### **AGENDA**

### **Lexington Planning Board**

Thursday, May 24, 2018 Hudson Room, Cary Memorial Building, 1605 Massachusetts Avenue 7:00 PM

### **Staff Reports**

- 1. General Update (as needed)
- 2. Hartwell Avenue Zoning Initiative Update

### **Development Administration**

- 1. Balanced Housing Development Special Permit Application: 443 Lincoln Street
- 2. 56 Webb Street: Preliminary Plan
- 3. PSDUP Sketch Decision: 7 Hartwell Avenue

### **Board Administration**

- 1. Board Member Updates
- 2. Comprehensive Plan Update
- 3. Upcoming Meetings & Anticipated Schedule
- 4. Minutes

### Adjourn



Meeting broadcast by LexMedia

### **AGENDA ITEM SUMMARY**

### LEXINGTON PLANNING BOARD

<b>AGENDA</b>	ITEM	TITL	E:
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General Update (as needed)

PRESENTER:

ITEM
NUMBER:

Aaron Henry

### **SUMMARY:**

The general update is a standing agenda item providing the Planning Office staff the opportunity to update the community and Board on day-to-day matters.

### **SUGGESTED MOTION:**

Staff's update requires no action on the part of the Board.

### **FOLLOW-UP:**

### **DATE AND APPROXIMATE TIME ON AGENDA:**

5/24/2018

### **AGENDA ITEM SUMMARY**

### LEXINGTON PLANNING BOARD

### **AGENDA ITEM TITLE:**

Hartwell Avenue Zoning Initiative Update

PRESENTER:

Melisa Tintocalis, Economic

ITEM

NUMBER:

**SUMMARY:** 

Development Director

Economic Development Director will provide an update to the Planning Board. A joint Planning Board/Board of Selectmen meeting to discuss the Hartwell Zoning Initiative is scheduled for Wednesday, May 30th (7PM) in Battin Hall, Cary Memorial Building.

### **SUGGESTED MOTION:**

### **FOLLOW-UP:**

### **DATE AND APPROXIMATE TIME ON AGENDA:**

5/24/2018

### **AGENDA ITEM SUMMARY**

### LEXINGTON PLANNING BOARD

### **AGENDA ITEM TITLE:**

Balanced Housing Development Special Permit Application: 443 Lincoln Street

PRESENTER:

NUMBER:

### **SUMMARY:**

In addition to documents submitted by the applicant, backup materials include previously submitted review memos from Planning & Engineering staff.

### **SUGGESTED MOTION:**

### **FOLLOW-UP:**

### **DATE AND APPROXIMATE TIME ON AGENDA:**

5/24/2018

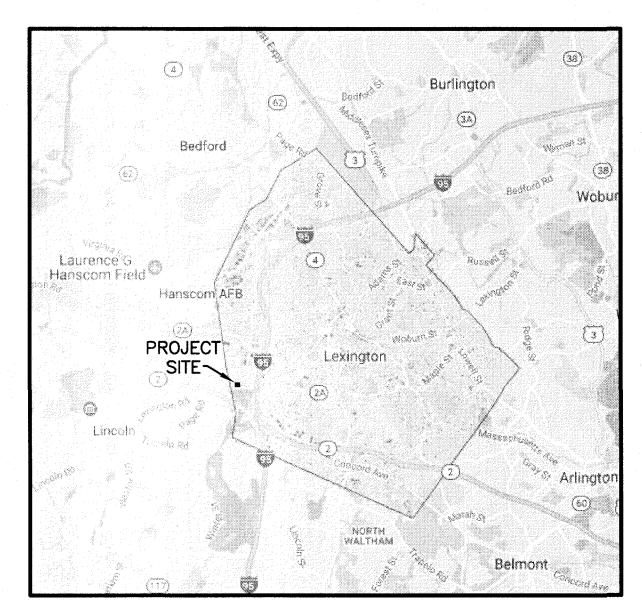
### **ATTACHMENTS:**

	Description	Type
D	Plan Set	Backup Material
D	Landscape Plan	Backup Material
D	Eversource Consent Letter	Backup Material
D	Project Narrative and Landscape Maintenance Plan Backup Ma	
D	Stormwater Packet	Backup Material
D	Planning Staff Memo Backup Ma	
D	Engineering Division Memo Backu	
D	Sewer Layout	Backup Material
D	Sewer Design Report	Backup Material

D	Sewer Hydraulic Report	Backup Material
D	05/16/2018 Response to Comments	Backup Material
D	NOI Timeline	Backup Material
D	Plans Updated 05/17/2018	Backup Material
	Landscape Plan Updated 05/17/2018	Backup Material
D	Water Supply Detail	Backup Material

### HOMES AT HOBBS BROOK

DEFINITIVE PLAN
BALANCED HOUSING RESIDENTIAL DEVELOPMENT
443 LINCOLN STREET
LEXINGTON, MASSACHUSETTS
FEBRUARY 20, 2018



TOWN LOCUS

SCALE: 1"=10,000"

### SHEET INDEX

SHEET 1 TITLE SHEET

SHEET 2 SITE ANALYSIS MAP

SHEET 3 PROPERTY RIGHTS PLAN OF LAND

SHEET 4 SITE CONSTRUCTION PLAN

SHEET 5 PLAN AND PROFILE

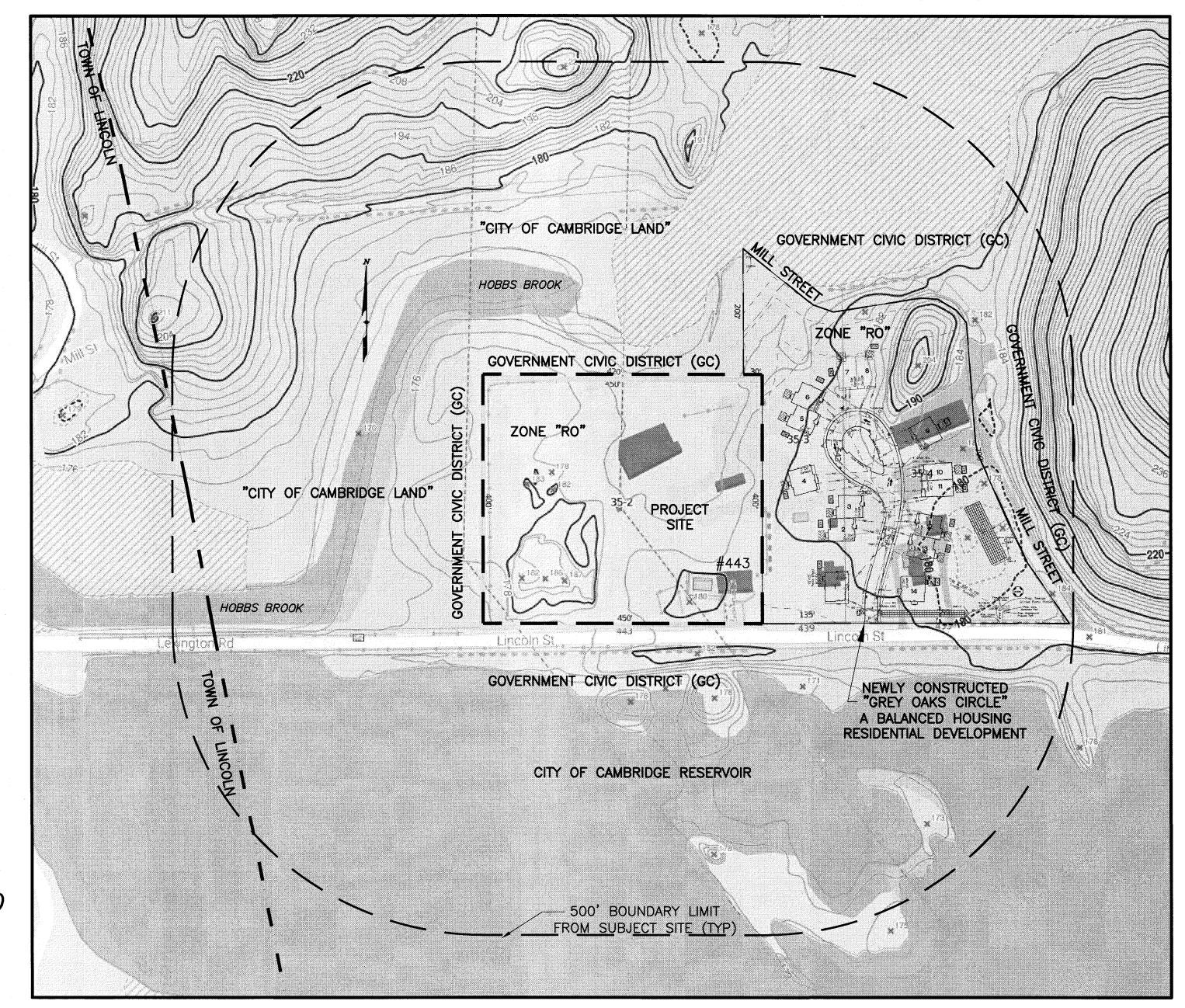
SHEET 6 UTILITY PLAN

SHEET 7 LANDSCAPE PLAN

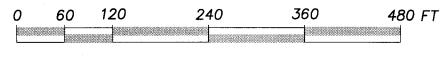
SHEET 8 CONVENTIONAL SUBDIVISION PROOF PLAN

SHEET 9-10 CONSTRUCTION DETAILS

SHEET 11 EROSION AND SEDIMENT CONSTROL PLAN



### LOCUS MAP SCALE: 1"=120"



### **APPLICANT**

SYMES DEVELOPMENT & PERMITTING, LLC 50 DODGE STREET BEVERLY, MA 01915

### LANDSCAPE ARCHITECT

JAMES EMMANUEL, ASSOCIATES 22 CARLTON ROAD MARBLEHEAD, MA 01945

### SURVEYOR/ENGINEER

STAMSKI AND MCNARY, INC. 1000 MAIN STREET ACTON, MA 01720

### **ATTORNEY**

LATHAM LAW OFFICES, LLC 643 MAIN STREET READING, MA 01867-3096

### RECORD OWNER

THE GERTRUDE M. PIANTEDOSI TRUST 443 LINCOLN STREET LEXINGTON, MA

### REFERENCE

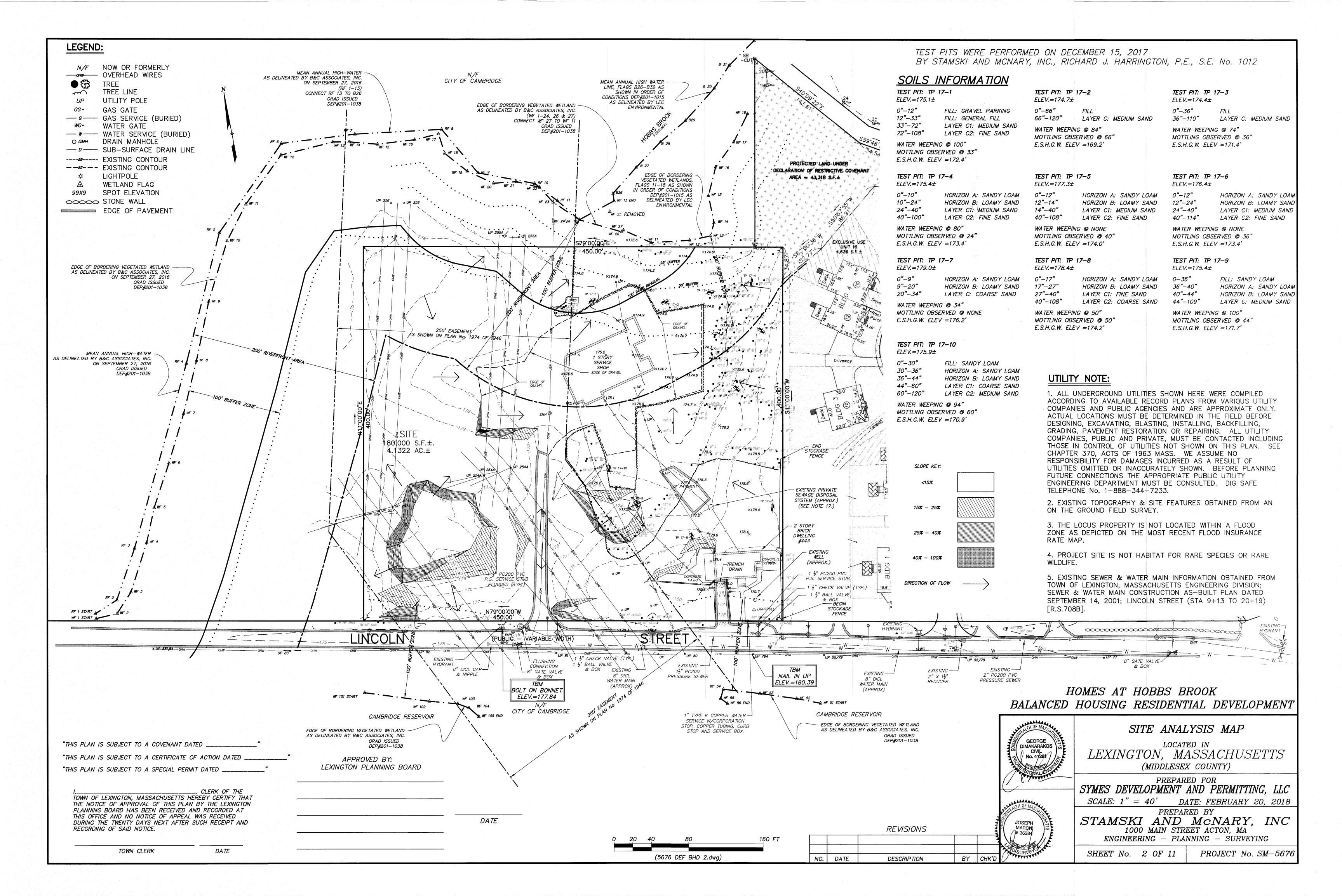
MIDDLESEX REGISTRY OF DEEDS SOUTH DISTRICT DEED BOOK 65347 PAGE 366 PLAN BOOK 239 PLAN 26 ASSESSOR'S MAP 35 PARCEL 2

