Subcatchment 201

Runoff = 0.09 cfs @ 12.10 hrs, Volume= 301 cf, Dep	epth= 1.79"	Depth= 1.7	'9"
--	-------------	------------	-----

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=6.60"

A	rea (sf)	CN	Description		
	416	98	Roofs, HSC	θA	CONTRACTOR OF THE OWNER
	1,513	39	>75% Gras	s cover, Go	bod, HSG A
*	90	98	Wall		
	2,019 1,513 506			verage vious Area pervious Ar	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
6.0					Direct Entry, Min. Standard Engineering Practice

Summary for Subcatchment SC301: Subcatchment 301

Runoff = 0.89 cfs @ 12.10 hrs, Volume= 3,084 cf, Depth=	: 1.79	9"
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Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=6.60" 8 Adams St, Lexington Ma Type III 24-hr 100-Year Design Storm Rainfall=6.60" Printed 5/24/2018 CAD Software Solutions LLC Page 22

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	rea (sf)	CN	Description			
	1,275	98	Roofs, HSC			
	15,334	39			ood, HSG A	
	3,152	98			AY/WALKS	
	947	98	PROPOSE			
	20,708	54	Weighted A			
	15,334		74.05% Pe			
	5,374		25.95% Im	pervious Ar	ea	
Тс	Length	Slope			Description	
(min) 6.0	(feet)	(ft/ft	t) (ft/sec)	(cfs)	Direct Entra	, Min. Standard Engineering Practice
0.0					Direct Entry	, Min. Standard Engineering Practice
		Sum	mary for	Subcatch	ment SC40	1: Subcatchment 401
unoff	=	0.14	cfs @ 12.1	5 hrs, Volu	ume=	875 cf, Depth= 0.76"
unoff b	V SCS TH	R-20 me	ethod, UH=S	SCS. Time	Span= 0.00-7	2.00 hrs, dt= 0.05 hrs
			Design Stori			
, po		, ioui i	beergin eten	in realization	0.00	
A	rea (sf)	CN	Description			
	13,241	39	the second s		ood, HSG A	
	488		PROPOSE			
	13,729	41	Weighted A	verage		
	13,729 13,241		Weighted A 96.45% Per		1	
				vious Area		
Тс	13,241 488		96.45% Pei 3.55% Impe	rvious Area ervious Are	а	
Tc (min)	13,241 488 Length	Slope	96.45% Per 3.55% Impe e Velocity	rvious Area ervious Are Capacity		
Tc (min) 6.0	13,241 488		96.45% Per 3.55% Impe e Velocity	rvious Area ervious Are	a Description	v, Min. Standard Engineering Practice
(min)	13,241 488 Length	Slope (ft/ft	96.45% Per 3.55% Impe e Velocity) (ft/sec)	rvious Area ervious Are Capacity (cfs)	a Description Direct Entry	
(min)	13,241 488 Length	Slope (ft/ft	96.45% Per 3.55% Impe e Velocity) (ft/sec)	rvious Area ervious Are Capacity (cfs)	a Description Direct Entry	v, Min. Standard Engineering Practice 1: Subcatchment 501
<u>(min)</u> 6.0	13,241 488 Length	Slope (ft/ft Sum	96.45% Per 3.55% Impe e Velocity) (ft/sec)	rvious Area ervious Are Capacity (cfs) Subcatch	a Description Direct Entry ment SC50	
<u>(min)</u> 6.0 unoff	13,241 488 Length (feet)	Slope (ft/ft Sum 0.48 c	96.45% Per 3.55% Impe e Velocity) (ft/sec) imary for s	rvious Area ervious Are Capacity (cfs) Subcatch 9 hrs, Volu	a Description Direct Entry ment SC50	1: Subcatchment 501 1,760 cf, Depth= 6.36"
(min) 6.0 unoff unoff b	13,241 488 Length (feet) = y SCS TF	Slope (ft/ft Sum 0.48 c 8-20 me	96.45% Per 3.55% Impe e Velocity) (ft/sec) mary for \$ ofs @ 12.09 ethod, UH=S	rvious Area ervious Are Capacity (cfs) Subcatch 9 hrs, Volu SCS, Time S	a Description Direct Entry ment SC50 ime= Span= 0.00-72	1: Subcatchment 501
(min) 6.0 unoff unoff b	13,241 488 Length (feet) = y SCS TF	Slope (ft/ft Sum 0.48 c 8-20 me	96.45% Per 3.55% Impe e Velocity) (ft/sec) imary for s	rvious Area ervious Are Capacity (cfs) Subcatch 9 hrs, Volu SCS, Time S	a Description Direct Entry ment SC50 ime= Span= 0.00-72	1: Subcatchment 501 1,760 cf, Depth= 6.36"
(min) 6.0 unoff unoff b ype III 2	13,241 488 Length (feet) = y SCS TF 24-hr 100	Slope (ft/ft Sum 0.48 c R-20 me 2-Year [96.45% Per 3.55% Impe e Velocity) (ft/sec) amary for s ofs @ 12.0 ethod, UH=S Design Storr	rvious Area ervious Are Capacity (cfs) Subcatch 9 hrs, Volu SCS, Time S	a Description Direct Entry ment SC50 ime= Span= 0.00-72	1: Subcatchment 501 1,760 cf, Depth= 6.36"
(min) 6.0 unoff unoff b ype III 2	13,241 488 Length (feet) = y SCS TF 24-hr 100 rea (sf)	Slope (ft/ft Sum 0.48 c 20 me 2-Year I CN	96.45% Per 3.55% Impe e Velocity) (ft/sec) amary for s ofs @ 12.0 ethod, UH=S Design Storr Description	vious Area ervious Are Capacity (cfs) Subcatch 9 hrs, Volu GCS, Time S n Rainfall=	a Description Direct Entry ment SC50 ime= Span= 0.00-72	1: Subcatchment 501 1,760 cf, Depth= 6.36"
(min) 6.0 unoff unoff b ype III 2	13,241 488 Length (feet) = y SCS TF 24-hr 100 rea (sf) 3,321	Slope (ft/ft Sum 0.48 c 20 me 2-Year I CN	96.45% Per 3.55% Impe e Velocity) (ft/sec) mary for s ofs @ 12.0 ethod, UH=S Design Storr <u>Description</u> PROPOSEI	vious Area ervious Are Capacity (cfs) Subcatch 9 hrs, Volu CCS, Time S m Rainfall=	a Description Direct Entry ment SC50 ime= Span= 0.00-72 6.60''	1: Subcatchment 501 1,760 cf, Depth= 6.36"
(min) 6.0 cunoff cunoff b ype III 2	13,241 488 Length (feet) = y SCS TF 24-hr 100 rea (sf)	Slope (ft/ft Sum 0.48 c 20 me 2-Year I CN	96.45% Per 3.55% Impe e Velocity) (ft/sec) amary for s ofs @ 12.0 ethod, UH=S Design Storr Description	vious Area ervious Are Capacity (cfs) Subcatch 9 hrs, Volu CCS, Time S m Rainfall=	a Description Direct Entry ment SC50 ime= Span= 0.00-72 6.60''	1: Subcatchment 501 1,760 cf, Depth= 6.36"
(min) 6.0 unoff unoff b ype III 2	13,241 488 Length (feet) = y SCS TF 24-hr 100 rea (sf) 3,321 3,321	Slope (ft/ft Sum 0.48 c 20 me 2-20 me 2-Year I <u>CN 98</u>	96.45% Per 3.55% Impe e Velocity) (ft/sec) amary for s ofs @ 12.0 ethod, UH=S Design Storr <u>Description</u> <u>PROPOSEI</u> 100.00% Im	vious Area crvious Are Capacity (cfs) Subcatch 9 hrs, Volu CCS, Time S m Rainfall= D ROOF pervious A	a Description Direct Entry ment SC50 ume= Span= 0.00-72 6.60"	1: Subcatchment 501 1,760 cf, Depth= 6.36"
(min) 6.0 unoff unoff b ype III 2	13,241 488 Length (feet) = y SCS TF 24-hr 100 rea (sf) 3,321	Slope (ft/ft Sum 0.48 c 20 me 2-Year I CN	96.45% Per 3.55% Impe e Velocity) (ft/sec) amary for s ofs @ 12.0 ethod, UH=S Design Storr <u>Description</u> <u>PROPOSEI</u> 100.00% Im e Velocity	vious Area ervious Are Capacity (cfs) Subcatch 9 hrs, Volu CCS, Time S m Rainfall=	a Description Direct Entry ment SC50 ime= Span= 0.00-72 6.60''	1: Subcatchment 501 1,760 cf, Depth= 6.36"