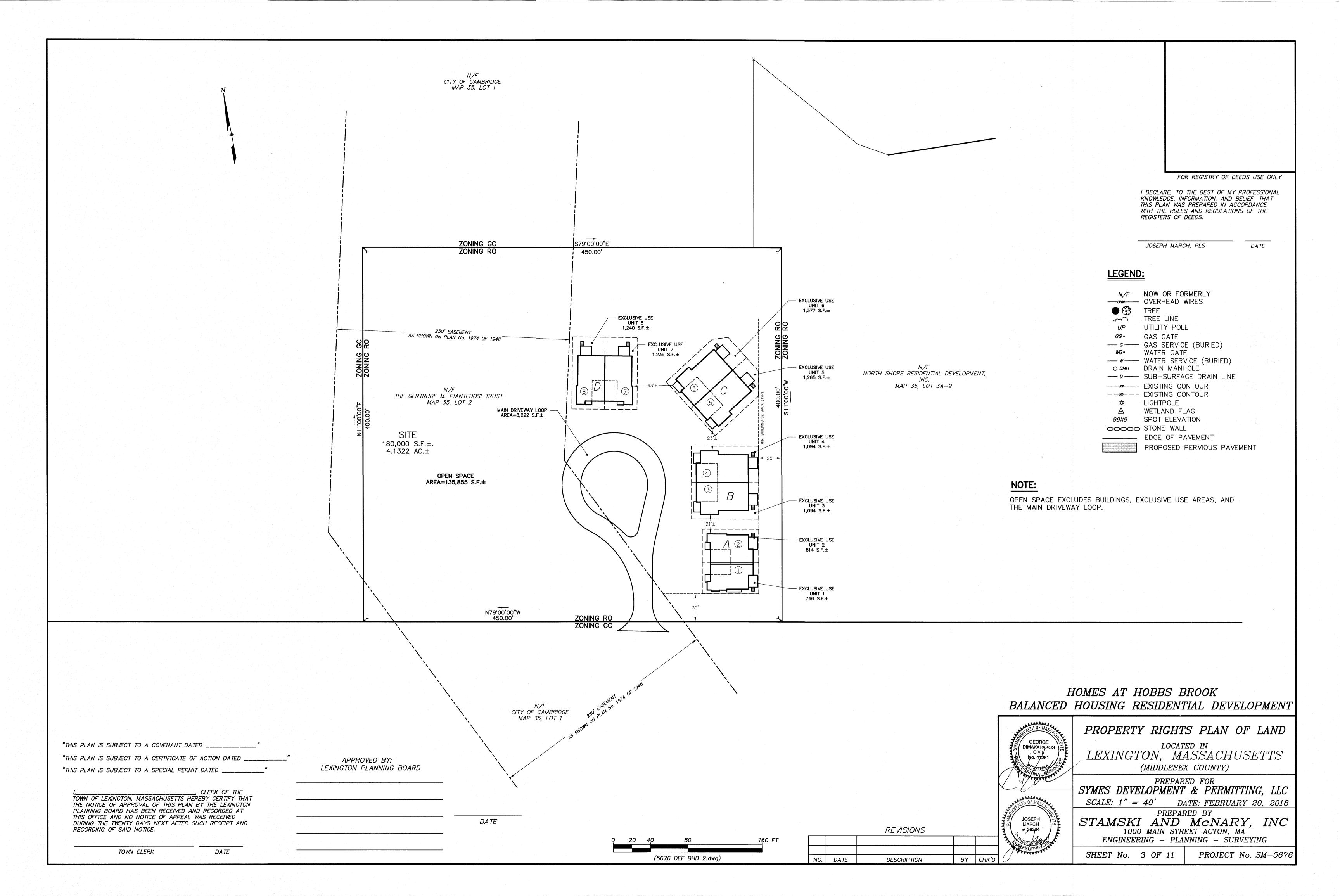
### ZONING DISTRICT

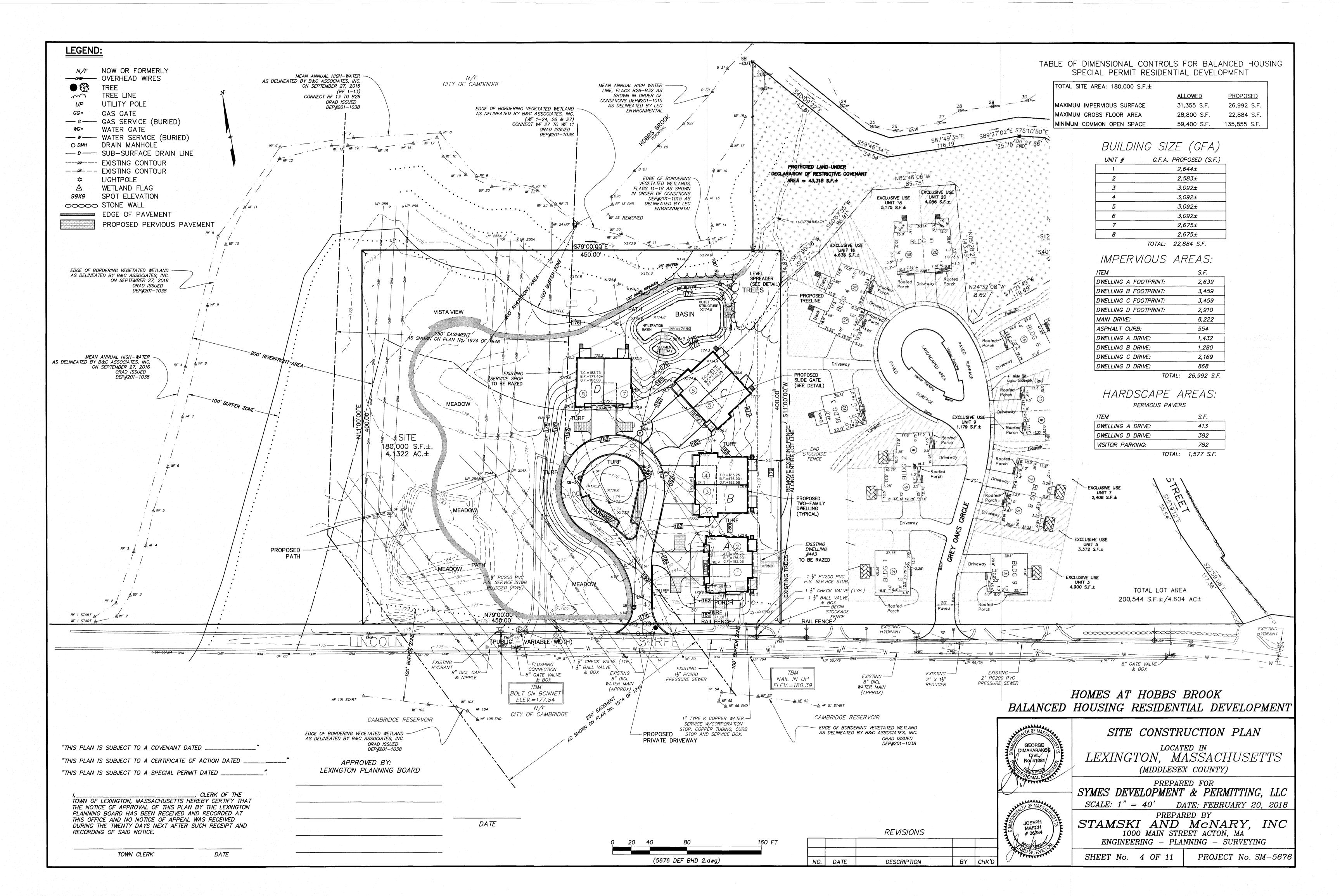
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### DATUM

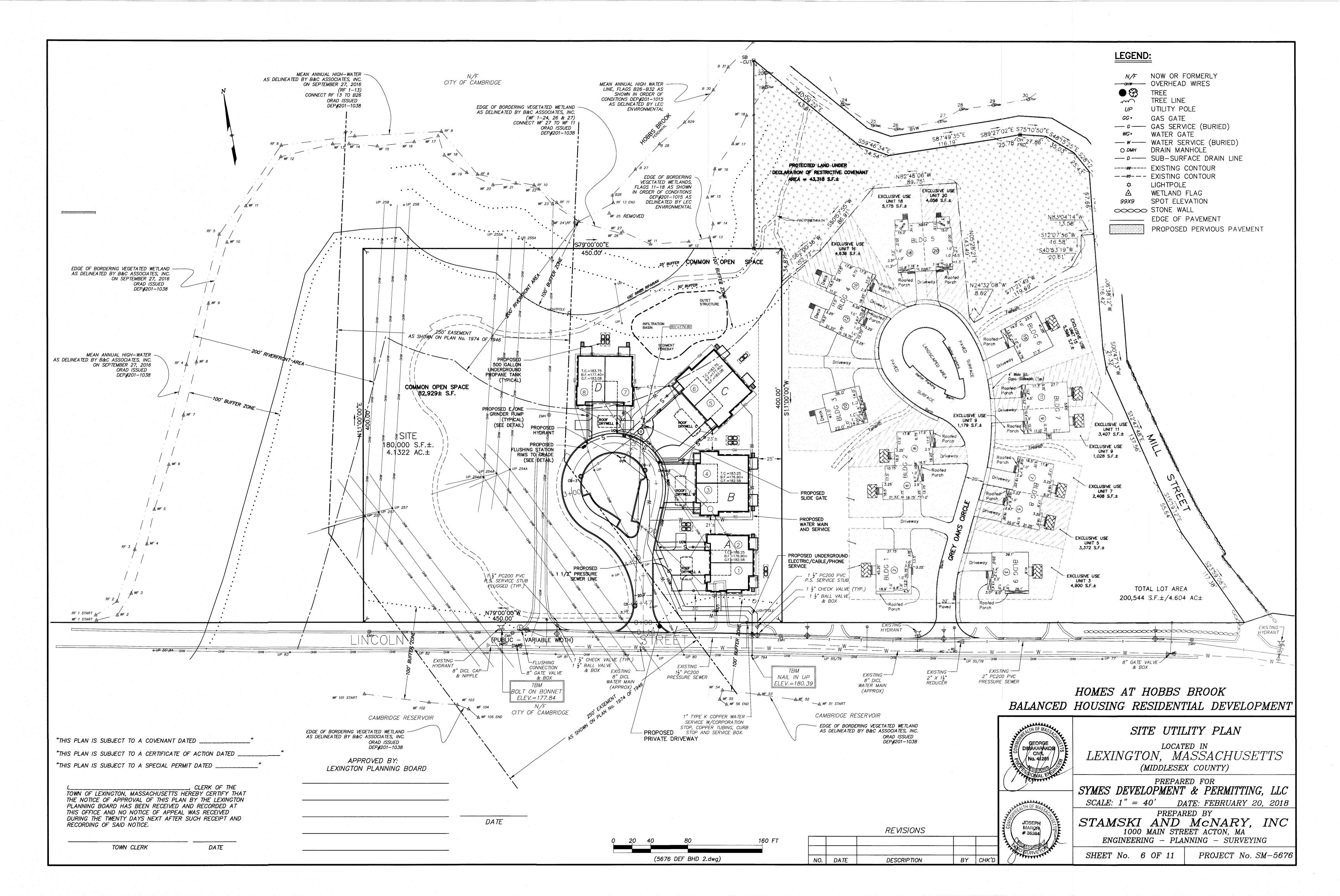
N.G.V.D. OF 1929

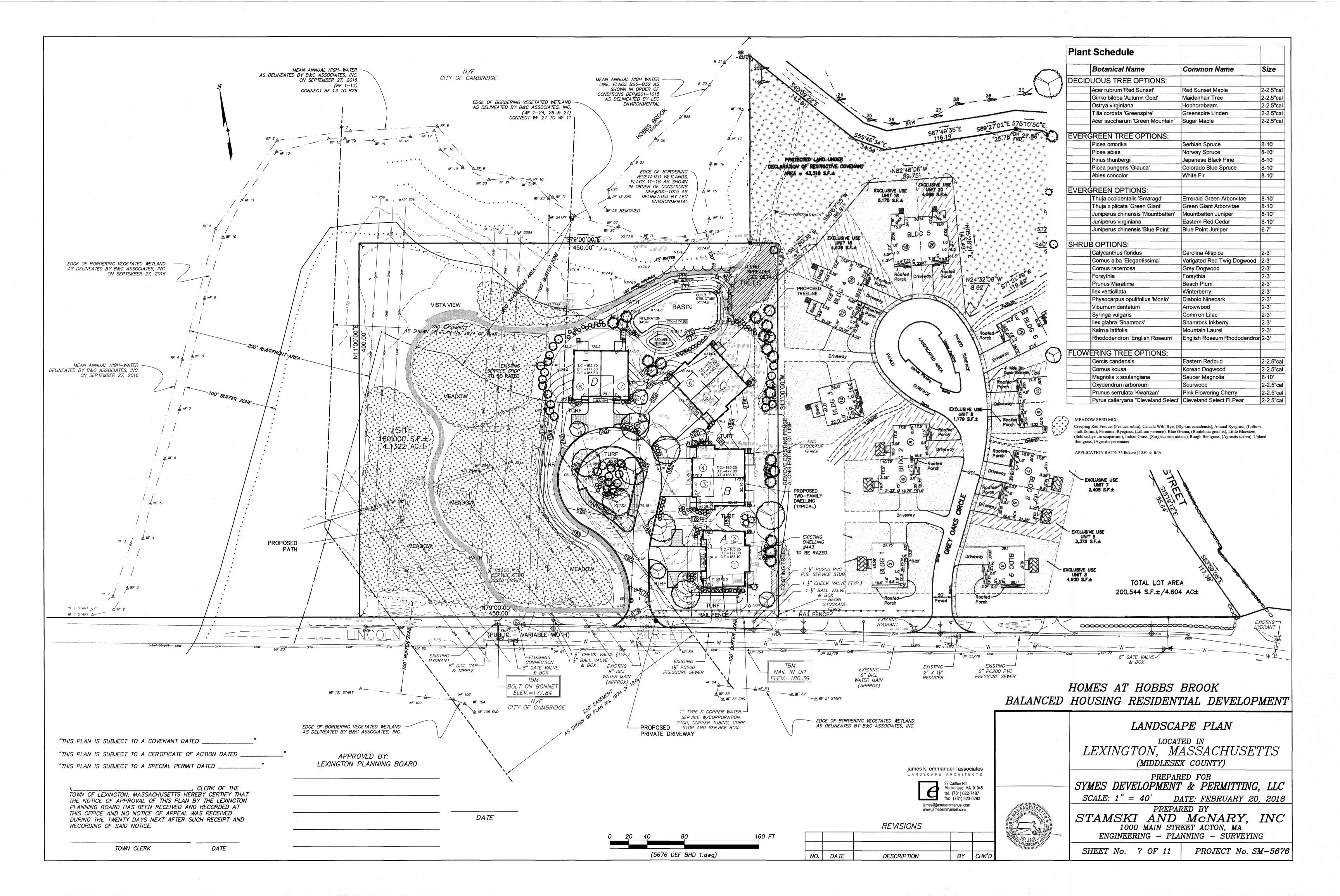


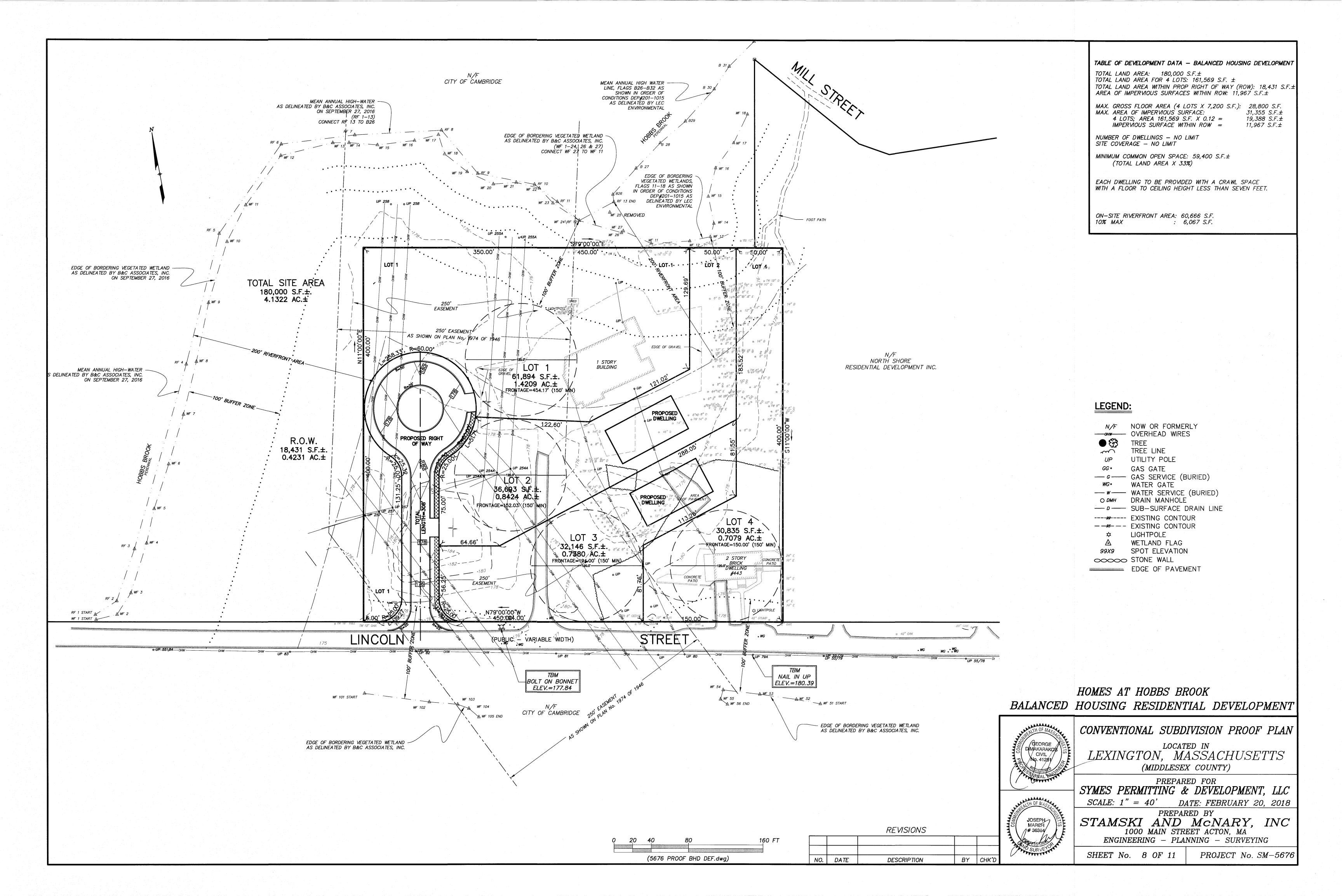


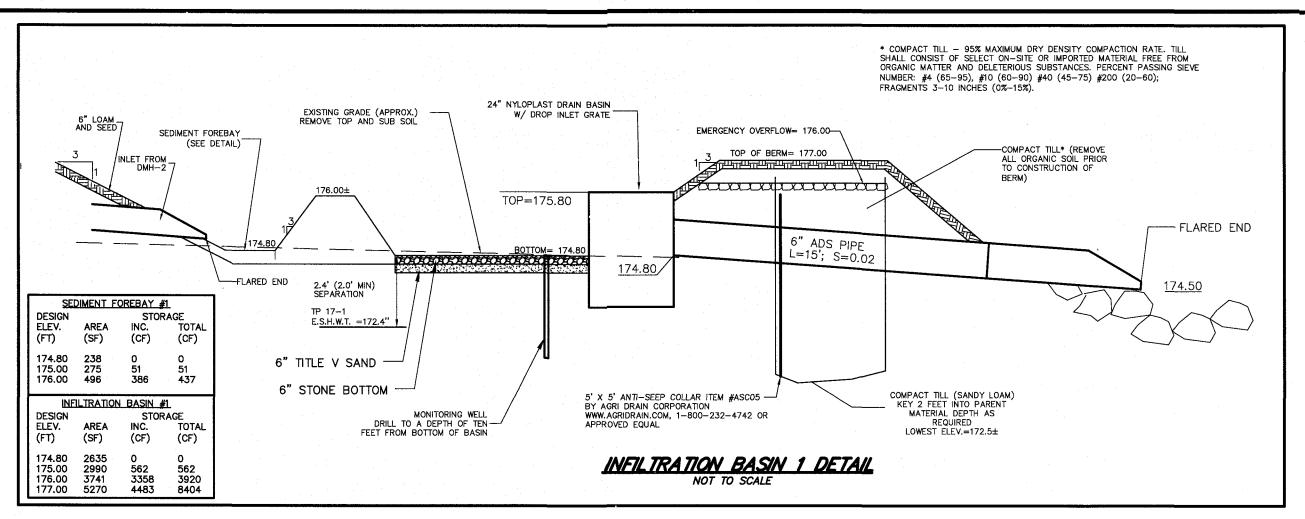


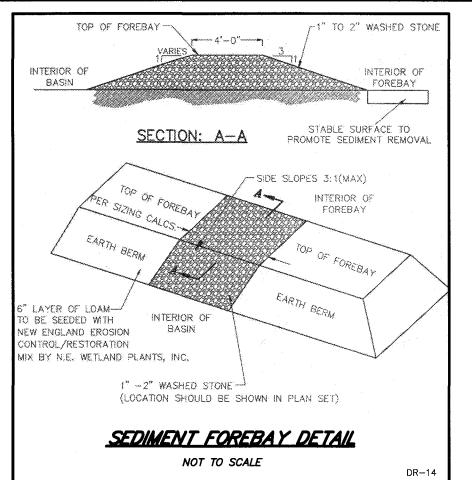
AVERAGE EXISTING GRADE CALCULATION/BUILDING HEIGHT	SITE CONSTRUCTION PLAN	<u>LEGEND:</u>
		N/F NOW OR FORMERLY
UNIT EXISTING GRADE ELEVATIONS AT BUILDING CORNERS AVERAGE EXISTING RIDGE HEIGHT  1 2 3 4 GRADE  EXISTING GRADE	UNIT FFE T.C. G.F. B.F.	TREE LINE
1     181.4     179.9     179.7     179.6     180.15     217.43     37.28	1 184.33 183.25 182.58 176.90*	UP UTILITY POLE  GG GAS GATE  GG GAS SERVICE (BURIED)
2 181.4 179.9 178.4 178.2 179.48 217.43 37.96	2 184.33 183.25 182.58 176.90*	ip 255A in the 255
3     176.3     178.6     178.4     177.0     177.58     213.60     36.03	3 184.33 183.25 182.58 176.90*	450.00 ·
4 176.3 178.6 178.5 175.9 177.33 213.60 36.28	4 184.33 183.25 182.58 176.90*	
5         174.7         175.6         177.7         174.2         176.05         214.10         38.05	5 184.83 183.75 183.08 177.40*	OUTET STRICTURE STRUCTURE 99X9 SPOT ELEVATION
6 174.7 175.6 174.3 174.6 174.80 214.10 39.30	6 184.83 183.75 183.08 177.40*	EDGE OF PAVEMENT
7 175.1 175.2 175.1 174.9 175.08 214.68 39.61	7 184.83 183.75 183.08 177.40*	AS SHOWN ON PLAN No. 1974 OF 1946
8         175.1         175.2         175.4         175.4         175.28         214.68         39.41	8 184.83 183.75 183.08 177.40* * CRAWL SPACE - MAX HEIGHT = 6'-8"**	SEDIMENT FOREBAY
	** MEASURED FROM BOTTOM JOIST TO BASEMENT FLOOR	PROPOSED E/ONE — PROP 12" ADS N-12
"THIS PLAN IS SUBJECT TO A COVENANT DATED"		(SEE DETAIL)  (SEE DETAIL)  (SEE DETAIL)  (SEE DETAIL)
	ROVED BY: I PLANNING BOARD	PROPOSED PROPOSED RIMS TO GRADE ROOF ROOF ROOF ROOF ROOF ROOF ROOF ROO
		(SEE DETAIL)    SEE DETAIL)   B2.30   DRYWELL C   SEE DETAIL)   B2.30   DRYWELL C   SEE DETAIL)   ROO 000 S.F.±.   PROP 12" ADS N-12   L=76', S=0.017
TOWN OF LEXINGTON, MASSACHUSETTS HEREBY CERTIFY THAT THE NOTICE OF APPROVAL OF THIS PLAN BY THE LEXINGTON PLANNING BOARD HAS BEEN RECEIVED AND RECORDED AT		4.1322 AC.±  L=175.08', R=46.00'  L=175.08', R=46.00'  L=175.08', R=46.00'  L=175.08', R=46.00'  L=175.08', R=46.00'
THIS OFFICE AND NO NOTICE OF APPEAL WAS RECEIVED  DURING THE TWENTY DAYS NEXT AFTER SUCH RECEIPT AND  RECORDING OF SAID NOTICE.	DATE	Δ=218°04'42" T=133.30  UP 2544  (B-3)  (B-3
TOWN CLERK DATE		ROOFI 3 B 181.40 PROPOSED WATER
		MAIN AND SERVICE    N23'56'25"   F 21'
		43.43' Δ=12'56'25" T=12.93
		T.C.=183.25   PROPOSED UNDERGROUND   B.F.=176.90+   G.F.=182.58   SERVICE   SERVICE   SERVICE   SERVICE   SERVICE   C.F.=182.58   SERVICE   C.F.=182.58
		Δ=62°59'40" T=58.21 179.60 UP  A.S. SERVICE STUB  PROP 12" ADS N-12  PROP 12" ADS N-12
		N11'00'00"E 73.28' CB-14+47 (20) - 1 ½" BALL VALVE & BOX
		450.00'
		PUBLIC - VARIABLE WINTH)  STEP 178.800  WEXTSTING HYDRANT  TX9.2018  STEP 188.800  WARRABLE WINTH  WARRABLE WI
PROPOSED PROPOSED  1 1/2" PRESSURE SEWER		OHW
PROP 12" ADS N-12 L=37', S=0.020	PROP 12" ADS N-12 L=76', S=0.017	8" DICL CAP—  & NIPPLE  8" GATE VALVE  & BOX  WATER MAIN  (APPROX)
184 PROP 12" ADS N-12	PROPOSED FLUSHING STATION RIMS TO GRADE INV.=177.60±	WF 101 START  WF 102  WF 104  BOLT ON BONNET  ELEV.=177.84  WF 55  AWF 55  AWF 55  AWF 56 END  WF 51 START  (APPROX)  WF 55  AWF 56 END
180 L=182', S=0.005	(4' MIN. COVER)	CAMBRIDGE RESERVOIR  CITY OF CAMBRIDGE  250 PLAN  1" TYPE K COPPER WATER —  SERVICE W/CORPORATION  STOR CORPER TURNS CURB.  CAMBRIDGE RESERVOIR  CAMBRIDGE RESERVOIR  SERVICE W/CORPORATION  STOR CORPER TURNS CURB.
4' MIN /		EDGE OF BORDERING VEGETATED WETLAND STOP, COPPÉR TUBING, CURB STOP AND SERVICE BOX.  AS DELINEATED BY B&C ASSOCIATES, INC.  ORAD ISSUED DEP#201-1038
4.5' MIN		
172 DMH-1 STA. 1+98 RIM=182.44 INV. IN=17	5.32 (CB-1) STA. 2+79.71	HOMES AT HOBBS BROOK  BALANCED HOUSING RESIDENTIAL DEVELOPMENT
INV. IN=17 INV. IN=17 INV. OUT=	5.32 (CB-2) 5.32 (CB-3) 6.32 (CB-3) 6.32 (CB-3) 6.32 (CB-3) 6.32 (CB-3) 6.32 (CB-1) 6.32 (CB-2) 6.32 (CB-2) 6.32 (CB-1) 6.32 (CB-2) 6.32 (CB-1) 6.32 (CB-2) 6.33 (CB-1) 6.32 (CB-2) 6.32 (CB-2) 6.33 (CB-1) 6.33 (CB-1) 6.34 (CB-1) 6.34 (CB-1) 6.34 (CB-1) 6.35 (	
168 CB-1 STA. 0+17.73 PRIOR TO  INSTALL A PRIOR TO  INSTALL A PRIOR TO  CB-2 STA. 1+69.23 RIM=180.80		GEORGE LOCATED IN  LOCATED IN  LOCATED IN  LOCATED IN
PROPOSED 8" WATER MAIN  DATUM ELEV  165.00	6 (DMH-1)	LEXINGTON, MASSACHUSETTS
165.00 9. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	75.6	PREPARED FOR
+50 +50	+50 +50 +50	SYMES DEVELOPMENT & PERMITTING, LLC  SCALE: 1" = 40' DATE: FEBRUARY 20, 2018
-0+50 0+00 <sup>+50</sup> 1+00 <sup>+50</sup> 2+00	3+00	PREPARED BY  PREPARED BY  STAMSKI AND McNARY, INC  REVISIONS  PREPARED BY  STAMSKI AND McNARY, INC  1000 MAIN STREET ACTON, MA
PROFILE: SCALE: 1"= 40' H.		REVISIONS  1000 MAIN STREET ACTON, MA  ENGINEERING - PLANNING - SURVEYING  CHIEFE N 5 OF 14 DEPONDER N CW 5 OF 1
		(5676 DEF BHD 2.dwg)  NO. DATE  DESCRIPTION  BY CHK'D  SHEET No. 5 OF 11  PROJECT No. SM-5676