5875-POST

5875-P	OST		8 Adams St, Lexington Ma Type III 24-hr 100-Year Design Storm Rainfall=6.60"
	ed by Meridia		es Printed 5/24/2018
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Device	Routing	Invert	Outlet Devices
#1	Discarded	239.50'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	/lax=0.04 cf iltration Cor	s @ 13.23 hrs HW=242.77' (Free Discharge) htrols 0.04 cfs)

Summary for Pond PSIS-2: Proposed Subsurface Infiltration System-2

Inflow Area	a =	2,396 sf,100.00% Impervious, Inflow Depth = 6.36" for 100-Year Design Storm event
Inflow	=	0.35 cfs @ 12.09 hrs, Volume= 1,270 cf
Outflow	=	0.03 cfs @ 13.10 hrs, Volume= 1,270 cf, Atten= 92%, Lag= 60.8 min
Discarded	=	0.03 cfs @ 13.10 hrs, Volume= 1,270 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 243.45' @ 13.10 hrs Surf.Area= 263 sf Storage= 532 cf

Plug-Flow detention time= 182.1 min calculated for 1,269 cf (100% of inflow) Center-of-Mass det. time= 182.0 min (925.8 - 743.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	240.00'	254 cf	15.75'W x 16.68'L x 3.50'H Field A
			919 cf Overall - 284 cf Embedded = 635 cf x 40.0% Voids
#2A	240.50'	284 cf	StormTech SC-740 x 6 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 3 rows
		538 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	240.00'	2.410 in/hr Exfiltration over Wetted area	

Discarded OutFlow Max=0.03 cfs @ 13.10 hrs HW=243.45' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Summary for Pond PSIS-3: Proposed Subsurface Infiltration System-3

Inflow Area	a =	18,711 sf, 35.87% Impervious,	Inflow Depth = 2.32" for 100-Year Design Storm event
Inflow	=	1.11 cfs @ 12.10 hrs, Volume=	3,624 cf
Outflow	=	0.07 cfs @ 14.91 hrs, Volume=	3,624 cf, Atten= 94%, Lag= 168.8 min
Discarded	=	0.07 cfs @ 14.91 hrs, Volume=	3,624 cf
Primary	=	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 244.83' @ 14.91 hrs Surf.Area= 928 sf Storage= 1,719 cf

Plug-Flow detention time= 275.8 min calculated for 3,622 cf (100% of inflow) Center-of-Mass det. time= 275.7 min (1,132.7 - 857.0) **5875-POST** Prepared by Meridian Associates 8 Adams St, Lexington Ma Type III 24-hr 100-Year Design Storm Rainfall=6.60" Printed 5/24/2018 D Software Solutions LLC Page 26

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Volume	Invert	Avail.Storage	Storage Description
#1A	242.00'	851 cf	30.00'W x 30.92'L x 3.50'H Field A
			3,246 cf Overall - 1,120 cf Embedded = 2,127 cf x 40.0% Voids
#2A	242.50'	1,120 cf	StormTech SC-740 x 24 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 6 rows
		1,970 cf	Total Available Storage

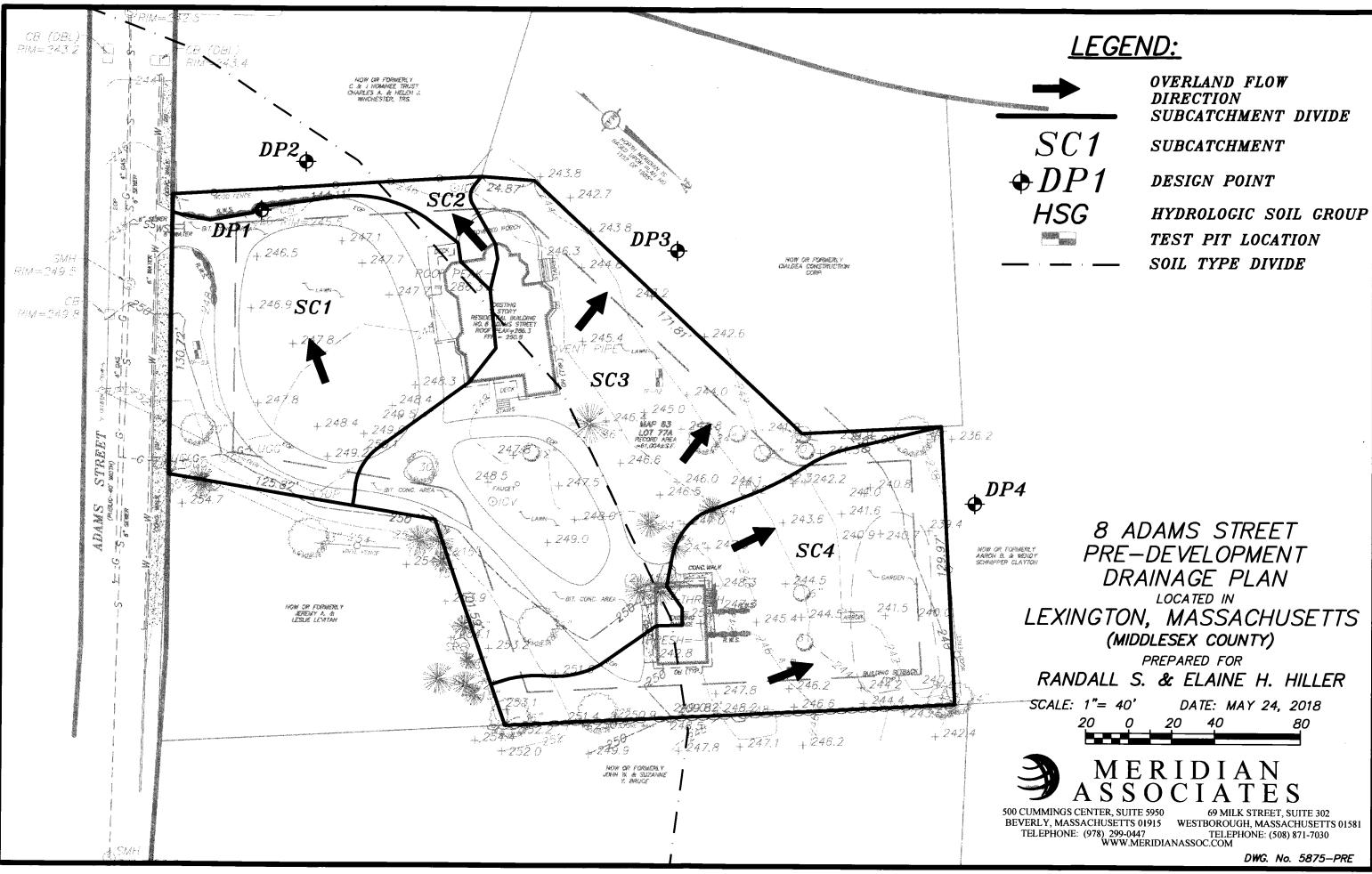
Storage Group A created with Chamber Wizard