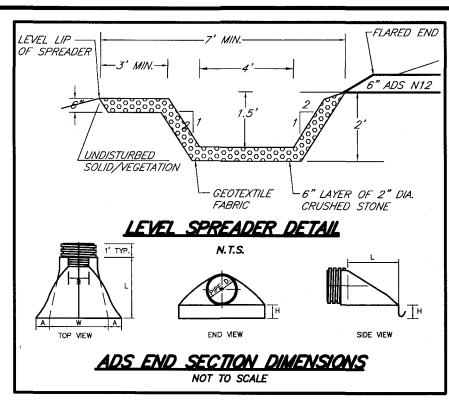


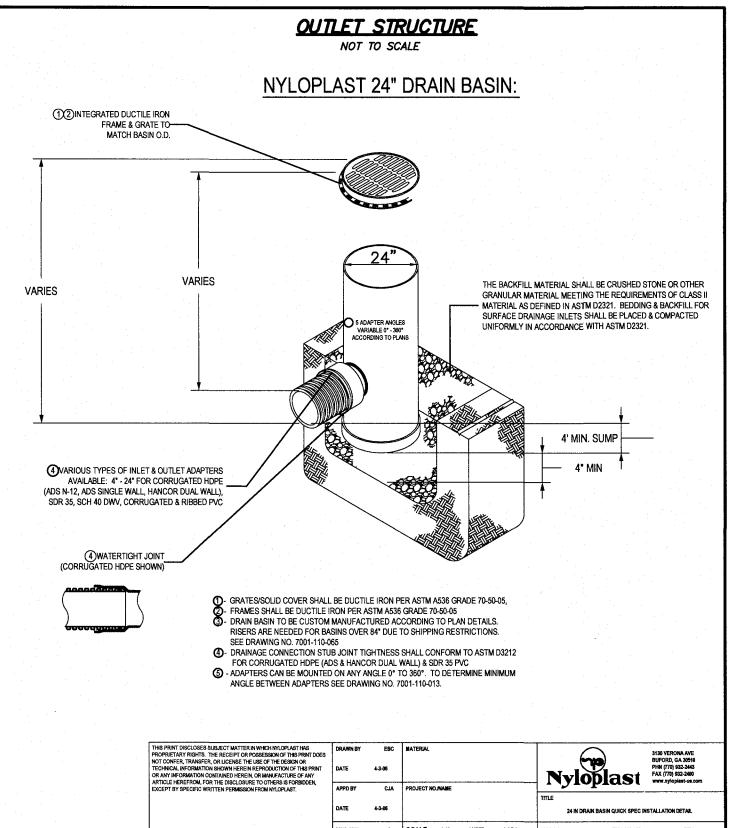


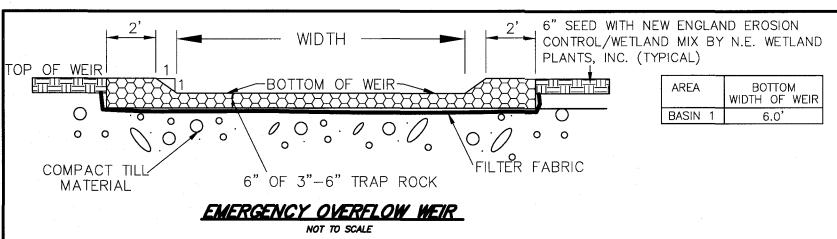


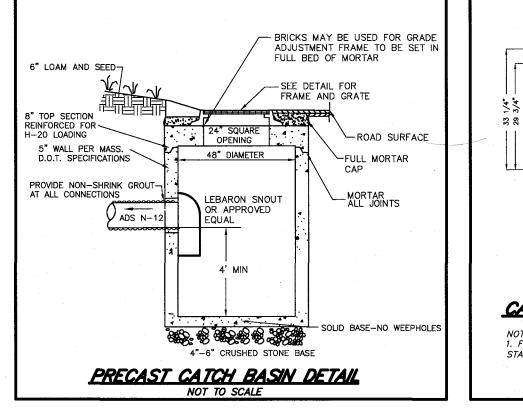


25 7/8" SQ. FRAMES AVAILABLE 4"-6"-8"









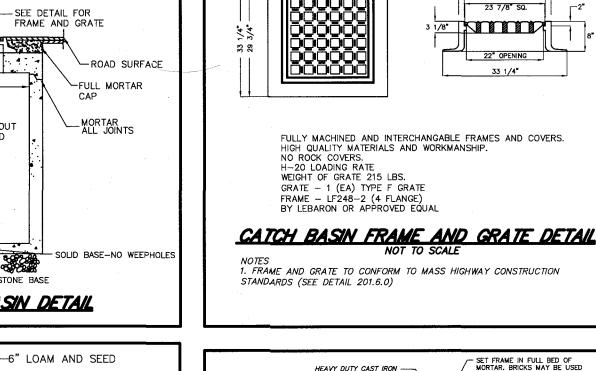
SELECT MATERIAL FOR BACKFILL CONTAINING NO STONES GREATER THAN

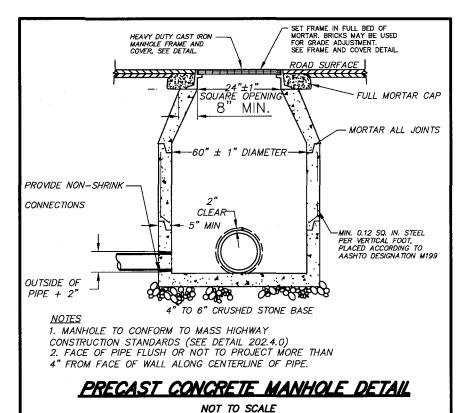
COMPACTED SCREENED GRAVEL

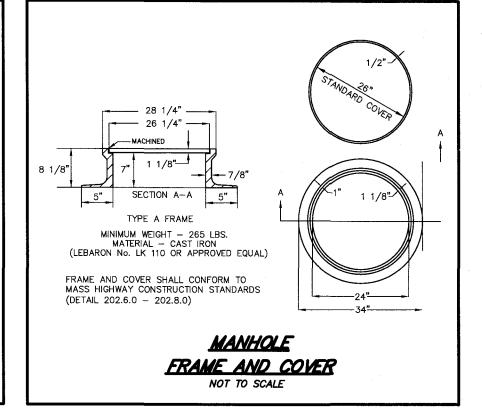
8 INCHES COMPACTED IN 6" LIFTS (MAX)