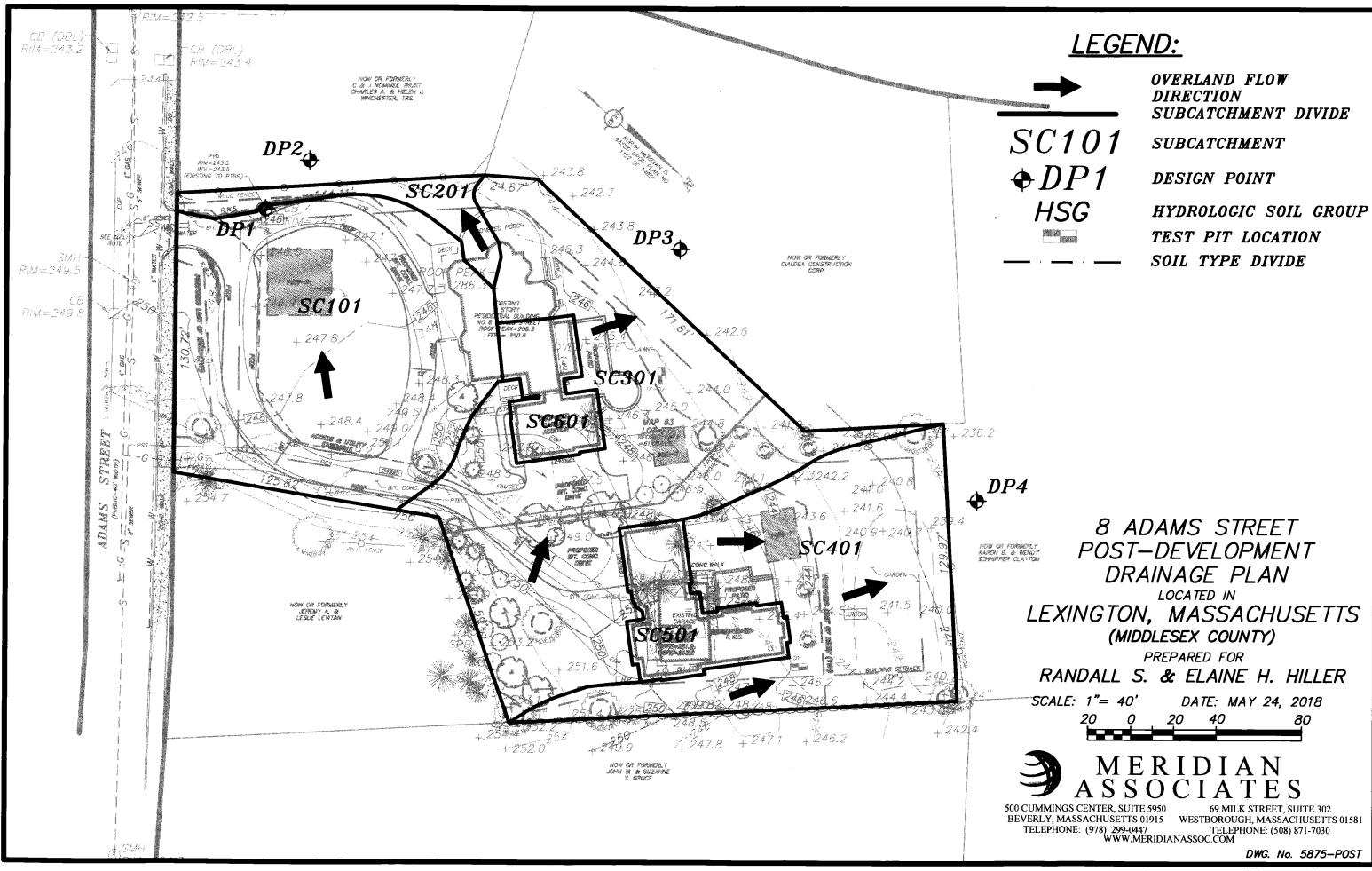
Device	Routing	Invert	Outlet Devices	
#1	Discarded	242.00'	2.410 in/hr Exfiltration over Wetted area	
#2	Primary	245.00'	6.0" Vert. Orifice/Grate C= 0.600	

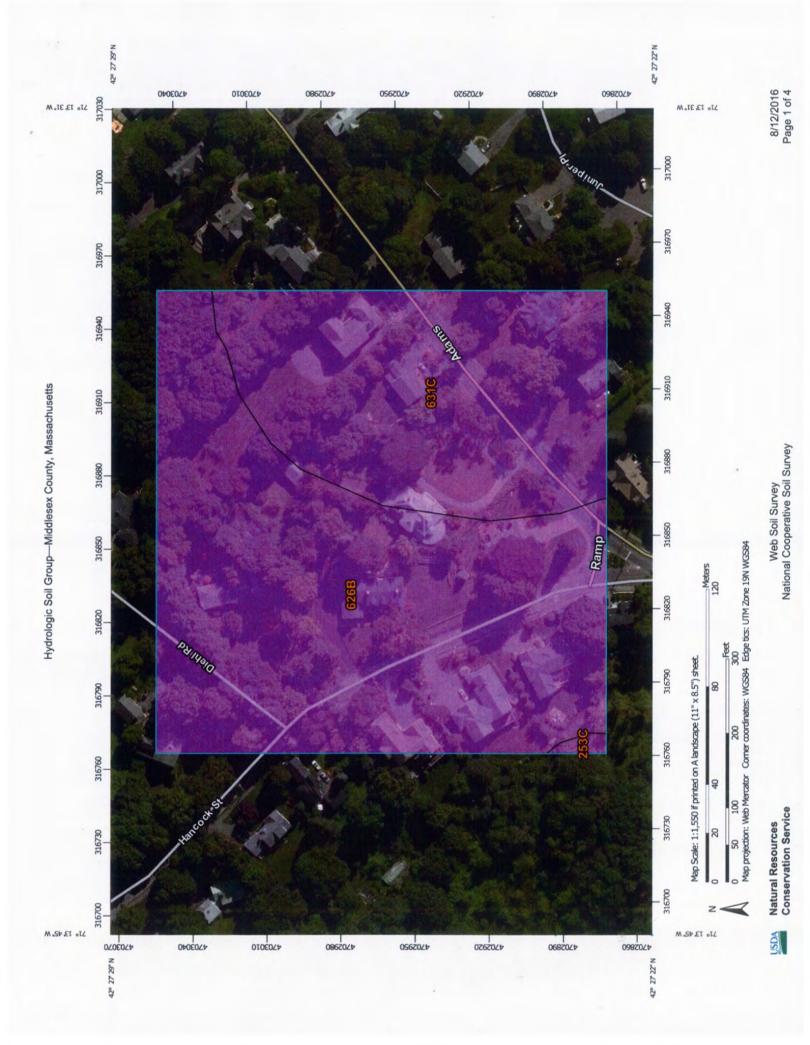
Discarded OutFlow Max=0.07 cfs @ 14.91 hrs HW=244.83' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=242.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)