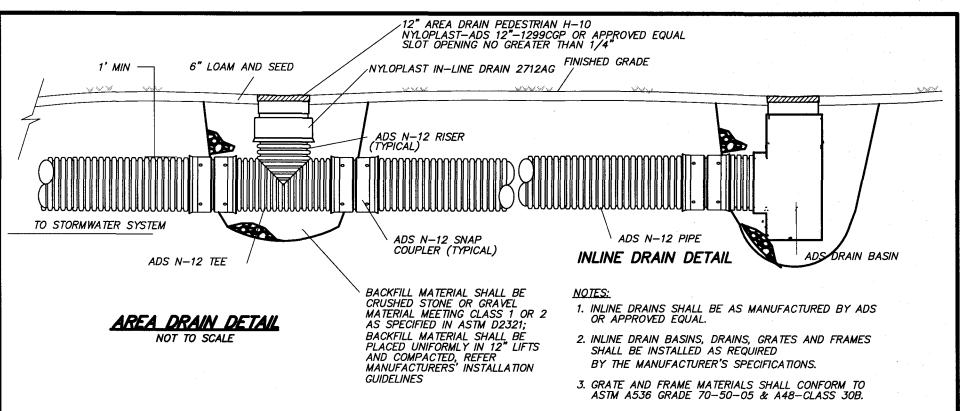
AVEMENT

GRAVEL BASE {







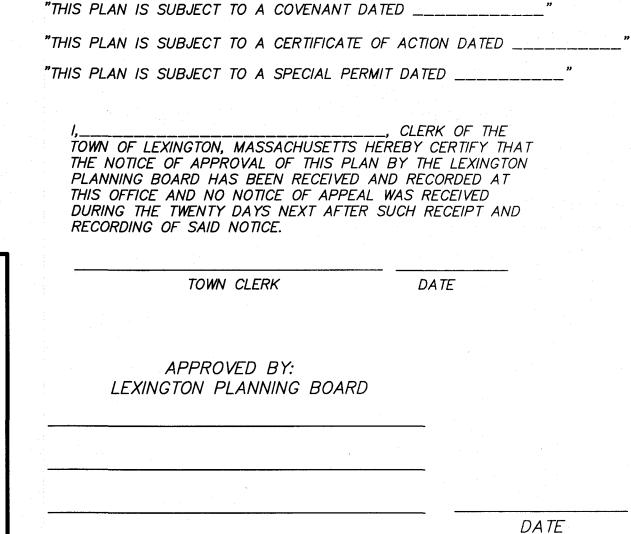


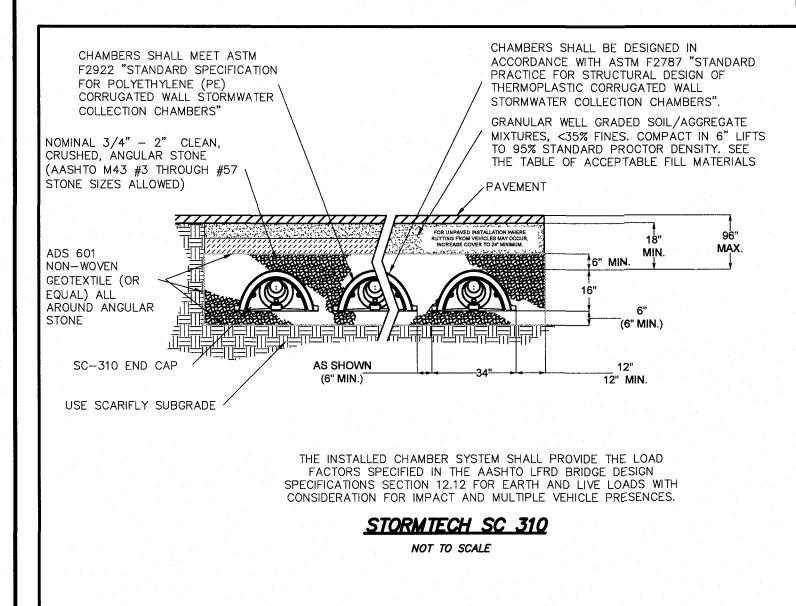
### **GENERAL NOTES:**

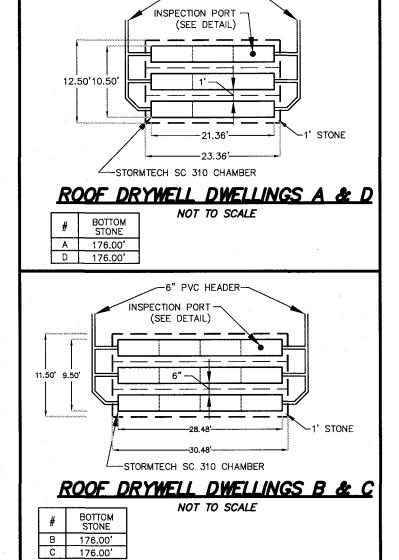
- ALL UNDERGROUND UTILITIES SHOWN HERE WERE COMPILED ACCORDING TO AVAILABLE RECORD PLANS FROM VARIOUS UTILITY COMPANIES AND PUBLIC AGENCIES AND ARE APPROXIMATE ONLY. ACTUAL LOCATIONS MUST BE DETERMINED BEFORE EXCAVATING.
- 2. BLASTING, INSTALLING, BACK FILLING, GRADING OR PAVEMENT RESTORATION OR REPAIR. ALL UTILITY COMPANIES, PUBLIC AND PRIVATE MUST BE CONTACTED, INCLUDING THOSE IN CONTROL OF UTILITIES. SEE CHAPTER 370, ACTS OF 1963 MASS.
- WE ASSUME NO RESPONSIBILITY FOR DAMAGES INCURRED AS A RESULT OF UTILITIES OMITTED OR INACCURATELY SHOWN. BEFORE PLANNING FUTURE CONNECTIONS. APPROPRIATE UTILITY ENGINEERING DEPT. MUST BE CONSULTED. THE CONTRACTOR SHALL NOTIFY PUBLIC UTILITY COMPANIES AT LEAST 72 HOURS PRIOR TO DIGGING OR EXCAVATING ON PUBLIC OR PRIVATE PROPERTY. DIG SAFE TEL. NO. 1-888-344-7233
- 4. ALL WATER LINE VALVES, ETC. SHALL MEET ALL SPECIFICATIONS OF THE TOWN OF LEXINGTON WATER & SEWER DIVISION.
- 5. ALL STUMPS AND OTHER CONSTRUCTION DEBRIS SHALL BE PROPERLY REMOVED FROM THE SITE. ANY FILL MATERIAL USED SHALL BE FREE OF HAZARDOUS MATERIALS, WASTE, AND CONSTRUCTION DEBRIS.
- RIP RAP SHALL CONSIST OF HARD DURABLE STONE, ANGULAR IN SHAPE, THAT IS WELL GRADED WITHIN THE 25# TO 125# RANGE. THE RIP RAP SHALL BE PLACED OVER A
- 12" BASE OF COARSE BANK RUN GRAVEL. RIP RAP SHOWN SCHEMATICALLY AT DRAINAGE
- OUTFALLS SHALL BE PLACED FOR A 3' WIDTH AND 6' LENGTH UNLESS OTHERWISE SPEC'D. THE LIMITS OF WORK SHALL BE CLEARLY MARKED IN THE FIELD PRIOR TO THE START OF
- CONSTRUCTION OR SITE CLEARING PER THE STORMWATER POLLUTION PREVENTION PLAN. EXISTING TOPSOIL SHALL BE STRIPPED, STOCKPILED, SCREENED AND SPREAD TO REQUIRED
- 10. CATCHBASIN SUMPS AND STORM WATER BASINS SHALL BE CLEANED FOLLOWING COMPLETION OF CONSTRUCTION AND ANNUALLY THEREAFTER PER O & M PLAN.
- THE ENTIRE WORK AREA SHALL BE CLEARED OF BUILDINGS TO BE RAZED, PAVEMENT, DEBRIS, BOULDERS, BRUSH, TREES, STUMPS, UNSUITABLE MATERIALS AND LIKE MATERIAL
- 12. ALL TOP AND SUBSOIL WITHIN WORK AREA SHALL BE REMOVED AND STOCKPILED ON SITE AS DIRECTED BY THE OWNER. LOAM SHALL BE SCREENED AND STOCKPILED ON-SITE FOR RE-USE IN AREAS OF GENERAL LOAM AND SEED.
- 13. THE CONTRACTOR SHALL MAINTAIN THE SITE IN A SAFE CONDITION THROUGHOUT THE CONTRACT PERIOD. THE CONTRACTOR SHALL FULLY COMPLY WITH ALL STATE, FEDERAL, AND LOCAL REGULATIONS PERTAINING TO SAFETY.
- SHRUBS PROVIDE PER LANDSCAPE PLAN SPECIFICATIONS. 14. THE PROPOSED SIGNS SHALL BE DESIGNED AND INSTALLED IN CONFORMANCE WITH THE U.S. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES 2009 EDITION FOR STREETS AND HIGHWAYS OR AS MOST RECENTLY AMENDED. EXISTING SIGNS TO BE RELOCATED WHERE NECESSARY. THE ELECTRICAL POWER DISTRIBUTION SHALL BE INSTALLED IN ACCORDANCE WITH THE

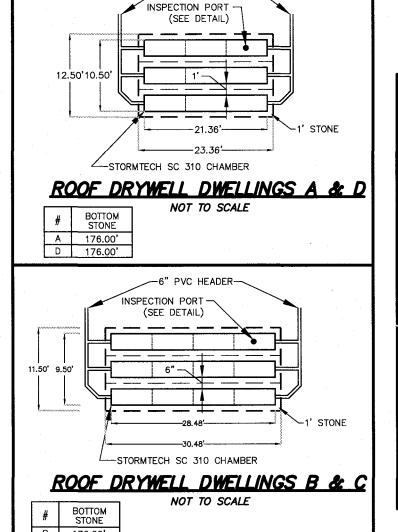
SPECIFICATIONS OF THE LEXINGTON MUNICIPAL LIGHT PLANT IN EFFECT AT THE TIME. ELECTRICAL REQUIREMENTS AND LOCATION TO BE DETEREMINED BY OTHERS AND CONFIRMED WITH OWNER.

- 15. NO EARTH SHALL BE REMOVED FROM SITE.
- 16. PLAN IS SUBJECT TO REVIEW AND COMMENT BY THE CITY OF CAMBRIDGE WATER DEPARTMENT, DUE TO LOCATION OF THE CAMBRIDGE RESERVOIR IN PROXIMITY TO SITE.
- 17. THE EXISTING PRIVATE ON-SITE SEWAGE DISPOSAL SYSTEM SHALL BE ABANDONED IN ACCORDANCE WITH 310 CMR 15.354: ABANDONMENT OF SYSTEMS.

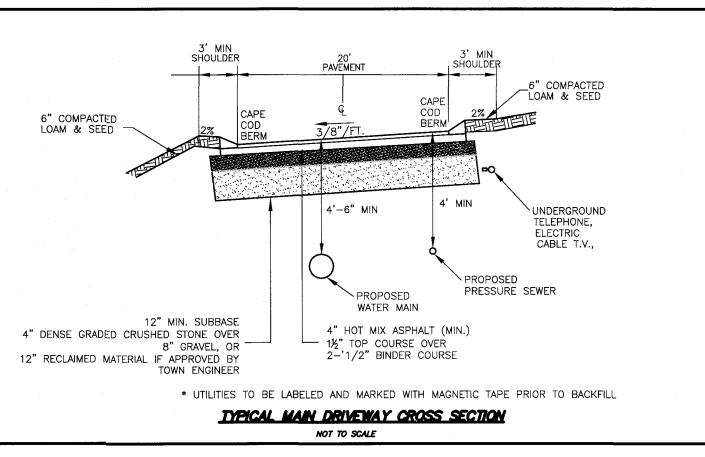


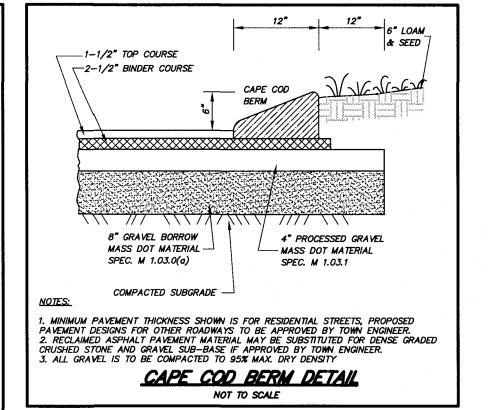






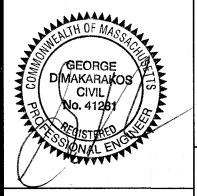
TYPICAL TRENCH DETAIL





**REVISIONS** NO. DATE **DESCRIPTION** BY CHK'D

### HOMES AT HOBBS BROOK BALANCED HOUSING RESIDENTIAL DEVELOPMENT



JOSEPH

MARCH # 36384

### CONSTRUCTION DETAILS

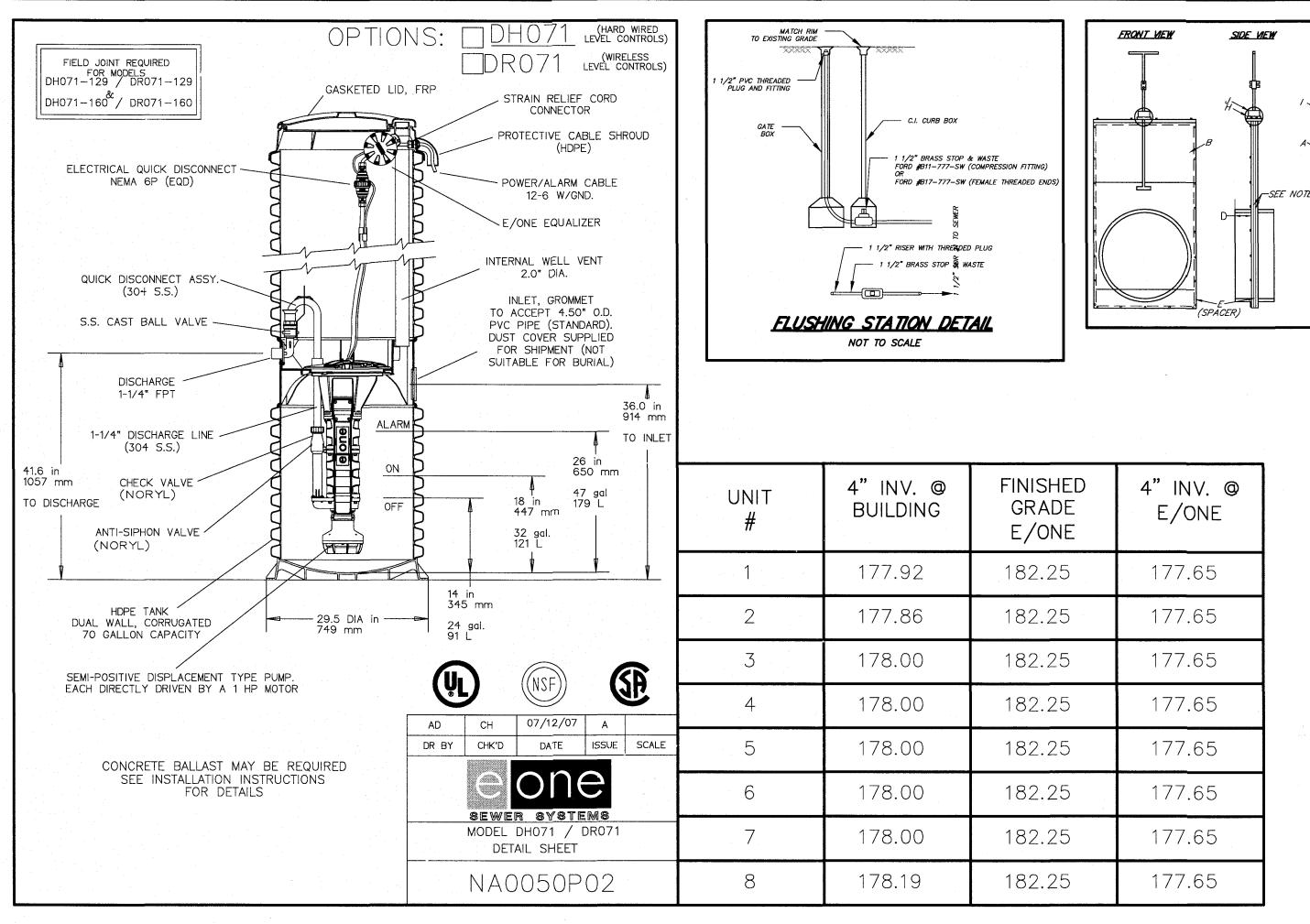
LOCATED IN LEXINGTON, MASSACHUSETTS (MIDDLESEX COUNTY)

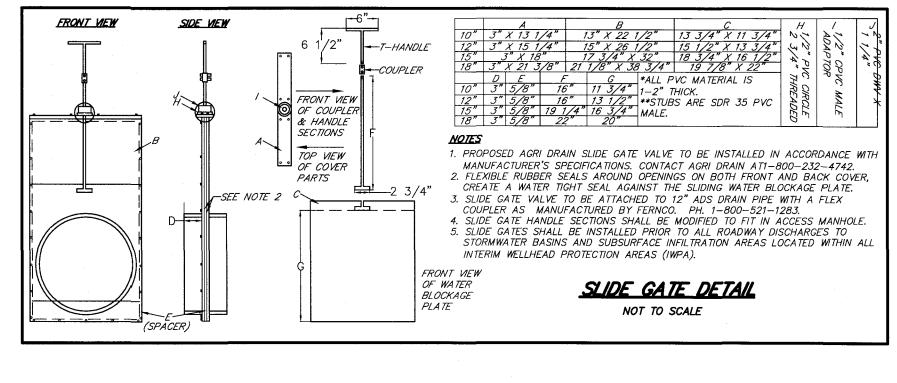
PREPARED FOR SYMES DEVELOPMENT AND PERMITTING, LLC SCALE: 1" = 40'DATE: FEBRUARY 20, 2018

PREPARED BY STAMSKI AND McNARY, INC 1000 MAIN STREET ACTON. MA

ENGINEERING - PLANNING - SURVEYING

SHEET No. 9 OF 11 PROJECT No. SM-5676





FINISHED GRADE-

--- WATER MAIN

JNLESS OTHERWISE AUTHORIZED BY THE ENGINEERING DIVISION.

ENCOUNTERED.

5. SERVICE TAPS SHALL BE PERFORMED BY THE WATER DIVISION.

1. A 10' HORIZONTAL SEPARATION MUST BE MAINTAINED FROM THE SEWER

3. WHERE AN EXISTING SERVICE IS BEING REPLACED TO THE MAIN, THE OLD SERVICE SHALL BE CAPPED AT THE CORPORATION.

SERVICE UNLESS OTHERWISE AUTHORIZED BY THE ENGINEERING DIVISION.
2. FOR SERVICE RENEWALS, TUBING SHALL BE REPLACED TO THE PROPERTY LINE

. THE WATER AND SEWER DIVISION MUST BE NOTIFIED IF LEAD SERVICES ARE

S. SERVICE TAPS GREATER THAN 1" REQUIRE A SADDLE AND ARE SUBJECT TO HE APPROVAL OF THE ENGINEERING DIVISION.

USE QUICK STYLE COMPRESSION CONNECTIONS FOR ALL SERVICE BRASS.

TO CURB STOP. MOST EXISTING CURB STOPS REQUIRE 3/4" X 1" FEMALE ADAPTERS FOR NEW ENGLAND STYLE THREADS.

9. ALL CONNECTIONS TO EXIST. CURB STOPS SHALL REPLACE SERVICE BOXES IF NOT BUFFALO STYLE.

10. WATER SERVICE SHALL INCLUDE A BALL VALVE WITH COMPRESSION FITTING

WATER SERVICE CONNECTION 2" AND SMALLER NOT TO SCALE

B. FOR 1" CONNECTIONS TO EXIST. 3/4" CURB STOP CONNECT ADAPTER DIRECTLY

BALL VALVE TYPE-

300 PSI WORKING PRESSURE SADDLE REQUIRE >

CORPORATION

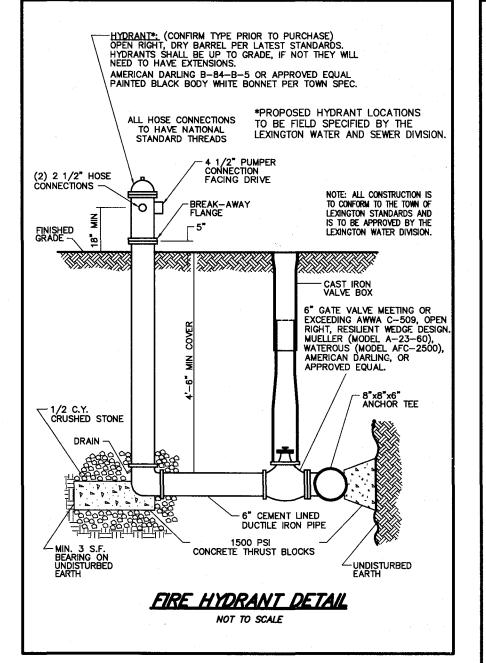
-2 1/2" BUFFALO STYLE, SLIDE TYPE

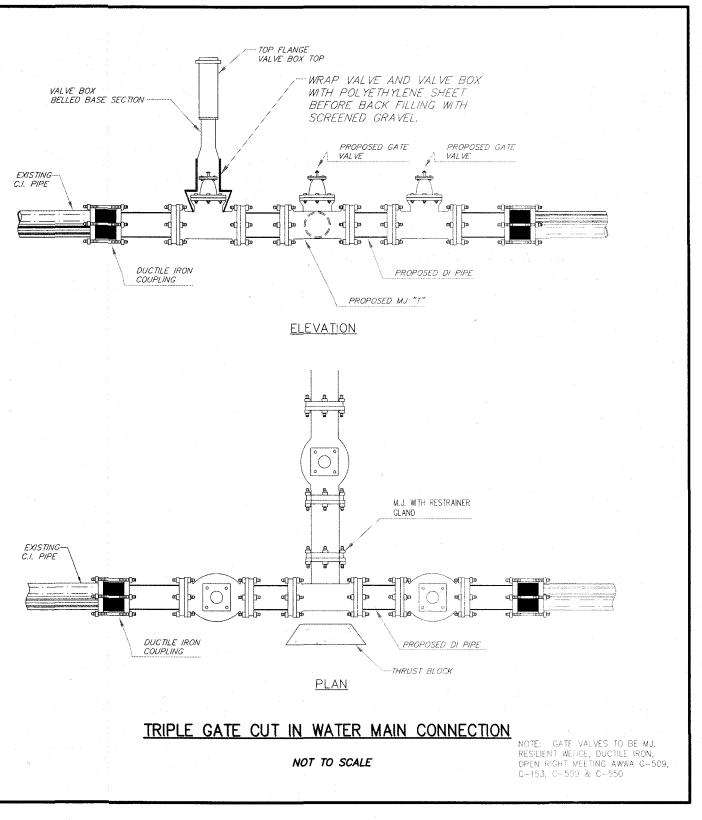
TO HOUSE OR BUILDING

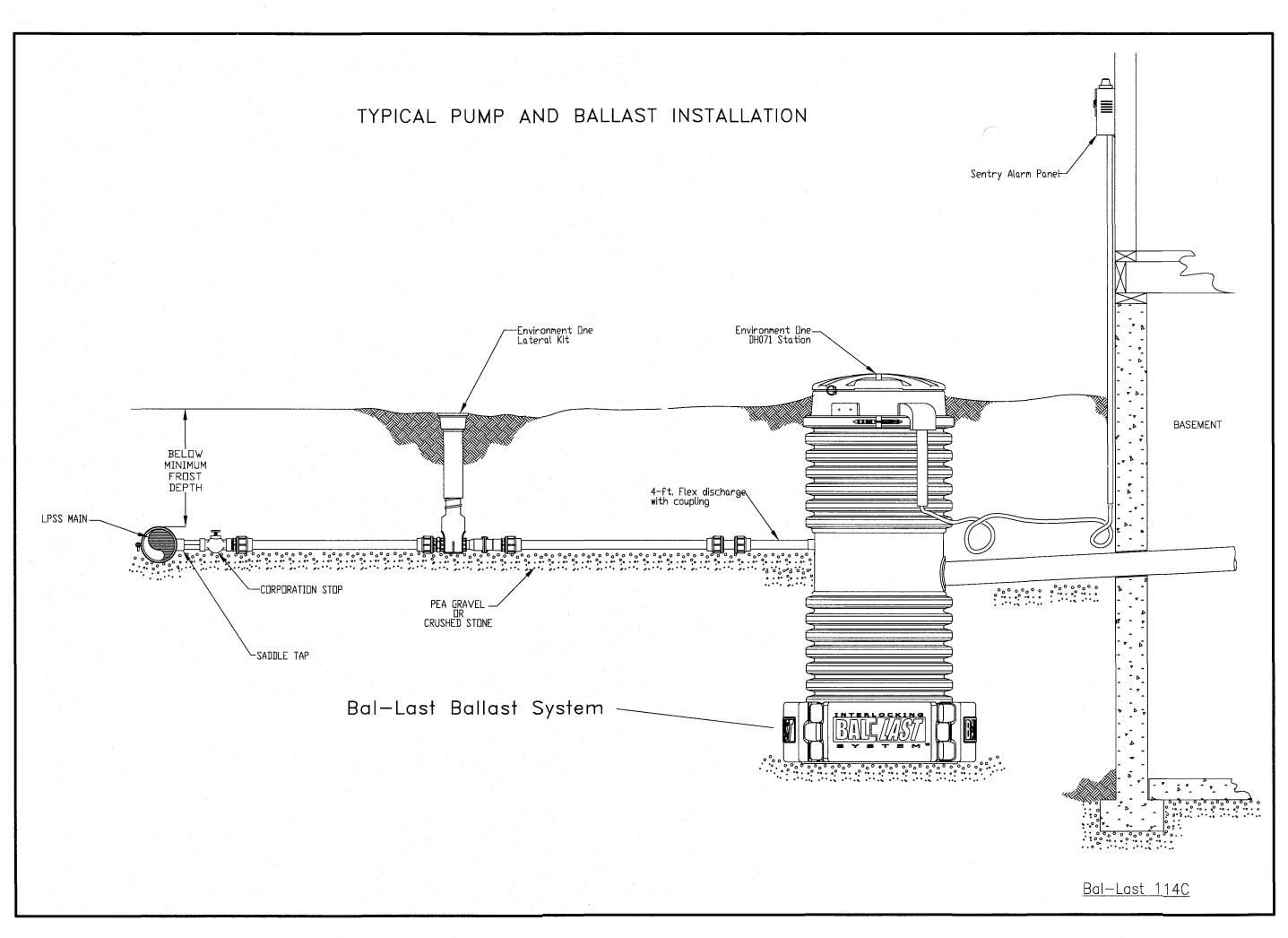
OPEN RIGHT BALL CURB STOP

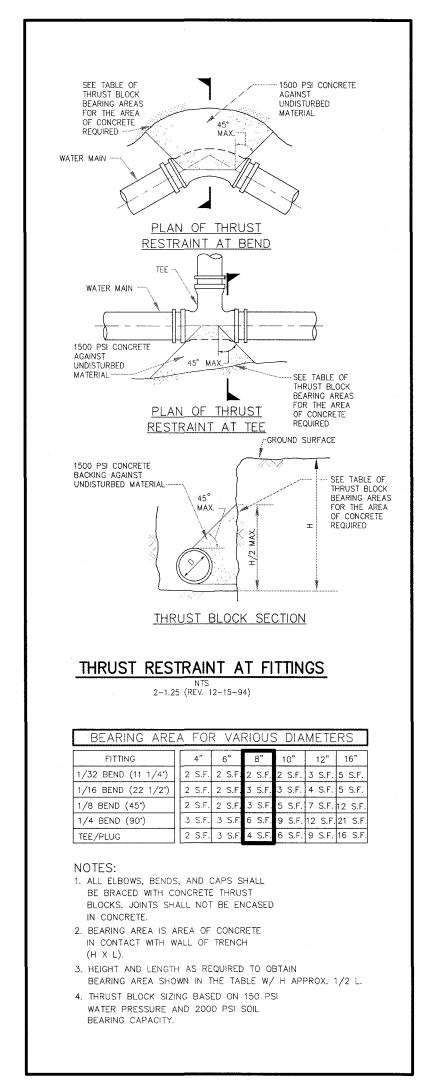
AWWA C800-89

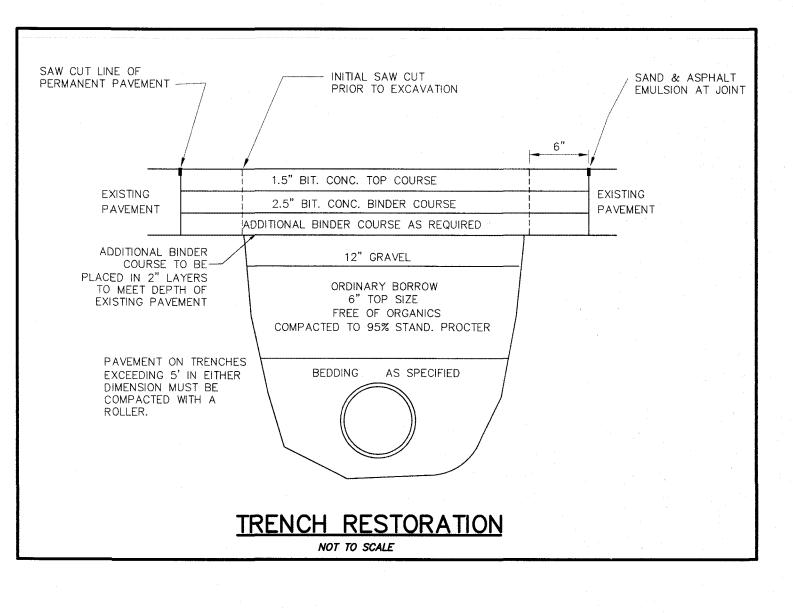
SLIDE TYPE SERVICE BOX











"THIS PLAN IS SUBJECT TO A COVENANT DATED \_\_\_\_\_"

"THIS PLAN IS SUBJECT TO A SPECIAL PERMIT DATED \_\_\_\_\_\_"

TOWN OF LEXINGTON, MASSACHUSETTS HEREBY CERTIFY THAT

THE NOTICE OF APPROVAL OF THIS PLAN BY THE LEXINGTON

PLANNING BOARD HAS BEEN RECEIVED AND RECORDED AT

DURING THE TWENTY DAYS NEXT AFTER SUCH RECEIPT AND

DATE

**REVISIONS** 

DESCRIPTION

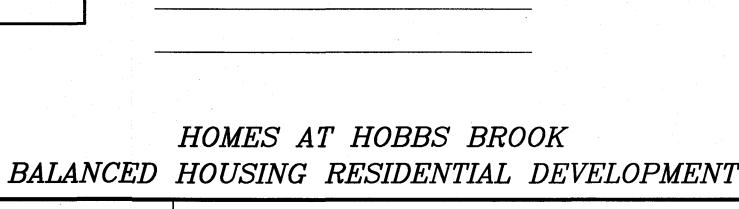
THIS OFFICE AND NO NOTICE OF APPEAL WAS RECEIVED

RECORDING OF SAID NOTICE.