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Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
253C	Hinckley loamy sand, 8 to 15 percent slopes	A	0.0	0.4%
626B	Merrimac-Urban land complex, 0 to 8 percent slopes	A	5.4	62.8%
631C	Charlton-Urban land- Hollis complex, 3 to 15 percent slopes, rocky	A	3.2	36.8%
Totals for Area of Inter	rest		8.6	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



EROSION AND SEDIMENTATION CONTROL PROGRAM for A PROPOSED STORMWATER MANAGEMENT SYSTEM located at 8 ADAMS STREET LEXINGTON, MASSACHUSETTS



Applicant:

Randall S. & Elaine H. Hiller 8 Adams Street Lexington, Massachusetts 02421

Prepared by:

Meridian Associates, Inc. 500 Cummings Center, Suite 5950 Beverly, Massachusetts 01915 (978) 299-0447

May 24, 2018

Project Name: 8 Adams Street

Owner Name: Randall S. & Elaine H. Hiller

Party Responsible for Maintenance During Construction:

Contractor

Party Responsible for Maintenance After Construction:

Homeowner's Association

Erosion and Sedimentation Control Measures during Construction Activities

Filtermitt (or approved equal)

Filtermitt (or approved equal) will be installed along the down gradient limit of work as depicted on the Site Plan. The FilterMitt shall be installed prior to the commencement of any work on-site and in accordance with the design plans. An additional supply of filtermitt shall be on-site to replace and/or repair any filtermitt that have been disturbed or are in poor condition. The line of FilterMitt shall be inspected and maintained on a weekly basis and after every major storm event (2-year) during construction. No construction activities are to occur beyond the FilterMitt at any time. Deposited sediments shall be removed when the volume of the deposition reaches approximately one-half the height of the filtermitt.

Stockpiles

All unused debris, soil, and other material shall be stockpiled in locations of relatively flat grades, away from any trees identified to be saved and upgradient of the filtermitt. Stockpile side slopes shall not be greater than 2:1. All stockpiles shall be surrounded by a row of filtermitt. Surrounding filtermitt shall be inspected and maintained on a daily basis.

Surface Stabilization

The surface of all disturbed areas shall be stabilized during and after construction. Disturbed areas remaining idle for more than 14 days shall be stabilized. Temporary measures shall be taken during construction to prevent erosion and siltation. No construction sediment shall be allowed to enter any infiltration system or formal drainage system. All disturbed slopes will be stabilized with a permanent vegetative cover. Some or all of the following measures will be utilized on this project as conditions may warrant.

- a. Temporary Seeding
- b. Temporary Mulching
- c. Permanent Seeding
- d. Placement of Sod
- e. Hydroseeding
- f. Placement of Hay
- g. Placement of Jute Netting

Dust shall be controlled at the site.

Tree Protection

Existing trees to be saved shall be protected with orange construction fence (offset from the tree trunk by professional standard based on canopy).

Construction Tracking Pad

A construction tracking pad shall be installed at the designated entrances/exits, as shown on the Site plans, to the site to reduce the amount of sediment transported off site. The construction tracking pad shall be inspected weekly.

Inspection and Maintenance of Area Drain

The performance of the area drain shall be checked after every major storm event during construction.

Subsurface Infiltration Facilities

Construction activity above and around the proposed location of the subsurface infiltration facility shall be limited to prevent compaction of the existing soil. Care shall be taken to redirect stormwater runoff from this area to prevent ponding. Installation of this system shall occur under dry weather conditions and system shall be backfilled immediately to prohibit the introduction of fines or other material that would compromise the functionality of this system.

Removal of Sediment and Erosion Controls

At the completion of construction activities and after receiving approval from the Town of Lexington, all physical sediment and erosion controls shall be removed from the site per Town of Lexington. The areas where the controls have been removed shall be seeded and stabilized immediately upon removal.

Long-Term Inspection and Maintenance Measures after Construction

Erosion Control

Eroded sediments can adversely affect the performance of the stormwater management system. Eroding or barren areas should be immediately re-vegetated.

Subsurface Infiltration Facility

The infiltration system inspections should include inspections following the first several rainfall events or first few months after construction, after all major storms (3.2" inches of rain over a 24-hour period or greater), and on regular bi-annual scheduled dates, to ascertain whether captured runoff drains within 72 hours following the event. Ponded water inside the system (as visible from the observation well) after several dry days often indicates that the bottom of the system is clogged. If the water does not drain, then a qualified professional should be retained to determine the cause of apparent infiltration failure and recommend corrective action. Such corrective action should be immediately implemented by

the homeowner. If depth of sediment is observed to be greater than 3" then the system should be cleaned. The homeowner shall contact a sewer and drain cleaning company to flood the system via pump truck so the water is forced back to the upstream cleanout where sediment can be vacuumed out.

Debris and Litter Removal

Trash may collect in the BMP's, potentially causing clogging of the facilities. All debris and litter shall be removed when necessary, and after each storm event. Sediment and debris collected from vacuuming and/or sweeping should be disposed of at a permitted waste disposal facility. Avoid disposing of this material on site, where it could be washed into the proposed subsurface infiltration systems.

Lawn Mowing

All lawn mowing to take place will be done with a mulch mower so grass clippings will not be an issue.

<u>Good Housekeeping Practices (in accordance with Standard 10 of the Stormwater</u> Management Handbook to prevent illicit discharges)

Provisions for storing paints, cleaners, automotive waste and other potentially hazardous household waste products inside or under cover

- All materials on site will be stored inside in a neat, orderly, manner in their appropriate containers with the original manufacturer's label.
- Only store enough material necessary. Whenever possible, all of a product shall be used up before disposing of container.
- Manufacturer, local, and State recommendations for proper use and disposal shall be followed.

Vehicle washing controls

- A commercial car wash shall be used when possible. Car washes treat and/or recycle water.
- Cars shall be washed on gravel, grass, or other permeable surfaces to allow filtration to occur.
- Use biodegradable soaps.
- A water hose with a nozzle that automatically turns off when left unattended.

Requirements for routine inspection and maintenance of stormwater BMPs

See Inspection and Maintenance Measures after Construction.

Spill prevention and response plans

 Spill Control Practices shall be in conformance with the guidelines set forth in the National Pollutant Discharge Elimination System (NPDES) Stormwater Pollution Prevention Plan (SWPPP)

Provisions for maintenance of lawns, gardens, and other landscaped areas

- Grass shall not be cut shorter than 2 to 3 inches and mulch clipping should be left on lawn as a natural fertilizer.
- Use low volume water approaches such as drip-type or sprinkler systems. Water plants
 only when needed to enhance root growth and avoid runoff problems.
- The use of mulch shall be utilized where possible. Mulch helps retain water and prevents erosion.

Requirements for storage and use of fertilizers, herbicides and pesticides

- Fertilizers used will be applied only in the minimum amounts recommended by the manufacturer. Once applied, fertilizer will be worked into the soil to limit exposure to storm water. Storage will be in a covered shed. The contents of any partially used bags of fertilizer will be transferred to a sealable plastic bin to avoid spills.
- Do not fertilize before a rainstorm.
- · Consider using organic fertilizers. They release nutrients more slowly.
- Pesticides shall be applied on lawns and gardens only when necessary and applied only in the minimum amounts recommended by the manufacturer.

Pet waste management

Scoop up and seal pet wastes in a plastic bag. Dispose of properly, in the garbage.

Provisions for solid waste management

 All solid waste shall be disposed of or recycled in accordance with local town regulations.

Snow disposal and plowing plans relative to Resource Area

- Snow shall be plowed and stored on gravel, grass, or other permeable surfaces to allow filtration to occur.
- Once snow melts all sand salt and debris shall be extracted from surface and properly disposed of.
- Snow shall not be disposed of in any resource area or waterbody.
- Avoid disposing snow on top of storm drain catchbasins or stormwater drainage swale.

Winter Road Salt and/or Sand use and storage restrictions

- Sand storage piles should be located outside the 100-year buffer zone and shall be covered at all times. No salt to be stored or used on site.
- Alternative materials, such as sand or gravel, should be used in especially sensitive areas.

Roadway and Parking Lot sweeping schedule

- Pavement sweeping shall be conducted at a frequency of not less than once per year.
- Removal of any accumulated sand, grit, and debris from driveway after the snow melts shall be completed shortly after snow melts for the season.

Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL

Not Applicable

Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan

To be determined by the owner.

List of Emergency contacts for implementing Long-Term Pollution Prevention Plan

To be determined by the owner.

Applicant's Certification

I certify under penalty of law that I have read, understand and agree to abide by the practices outlined in this document.

Signed:_____ Date:____

Homeowner

Contractor's Certification

I certify under penalty of law that I have read, understand and agree to abide by the practices outlined in this document.

Signed:_____ Date:_____

Contractor

P:\6009_Lexington_Mass Ave_Maple St\ADMIN\Reports\Stormwater\SMR\Operations&Maintenance.doc

STORMWATER MANAGEMENT CONSTRUCTION PHASE

INSPECTION SCHEDULE AND EVALUATION CHECKLIST

PROJECT LOCATION: 8 Adams Street Lexington, MA

WEATHER:

Inspector	Area Inspected	Required Inspection Frequency if BMP	Comments	Recommendation	Follow-up Inspection Required (vec/no)
	FilterMitt	Weekly and After Major Storm Events			(as m)
	Construction Tracking Pad	Weekly and After Major Storm Events			
	Subsurface Infiltration Systems	Weekly and After Major Storm Events			
	Area Drain	Weekly and After Major Storm Events			

- Refer to the Massachusetts Stormwater Handbook, Volume Two: Stormwater Technical Handbook (February 2008) for recommendations regarding frequency for inspection and maintenance of specific BMP's. (1)
 - Inspections to be conducted by a qualified professional such as an environmental scientist or civil engineer. (7)

Limited or no use of sodium chloride salts, fertilizers or pesticides recommended.

Other notes: (Include deviations from: Con. Comm. Order of Conditions, PB Approval, Construction Sequence and Approved Plan) Stormwater Control Manager: STORMWATER MANAGEMENT AFTER CONSTRUCTION

INSPECTION SCHEDULE AND EVALUATION CHECKLIST

PROJECT LOCATION: 8 Adams Street, Lexington, MA

WEATHER:

Inspection Inspector Date	Area Inspected	Required Inspection Frequency if BMP	Comments	Recommendation	Follow-up Inspection Required (ves/no)
	Area Drain	Bi-annually and After Major Storm Events			
	Subsurface Infiltration Systems	Bi-annually and After Major Storm Events			

- Refer to the Massachusetts Stormwater Handbook, Volume Two: Stormwater Technical Handbook (February 2008) for recommendations regarding frequency for inspection and maintenance of specific BMP's. (3)
 - Inspections to be conducted by a qualified professional such as an environmental scientist or civil engineer. (4)

Limited or no use of sodium chloride salts, fertilizers or pesticides recommended.

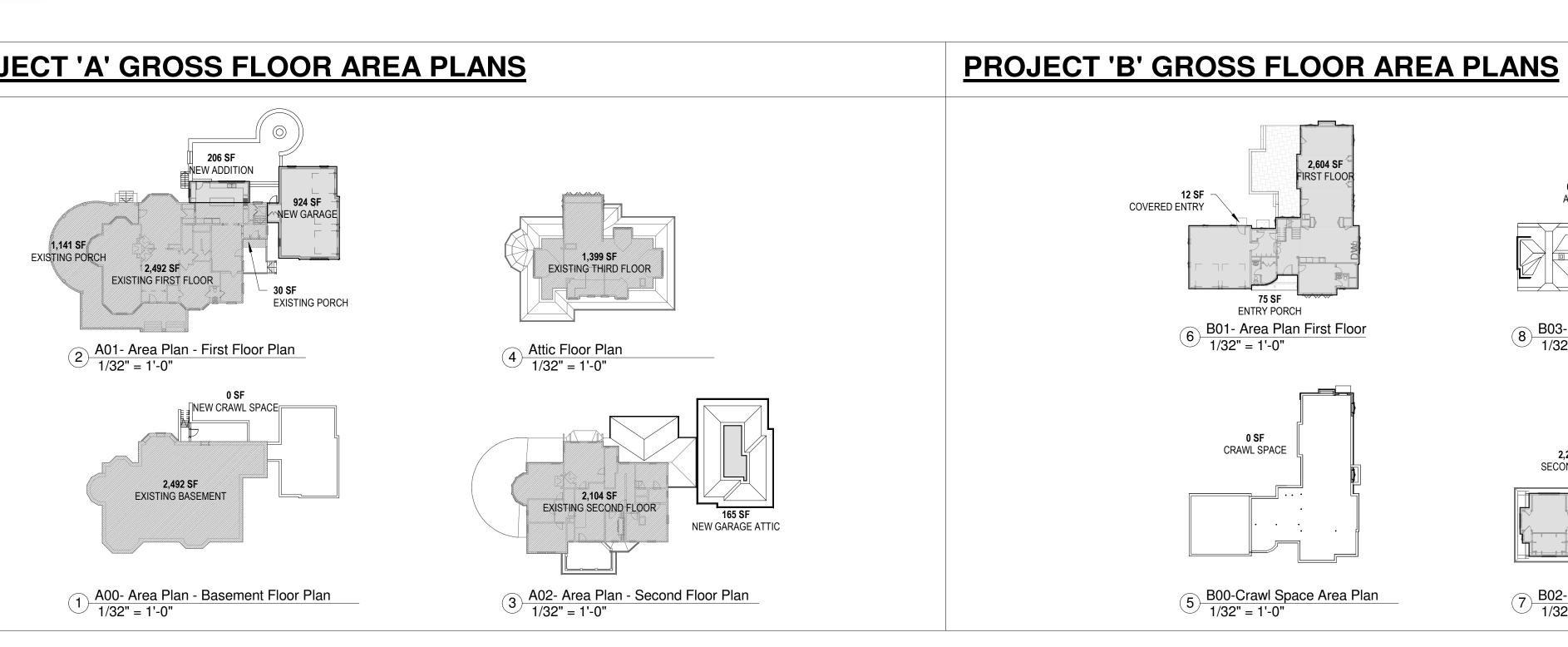
Other notes: (Include deviations from: Con. Comm. Order of Conditions, PB Approval, Construction Sequence and Approved Plan) Stormwater Control Manager:



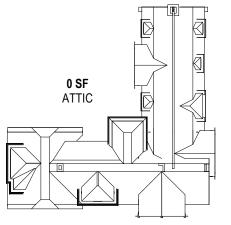
PROJECT AREA CALCULATIONS

|--|

GFA CALCULATIONS	'A' - Existing Hou	use Renovatior	ı
	Existing	Addition	New Total
Lower Level	2,492 SF	0 SF	2,492 SF
Level One	2,492 SF	1,130 SF	3,622 SF
Level Two	2,104 SF	165 SF	2,269 SF
Attic	1,399 SF	0 SF	1,399 SF
Covered Porches	1,171 SF	0 SF	1,171 SF
Subtotal	9,658 SF	1,295 SF	10,953 SF
			Total
Lower Level			0 SF
Level One			2,604 SF
Level Two			2,239 SF
Attic			0 SF
Covered Porches			87 SF
0			4,930 SF
Subtotal			4,950 51



PERSPECTIVE FROM ADAMS STREET



8 B03- Area Plan Attic 1/32" = 1'-0"



1666 Massachusetts Ave. Lexington, MA 02420 781.274.0955 STRUCTURAL ation pplic SE bg Plannir \mathbf{O} SEAL spective er rchitectural Area Plans A w SHEET ISSUED: 5-22-18 SCALE: As indicated DRAWN BY: CJB PROJECT #: 2018-21B SHEET NUMBER A1.0

LEXINGTON PLANNING BOARD

AGENDA ITEM TITLE:

55 & 56 Watertown Street (Belmont Country Club): Planned Development (Public Hearing)

PRESENTER:

<u>ITEM</u> <u>NUMBER:</u>

Steve Senna, National Development

SUMMARY:

The Planning Board will be opening a public hearing to discuss this item. The applicant, National Development (ND Acquisitions LLC), has submitted a proposal to rezone a 17.7 acre site bisected by Watertown Street. The rezone proposes the construction of a 116 unit independent living facility and a 40 unit assisted living facility on the west side of Watertown Street as well as a memory care facility housing 48 residents along the eastside of Watertown. Please click **here** to view plans of the proposal and other submitted documentation.

SUGGESTED MOTION:

FOLLOW-UP:

DATE AND APPROXIMATE TIME ON AGENDA:

7/19/2018

LEXINGTON PLANNING BOARD

ITEM NUMBER:

AGENDA ITEM TITLE:

Comprehensive Plan Update

PRESENTER:

Carol Kowalski

SUMMARY:

This is a standing agenda item to provide updates to the Planning Board on the status of the Comprehensive Plan. Upcoming meetings include the following:

- CPAC Meeting July 24, 2018 (7PM) Location TBD
- CPAC Meeting August 28, 2018 (7PM) Location TBD
- Public Event (World Café) September 25, 2018 (7PM) Battin Hall

SUGGESTED MOTION:

Staff's update requires no action on the part of the Board.

FOLLOW-UP:

DATE AND APPROXIMATE TIME ON AGENDA:

7/19/2018

LEXINGTON PLANNING BOARD

ITEM NUMBER:

AGENDA ITEM TITLE:

Upcoming Meetings & Anticipated Schedule

PRESENTER:

Carol Kowalski

SUMMARY:

This recurring agenda item is to inform the Board and public of the proposed meeting schedule. Upcoming Planning Board meetings are scheduled for the following dates:

- August 16, 2018
- August 30, 2018

SUGGESTED MOTION:

FOLLOW-UP:

DATE AND APPROXIMATE TIME ON AGENDA:

7/19/2018

LEXINGTON PLANNING BOARD

AGENDA ITEM TITLE:

Minutes

PRESENTER:

<u>ITEM</u> <u>NUMBER:</u>

SUMMARY:

Drafts of the following meeting minutes will be reviewed by the Planning Board:

- June 4, 2018
- June 7, 2018
- June 21, 2018

SUGGESTED MOTION:

FOLLOW-UP:

DATE AND APPROXIMATE TIME ON AGENDA:

7/19/2018

ATTACHMENTS:

Description

- **6**-4-18 PB Draft Meeting Minutes
- 6-7-18 PB Draft Meeting Minutes
- 6-21-18 PB Draft Meeting Minutes

Type Backup Material Backup Material Backup Material

PLANNING BOARD MINUTES MEETING OF JUNE 4, 2018

A meeting of the Lexington Planning Board, held in the Battin Hall, in the Cary Memorial Building was called to order at 7:04 p.m. by Chair, Ginna Johnson with members Richard Canale, Charles Hornig, Nancy Corcoran-Ronchetti, and Bob Creech, and planning staff Carol Kowalski, David Kucharsky, and David Fields present.

On a motion duly made and seconded, it was voted 5-0, to adjourn at 8:50 p.m.

Nancy Corcoran-Ronchetti, Clerk

PLANNING BOARD MINUTES MEETING OF JUNE 7, 2018

A meeting of the Lexington Planning Board, held in the Hudson Room, in the Cary Memorial building was called to order at 7:01 p.m. by Vice Chair, Bob Creech with members Richard Canale, Charles Hornig, Nancy Corcoran-Ronchetti, and planning staff Carol Kowalski and David Kucharsky present. Ginna Johnson was absent.

General Updates:

There was a Hartwell Avenue event last week and the Comprehensive Plan kick off was this week.

Hartwell Avenue Zoning Initiative Update:

A zoning consultant was hired and we are awaiting the traffic analysis from Stantec and RKG is doing a fiscal analysis. Are the analysis only looking at existing conditions? Ms. Kowalski said that some future build-out is being done as well. There will be further discussions on this once more information is received.

PUBLIC HEARING

32-40 Hartwell Avenue, special permit:

Vice Chair, Mr. Creech, opened the public hearing for a special permit at 7:10 p.m. with approximately 1 person in the audience. Mr. Dominic Rinaldi of the BSC group was present and gave an explanation of the requested changes for an awning between the two buildings.

Board Comments:

- Believe this meets the requirements which was the hope for connectivity of the two buildings.
- The Board voiced approval for this change.

The public hearing was closed at 7:16 p.m.

The Board requested that staff draft a decision for granting the special permits for the next meeting.

7 Hartwell Avenue, sketch PSDUP:

The Board recommended the applicant go with a zoning change the CM district instead of a new Planned Development District.

On a motion of Mr. Hornig, seconded by Ms. Corcoran-Ronchetti, it was voted, 4-0, to approve the decision drafted by staff.

56 Webb Street, preliminary subdivision plan:

Present was James Decoulos, civil engineer, for Angie Kavlakian the applicant. It came to the Planning Board's attention that clearing has been done on the property and that is not allowed under the subdivision regulations and to contact the Planning Board before doing anything on the site.

Mr. Decoulos gave a summary and submitted papers regarding the history for the title and rights with deeds and plans showing the Trebino's right to convey the use of Dunham Street for access.

Individual Board Questions:

• Is there anything in writing to grant this to the Kavlakian family? *Mr. Decoulous said not explicitly but that does not mean the rights don't exist. We recommend that staff speak with Town Counsel. Our attorney Chris Heep feels we are on solid ground.* Are the Lee's on board with you about this we have a letter from Melissa Lee stating that you do not have those rights? No.

Mr. Decoulos showed the fire safety access off Webb Street at 10 and 20 scale with the Fire Department's largest truck. The applicant would like the Board to have a site visit to show access with a rented private truck to do the test.