TOWN CLERK

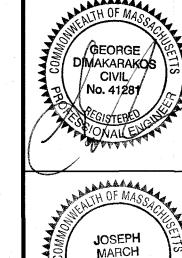
NO. DATE

"THIS PLAN IS SUBJECT TO A CERTIFICATE OF ACTION DATED \_\_\_



APPROVED BY:

LEXINGTON PLANNING BOARD



BY CHK'L

CONSTRUCTION DETAILS LOCATED IN LEXINGTON, MASSACHUSETTS (MIDDLESEX COUNTY)

LARGER PIPE DIAMETER SLEEVE

WATER MAIN

1. PIPE SLEEVE TO BE PROVIDED ONLY WHEN SEPARATION REQUIREMENTS OF WATER

AND SEWER DIVISION CANNOT BE MET.

2. WHEREVER POSSIBLE, WATER SERVICES SHALL BE INSTALLED WITH A MINIMUM OF 10 FEET HORIZONTAL SEPARATION FROM SEWER SERVICES AND DRAINS AND A MINIMUM OF 3 FEET FROM ALL OTHER UTILITIES. ENCASEMENT OF EITHER THE WATER OR SEWER SERVICE IS REQUIRED IN THE FORM OF A 10—FOOT SLEEVE ON EITHER SIDE OF THE ADJACENT STRUCTURE IN THE FOLLOWING CASES:

A) THE MINIMUM 10—FOOT HORIZONTAL SEPARATION FROM SEWER SERVICES AND DRAIN CANNOT BE MET;

B) THE TOP OF THE SEWER BELL IS LESS THAN 18" FROM BOTTOM OF THE WATER LIN

) A STORM DRAIN IS WITHIN 1.5 FEET ABOVE THE WATER LINE; OR

4. JOINTS OF BOTH PIPES SHALL BE LOCATED AS FAR AWAY AS POSSIBLE.

) A SEWER MAIN OR CONNECTION IS ABOVE WATER MAIN OR CONNECTION.

WATER & SEWER CROSSING DETAIL

FILL WITH GRANULAR MATERIAL

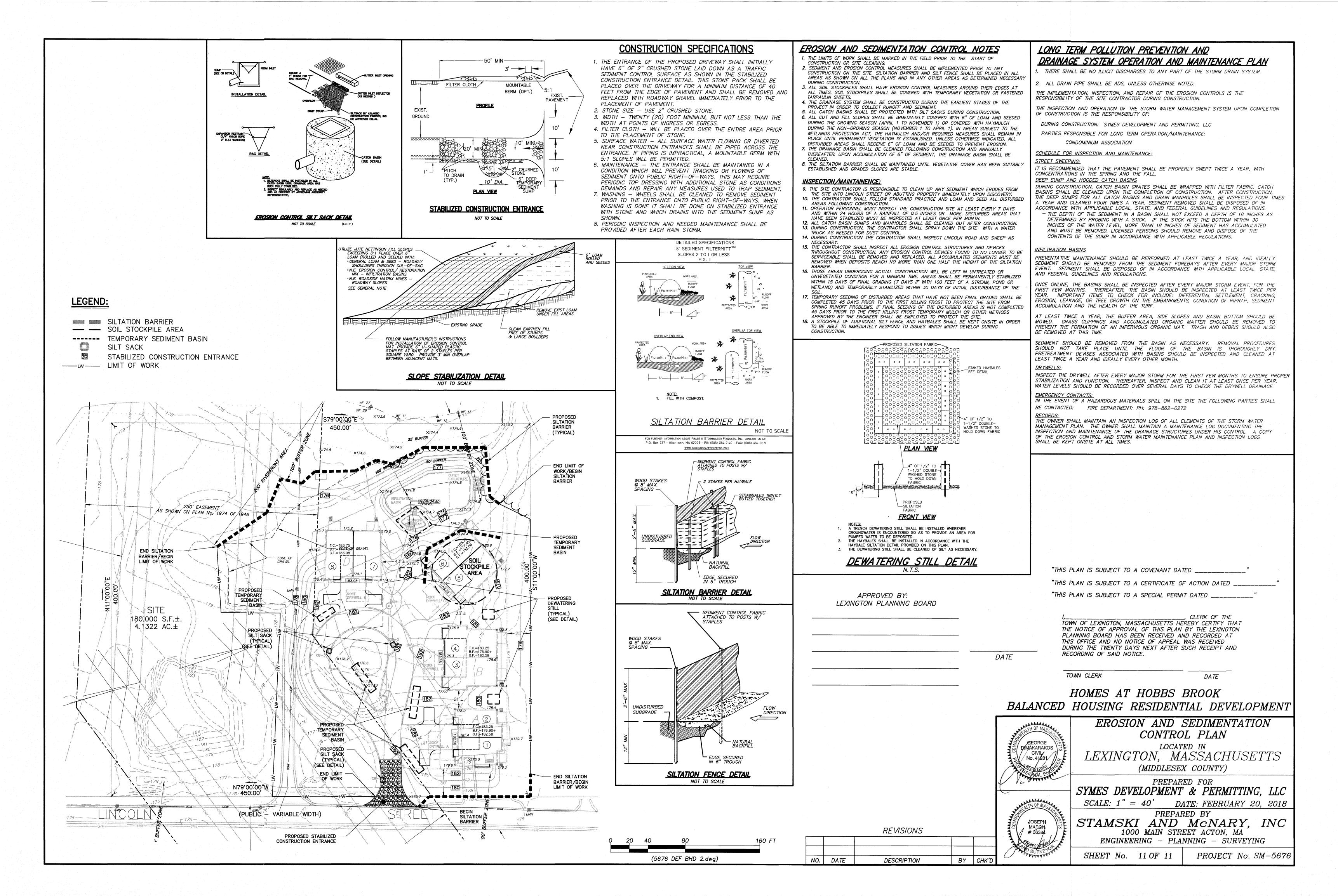
<del>-,-</del>S----10' MIN. (SEE NOTE

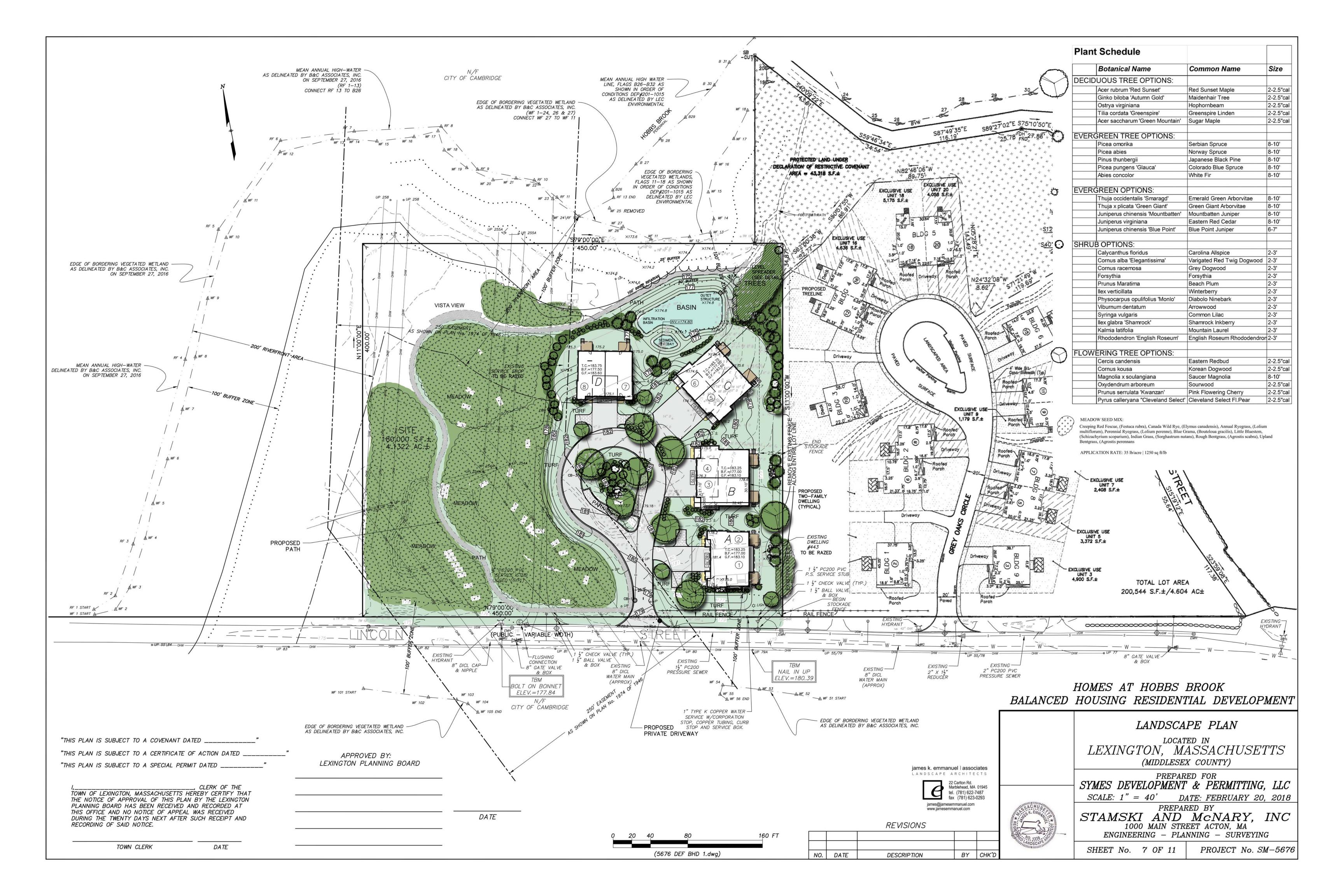
DATE

PREPARED FOR SYMES DEVELOPMENT AND PERMITTING, LLC SCALE: 1" = 40' DATE: FEBRUARY 20, 2018

PREPARED BY STAMSKI AND McNARY, INC
1000 MAIN STREET ACTON, MA ENGINEERING - PLANNING - SURVEYING

SHEET No. 10 OF 11 PROJECT No. SM-5676







September 6, 2017

Mr. Jeffrey Rhuda Symes Permitting & Development LLC 50 Dodge Street Beverly, MA 01917



### Dear Mr. Rhuda:

You have contacted us regarding the property at 443 Lincoln Street, Lexington, Massachusetts, thru which Eversource has an established easement. You have provided us with the following two plans showing alternative development of that property:

- Conventional Subdivision: One plan is entitled "conventional subdivision proof plan"
  (sheet 3 of 4). This plan shows a dead-end road in the easement area that would serve as
  access to only three dwellings. A fourth lot fronts on Lincoln Street. No dwellings are
  located within our easement area.
- Balanced Housing: One plan is entitled "site construction plan, balanced housing residential development" (sheet 2 of 4). On this plan, only a small portion of the proposed roadway is within the easement area. No dwellings or driveways are within the easement area.

You state that while you prefer to develop the site using the balanced housing plan (sheet 2), the Lexington Zoning Bylaws require that before you are permitted to do so, you must satisfy the Planning Board that the development shown on sheet 3, the proof plan (conventional subdivision), is possible. Because of that requirement, you have asked whether the road could be built as shown on the plan entitled "conventional subdivision proof plan" (sheet 3). Our concern is for safety, reliability, integrity and security of our system. We always review requests like yours on a case by case basis, as the circumstances in each case vary. The fact that we allow a certain activity in one area does not mean that we shall allow that activity in another area. We note that there are improvements within the easement area that was previously approved by us under a license agreement, as the location of such improvement at the time of the Company's review and current configuration of our lines did not conflict with our use of our easement. The license granted in no way restricts the Company's future use and enjoyment of its easement rights as it conditions the land owners use of the easement.