Individual Board Questions:

- If this is an emergency vehicle access only, are you asking the Board to waive the dead end street requirement? *Mr. Decoulos said they disagree because alternate vehicle access is being provided. The applicant will seek a waiver to pursue this option as well.* What sort of vehicle will be supported with the access? There needs to be some sort of standard for vehicles under section 7.2 as a subdivision street.
- How will you handle snow removal on the emergency access? It will be removed from the site for the emergency access only with 16 feet wide clearance.

Mr. Decoulos said with the watershed and stormwater plan we agree to not use salt in this area since it discharges into Burlington. We are very aware of the impact to watersheds. There is no evidence of red maple cuts in any resource areas.

- Do you plan to speak with Burlington regarding the threat to the watershed or anything with the wetlands protection act? *We are working with Burlington now on another project. We do not view this as an impact or threat.*
- We have a letter from the Fire Department that does not agree with your assessment of the emergency access which is based on the fire code. *Mr. Decoulos said he would like to see the letter from the Fire Department and would like time to respond to it.*

On a motion of Mr. Hornig, seconded by Ms. Corcoran-Ronchetti, it was voted, 4-0, to deny approval of preliminary subdivision plans for 56 Webb Street as the length of dead end street is longer then permitted in the subdivision regulations the applicant has not clearly demonstrated the right to improve and use the private section of Dunham Street.

On a motion of Mr. Hornig, seconded, by Mr. Creech, it was voted to approve the decision with the additional reason to deny and authorize the acting interim Planning Director to sign on the Board's behalf.

Board Member Updates:

The RFQ is being prepared for a technical person and are doing some outreach for a facilitator for the Special Permit Residential Development Committee and have identified some good people. The Planning Director position closes tomorrow.

Comprehensive Plan Update:

Howard Stein Hudson has been selected and the facilitator for the Comprehensive Plan. Staff is trying to get the trend reports finished and updated to put on the website. The second Economic Development panel will be June 13 in the DPW cafeteria and is the last panel for the Comprehensive Plan. There is currently a vacant seat on the CPAC if there some individuals the Board feel might be a good participants please make sure they contact the planning office.

Board individual comments:

- Pleased with the quality of input for the kick-off event, but not necessarily the number of people who attended. There was also a good mix of people who do not usually participate.
- Give residents and stakeholders a better sense of the actual schedule on what they should be expecting over the next year.
- The materials put together were very good. The participation was very good and so was the feedback.

Upcoming Meetings & Anticipated Schedule:

The Board will be going back to Wednesday night meetings sometime in the near future.

Minutes Review and Approval:

On a motion of Mr. Hornig, seconded by Ms. Corcoran-Ronchetti, it was voted, 4-0, to approve the minutes May 24, 2018, as amended.

On a motion, duly made and seconded, it was voted to adjourn the meeting at 8:05 p.m.

The meeting was recorded by LexMedia.

The following documents used at the meeting can be found on the Planning Board website in Planning Board packets.

- 7 Hartwell Avenue, sketch PSDUP draft decision from staff (1 page).
- Letter from the assistant Fire Chief regarding 56 Webb Street (1 page).
- Draft decision from staff regarding 32-40 Hartwell Avenue (4 pages).
- Plan set for 32-40 Hartwell Avenue, dated April 5, 2018 (5 pages).

Nancy Corcoran-Ronchetti, Clerk

PLANNING BOARD MINUTES MEETING OF JUNE 21, 2018

A meeting of the Lexington Planning Board, held in the Selectmen's Meeting Room, was called to order at 7:01 p.m. by Chair, Ginna Johnson with members Charles Hornig, Nancy Corcoran-Ronchetti, and Bob Creech, and planning staff Carol Kowalski, David Fields, and Lori Kaufman present. Richard Canale was absent.

Hartwell Avenue Zoning Initiative Update:

Ms. Kowalski provided the Board with an update on the Hartwell Avenue Initiative.

We are preparing a contract for the consultant and a calendar for outreach.

245 Woburn Street, ANR:

On a motion of Mr. Hornig, seconded by Ms. Corocran-Ronchetti, it was voted, 4-0, to endorse the ANR plan for 245 Woburn Street.

32 & 40 Hartwell Avenue, Special Permit Decision:

On a motion of Mr. Hornig, seconded by Ms. Corcoran-Ronchetti, it was voted 4-0, to approve the special permits for 32 & 40 Hartwell Avenue in accordance with the decision drafted by staff. CONTINUED PUBLIC HEARING

443 Lincoln Street, Definitive Balanced Housing Development (BHD) special permit:

Ms. Johnson recused herself from this special permit and Mr. Leon, Associate Planning Board Member will sit in her place for this special permit.

Vice Chair, Mr. Creech, opened the continued public hearing at 7:07 p.m. with approximately 35 people in the audience.

Present at the meeting were Jeff Rhuda, applicant, and Rich Harrrington, engineer.

Mr. Rhuda met with the Conservation Commission last week and the public hearing was closed and expect an Order of Conditions next week. We received the letter from the Cambridge Water Department that you requested and additional correspondence from the Engineering Department that all plans are corrected and updated to address all the concerns of staff and we are here to close the public hearing.

Board Comments:

- The plans then are the same as at the last meeting? Yes.
- There were questions from the Cambridge Water Department about the way you would be sewering the facility with pump grinders and pumping it out in instead of a Title 5

system and there were concerns with the stormwater management program. Would the concerns stated by the Cambridge Water District for the stormwater management program be included in the special permit? *Yes the Board could add to special conditions*.

- There was a concern about the pump station design for water consumption and what is the water flow calculation? *Mr. Rhuda said it was based on an approved program from next door development.*
- This will be a condominium and the Board will incorporate the requirements into the documents for the condominium association.

On a motion of Mr. Hornig, seconded by Ms. Corcoran-Ronchetti, it was voted 4-0, close the public hearing at 7:13 p.m.

Staff should draft a decision and the Board will put it on the agenda for July 19 to discuss.

The applicant has requested that the Board vote when there is a full Board, which will be July 19.

287 Waltham Street, Sketch Site Sensitive Development (SSD):

Present was Gary Larson, landscape architect, John Farrington, attorney and Iqbal Quadir the applicant.

Mr. Farrington presented a preview of the plan and discussed the access easement that is registered in Land Court and the historic house on the property. This is an 11 unit SSD with 10 new units and keep the existing historic house on the property and which has only a fraction of what would be allowed for GFA of a conventional subdivision. The applicant is not a developer and would own the site.

Mr. Larson said this site is made up of four parcels with 3 existing homes. The proof plan shows an 11 lot subdivision. Emergency access would be provided to Bushnell Drive and many trees will be retained and the units would be from 2,600 to 2,700 square feet to allow for downsizing for Lexington residents who want to age in the community.

Board Comments:

- Is there a reason you would not do a BHD this doesn't seem like a SSD.
- Want more information on the easement. *Mr. Farrington said that all the land is registered land and the easement information exists and is clear.* What is the width of the easement? *It varies at one point 10-12 feet and other points 20 feet wide.*
- The access on Waltham Street is a concern with traffic sight line and vehicles entering and leaving.
- There is open space only because the space is not a good place to build houses.

- Do you really need to build the 4 houses on the northeast corner? *In order to build the road the reality is I need to spend more money and building those houses makes sense.*
- There is no wetlands on this site but there is everything else. Concern was expressed that the blasting that would obliterate the existing landscape. Pulling out of the drive the sight line is problematic.

Public Comments:

- Concerned with flooding and runoff flooding for the houses down below.
- A 2,500 square foot home seems large for downsizing.
- Concerned with traffic access on Waltham Street.
- What provision would be made for the existing wildlife?
- Are these four story houses or will the footprint grow? *This includes gross floor area* (*GFA*).
- The plans that were sent to residents will those buildings be towering over the existing houses.
- After a large rainstorm there is a lake formed on the property and neighbors have water in the basement and blasting may cause more problems. *The bylaws require that no additional runoff come off the site*.
- There is so much traffic where the houses are being proposed and trying to get in and out of the site not sure how much backing up will happen if someone wants to make a left turn. Has a traffic study been done?
- Can anything be stipulated that families cannot move in? *That is not allowed by fair housing practices*.
- Concerned with safety for the increased traffic.
- Questions were asked about the suitability of the lot. Looking at the site topography this does not appear suitable for a SSD. The easement said that it is a driveway and not a road and this is a concern. *The buildability of the lot was not in question*.
- Water does flow downhill and bedrock does not percolate well. The bottom part of Wachusett Drive has a boulder and there must be a reason it was placed there.
- There was destruction of another house from blasting that will be a concern.
- This will be a common driveway and the emergency access has a hairpin drive how can the fire truck make that turn. *Right now the fire truck cannot reach our home at this point and that is a concern.* Is it necessary for you to build 10 units to obtain a driveway?

- Page 4
 - As a senior we do not want a two-story home with stairs and 2600 square feet seems large and not suitable for seniors.
 - The road proposed from Waltham Street what is the length and slope of that street. 600 feet and the grade is designed with the steepest part at 10% and in the special permit the grade can be up to 12%.
 - Is this driveway going to be private, who will be responsible for it? *It will be a common driveway and maintained by the association.*
 - There are a lot of springs in that area and the land is not so stable and blasting this area how are residents going to be protected from damage.
 - Concerned with the streets incline and going up and down the road especially in the winter.
 - This is exactly the kind of project looking for older seniors and hope it gets support.

Planning Board Comments:

- Would like to see the lot.
- Look forward to getting the information on the easement from Mr. Farrington. Have concerns that are shared with the residents and want some kind of write-off from the fire department regarding blasting.
- The design for this site is better for a public benefit development.
- Location of driveway is an issue regarding the existing height of the stone wall on Waltham Street, access and emergency access is problematic, this will destroy the historic landscape, blasting is a major concern. 10 Bushnell Drive will have four units that will not appreciate having him in the back yard especially regarding privacy and concern about wildlife.
- No way this should be a SSD with the impacts this would have on the site. On the lower portion there is question on the size of the units. When additional units are added need to keep up with the 10% affordable units. There is no benefit to the Town with this project.
- Mark the trees that will be removed you will be surprised how many would be removed. The applicant requested that the Planning Board visit the site.

114 Wood Street, Sketch Site Sensitive Development:

Mr. Angelo Tortulo, the applicant and Mr. Novak, Meridian Associates were present for 114 Wood Street. Mr. Novak gave a preview of the site project the proof plan, access to the lots, addressed the Eversource easement, resource areas, and explained that the wetlands that have been flagged. We are working to get a letter regarding the easement from Eversource.

Individual Board Comments:

- Why are the two new houses located so far back? *This is only a first pass and wanted input*. They should be brought in closer to the existing house. Be better if they were pulled up to get further away from the houses across the street.
- Need a letter from Eversource that this can be done since it is so close to the structure.
- You could build closer to the easement but even though near conservation land this could improve the site significantly. Pull the development as close to Wood Street as possible and anything you do to that land would be an improvement. If doing a SSD make it worth our while give us something that will be a big improvement.
- Encourage you not to go within the 100 foot buffer of the resource area.
- If the applicant has items on other people's property they need to remove all improvements, landscape, and pavement to their own property.
- What are you preserving here to make it a SSD, access and the drive are problematic it has a way to go.
- Has your research found who was the owner of that gore? *No we have taken an extensive look and have not found anything yet.*
- Just build one house and move closer to Wood Street and preserve the environment.

Audience Comments:

- Will they connect to Beaumont Street and will they be condos? *No all will be single family homes and will not connect to Beaumont Street.*
- Concern about a high water table level and a stream running through my property and any additional building will have more water running though my property.
- Concerned about the existing wildlife in that area.
- What would happen with the vegetation there right now? What will we end up with?
- Concern that this will ruin the entire landscape, blasting where the powerlines are near my house and am worried will have more water in my basement. This will ruin the entire landscape go down and see the site.
- There was concern at the bottom of Amherst Street for a vernal pool Cooks Pond which is protected by the National Park. The resident read a letter from the National park and they are waiting for certification of the vernal pool and the development needs to move away from the vernal pool and this project needs to be done right to minimize the impact on the vernal pool.

• Across from us surveyors have marked trees with pink tape. Does that mean those trees are being marked for removal? *Nothing has been designated for the removal at this time. Pink ribbon is generally used as a benchmark.*

Individual Board Comments:

- Please provide a copy of the letter regarding the vernal pool.
- The hill on Amherst Street will not be removed. *Correct*.
- Need more site analysis, what is being preserved, tree loss, removal of property that is over the property line. Believe the pavement extends over the property line south of the existing house that is in question. *Mr. Novak will look into that*.

The owner Angelo Turtola said he owns two properties and love what they have and would like to build a one-story house to age in place. The powerlines are our neighbors one day there was a fire next to my house right under the powerline and was caused by a powerline surge. The wildlife is an important part of our lives and want one small house to age in place there will be no blasting since it is sand. There has been a perennial problem with water in the basements.

Comprehensive Plan Update:

Ms. Kowalski gave an update regarding the comprehensive plan activity work schedule for June through August.

Upcoming Meetings & Anticipated Meetings:

The Board discussed the upcoming schedule through the 2019 Annual Town Meeting. On a motion, duly made and seconded, it was voted to adjourn the meeting at 9:52 p.m.

The meeting was recorded by LexMedia.

The following documents used at the meeting can be found on the Planning Board website in Planning Board packets.

- Project Narrative from the applicant regarding 114 Wood Street (2 pages).
- Project Plan set for 114 Wood Street (6 pages).
- Staff report regarding 114 Wood Street (4 pages).
- Letter from Meridian regarding 114 Wood Street (2 pages).
- Project Plan set for 287 Waltham Street (5 pages).
- Staff report regarding 287 Waltham Street (5 pages).
- Revised Plan set for 443 Lincoln Street balanced housing development (Homes at Hobbs Brook), dated 5/30/18 (11 pages).

- Letter dated May 30, 2018 from Stamski and McNary regarding the updated plans for 443 Lincoln Avenue (2 pages).
- Eversource Energy letter regarding established easement for 443 Lincoln Street (2 pages).
- Homes at Hobbs Brook, Project narrative 443 Lincoln Street (36 pages).
- Sewer layout regarding 443 Lincoln Street (1 page).
- E/One pressure sewer design report regarding 443 Lincoln Street (14 pages).
- E/One pressure sewer preliminary cost and design analysis report regarding 443 Lincoln Street (4 pages).
- Responses to comments from Stamski & McNary regarding 443 Lincoln Street, Homes at Hobbs Brook (8 pages).
- Updated landscape Plan for 443 Lincoln Street, Homes at Hobbs Brook (1 page).
- Water supply details for 443 Lincoln Street, Homes at Hobbs Brook (1 page).
- Plan of land ANR 285 Woburn Street.

Nancy Corcoran-Ronchetti, Clerk