In response to your specific question, we respond that we would consider the conventional

In response to your specific question, we respond that we would consider the conventional approach as shown on sheet 3, but would require modifications to details before construction. For example, any roadway within our easement must provide adequate clearance between the finished roadway surface and our overhead wires. The precise location and construction of project utilities and drainage system would require our approval, as we have underground rights as well within the entire 250 foot wide corridor. We would make sure that any roadway and utility infrastructure are safely buffered from our structures and utilities cross the easement at 90

degrees. The Company would also evaluate any such proposal to ensure it does not interfere with the Company's likely future exercise of its easement rights.

We trust that this letter is sufficient to address the question regarding the hypothetical approval of your conceptual, conventional subdivision plan, so that the Town allows you to proceed with your preferred plan, which we believe is the appropriate approach to your development.

Sincerely

Theresa M. Feuersanger

Supervisor &D Rights and Survey

247 Station Drive SE 210 Westwood Mass 02090

781-441-8277

### <u>Homes at Hobbs Brook</u> Project Narrative – 443 Lincoln Street

Existing conditions - The 4.13 acre site contains a single family dwelling (#443) near Lincoln Street and a detached multi use service shop (automobile repair) towards the rear line of the lot which are both proposed to be razed. The site is rectangular in shape consisting of four-hundred and fifty feet (450') of frontage along Lincoln Street with a lot depth of four-hundred feet (400'). This 180,000 square foot site is located entirely within the Residential District (RO) and has just two direct abutters. The recently constructed "Grey Oaks Circle" Balanced Housing Development consisting of fourteen units is located to the east and the City of Cambridge Reservoir Land is located to the north, south and west of the site.

The structures on the site are respectful of the two-hundred and fifty-foot wide Utility Easement which overlays a portion of the site at an angle from front to back along the westerly side line of the lot in common the City of Cambridge land. The paved driveway and portion of the gravel parking area associated with the service shop are within this utility easement, while the paved driveway serving the dwelling's garage under is located just outside this easement. The existing pavement in the public right-of-way is also greater in width in front of the dwelling to allow for on-street parking. Accessory to the existing dwelling are patios with typical landscaping, retaining walls, fences and lawn areas. A six-foot high wooden stockade fence near the dwelling is also present along the easterly side line of the lot in common with Lincoln Woods. The remaining area outside the easement between the existing structures and along the gravel parking area, is primarily woodland. The area within the utility easement is primarily cleared in fair condition with areas of emerging vegetation consisting of overgrown brush and selective trees present primarily along the street frontage and site perimeter.

Existing utility services - The dwelling and service shop are currently served by town water service and private on-site sewer services. Electrical services appear to be both above ground and below ground; there is an underground line within the utility easement. According to the Sewer & Water Main Record As-built Plan (RS 708B), both the 8-inch water main and 1 ½ inch pressure sewer main, which originate from Weston Street to the east, terminate just past the existing service shop driveway to the west prior to the Lincoln Town Line. The pressure sewer main reduces down from a 2-inch main approximately 200' east of the site. Fire protection is provided by the existing hydrants within Lincoln Street.

Existing wetland resource areas – Abutting the site to the north and west is Hobbs Brook which is a perennial stream with associated bordering vegetated wetland and Bordering Land Subject to Flooding. Hobbs Brooks flows under Lincoln Street and into the Cambridge Reservoir to the southwest. Abutting the site to the south are two segments of wetlands bordering on the Reservoir along the opposite side of Lincoln Street. The delineation of these abutting resource areas have been recently confirmed, thru the issuance of an Order of Resource Areas Delineation, by the Lexington Conservation Commission. A portion of the two-hundred foot (200') Riverfront Area measured from the mean annual high water line of Hobbs Brook is present along the rear line of the lot in addition to the one-hundred foot (100') buffer zone which is measured from the edge of the wetlands bordering Hobbs Brook. The outer one-hundred foot (100') buffer zone is also present within the front yard of the dwelling and to the west of the

service shop driveway. The Buffer Zone is a Protected Resource Area under the Code of the Town of Lexington for Wetland Protection, Chapter 130.

Existing stormwater runoff – On-site stormwater runoff drains to Hobbs Brook via sheet flow. A majority of the site drains to a low point behind the service shop to the north, while the runoff from the front of the site drains towards the public street to the south. Runoff within Lincoln Street primarily drains to the west towards Hobbs Brook from a high point near the existing dwelling. According to the NRCS Soil Survey, existing on-site soils consist of Windsor Loamy Sand which is excessively drained and Deerfield Loamy Sand which is moderately well drained.

Proposed Project - The proposed Balanced Housing Residential Development will provide a diversity of household types and sizes currently not available within a conventional development at this location. The granting of a special permit by the Planning Board will permit the construction of four two-family dwellings with open space. Access to the eight dwelling units from Lincoln Street will be provided via a private interior driveway with circular emergency turnaround. Individual driveways will be provided to each two-family dwelling from the interior driveway. The required sixteen (16) parking spaces required per zoning, two per dwelling, will be provided within the proposed garages and individual driveways. Four units will have a twocar garage and the remaining four units will have a one-car garage with a second parking space in front of each garage door. Additional parking is also available for most units within the individual driveways. The interior driveway has been designed to a width of twenty feet (20') to allow for proper circulation. The plan will also improve the riverfront buffer area by removing the large service shop and associated gravel parking area and incorporating native trees & shrubs. The proposal also provides controls from stormwater runoff, where currently there is none. A path is proposed that will connect to the existing path in the Grey Oaks Circle development to the east and loops around the proposed project to provide greater connectivity within the neighborhood. The proposed project also avoids conflict with the utility easement on the lot.

<u>Proof Plan</u> – The Applicant met last year with the Planning staff on a Conceptual basis to discuss the proof plan and a proposed BHD concept plan. Based on feedback from this meeting, the Proof Plan has been updated to include the proposed grades for the subdivision road option. The BHD Sketch plan has been updated to provide an alternative pavement layout with reduced building footprints provided by the Architect.

<u>Proposed utilities</u> – A proposed water main with hydrant from Lincoln Street is proposed within the private interior driveway. Individual water services will be provided from this main to each dwelling unit. E/One grinder pumps are proposed for each unit that will pump the wastewater to o the existing pressure sewer main in Lincoln Street. A condominium association consisting of the unit owners will be responsible for the operation and maintenance of the private utilities and stormwater controls.

### **Definitive List of Waivers**

BALANCED HOUSING RESIDENTIAL DEVELOPMENT Stamski and McNary, Inc.- Plan Date: February 20, 2018 443 Lincoln Street Lexington, MA

In reference to the Town of Lexington's Planning Board Zoning Regulations dated August 30, 2017, here is a list of waivers that this Balanced Housing Residential Development at 443 Lincoln Street requires.

 Referring to §5.1.2, Document and Plan Formatting Requirements, we request a waiver to 5.1.2.2 Vertical Datum: All elevations shown on profiles and topographic plans must be based on the North American Vertical Datum of 1988 (NAVD88) and identify all benchmarks used and their elevations.

The USGS vertical datum provided matches the neighboring Grey Oaks Circle Balanced Housing Development to the east and also matches the "Sewer & Water Main Construction," Lincoln Street, STA. 9+13 to STA. 20+19 plan prepared by Tutela Engineering Associates dated February, 2001. The use of the USGS Datum allows the Town and public to understand the neighborhood all at the same elevation system. The use of the required Datum is possible but could offer confusion to abutting plan continuity.

The applicant and Planning Board Reserve the right to modify the contents of this Definitive List of Waivers as a result of discussion at public meetings.

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- adjustments to window sizes and other exterior elements. Increasing or decreasing ceiling heights requires

for ensuring that they understand features in the home that are important to them. We are not responsible for typographical errors. Home Buyer documents provided to them and shall be solely responsible shall give thoughtful consideration to all drawings and



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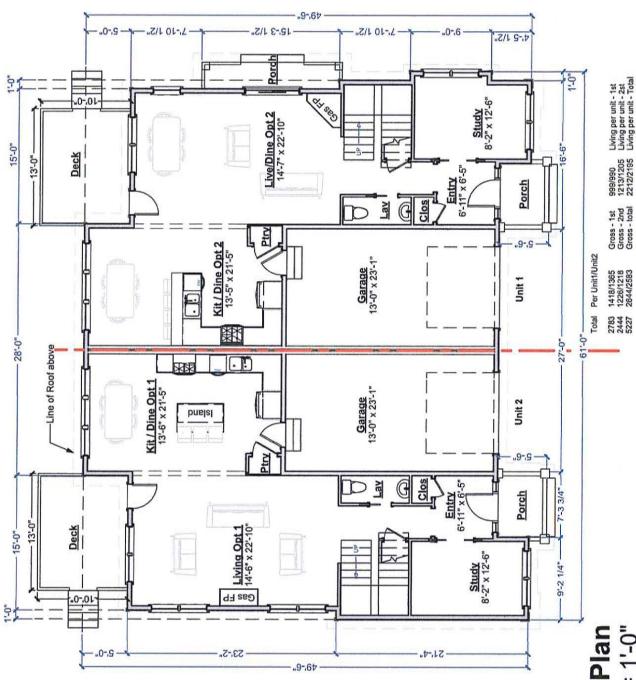


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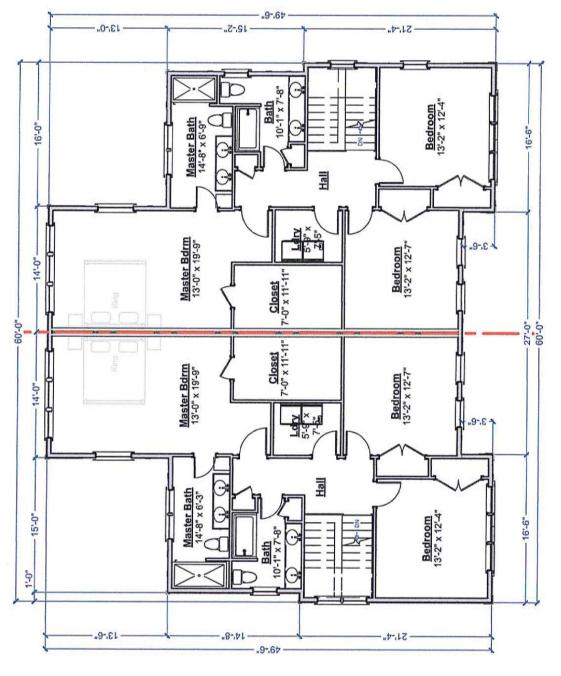
First Floor Plan

Scale: 3/32" = 1'-0"

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# Second Floor Plan

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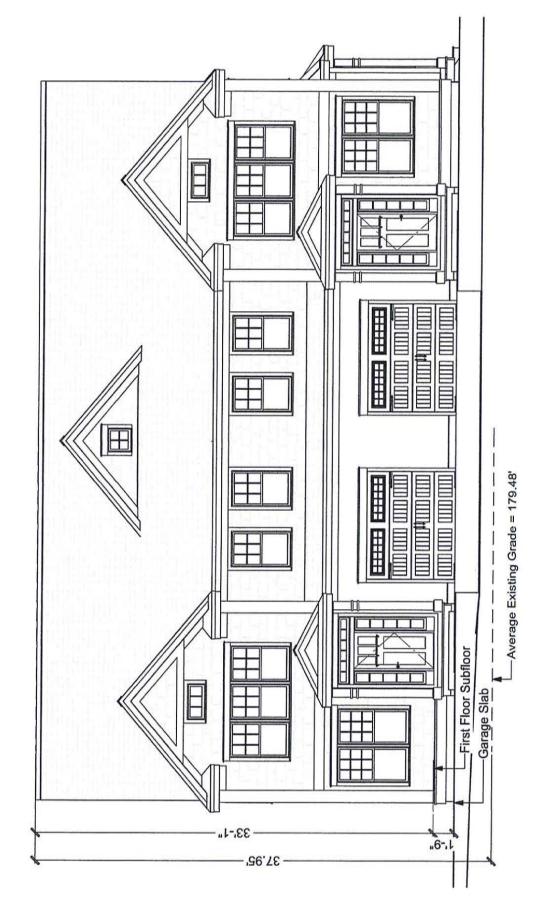
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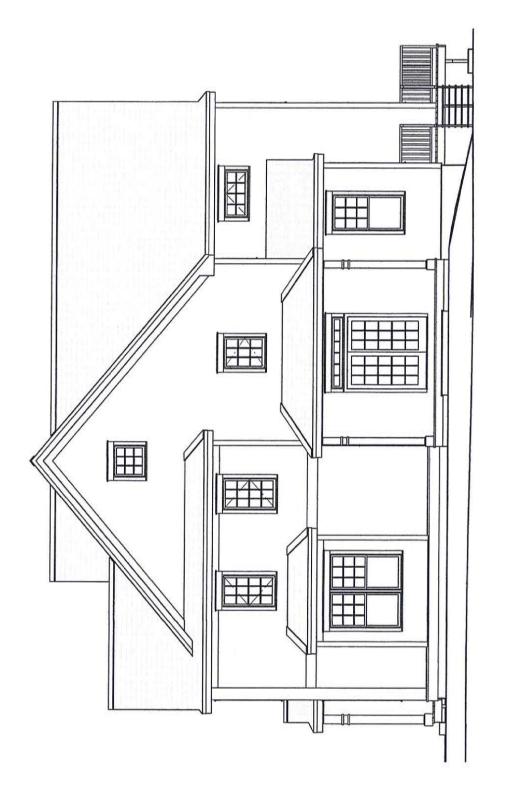
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# Front Elevation Scale: 1/8" = 1'-0"

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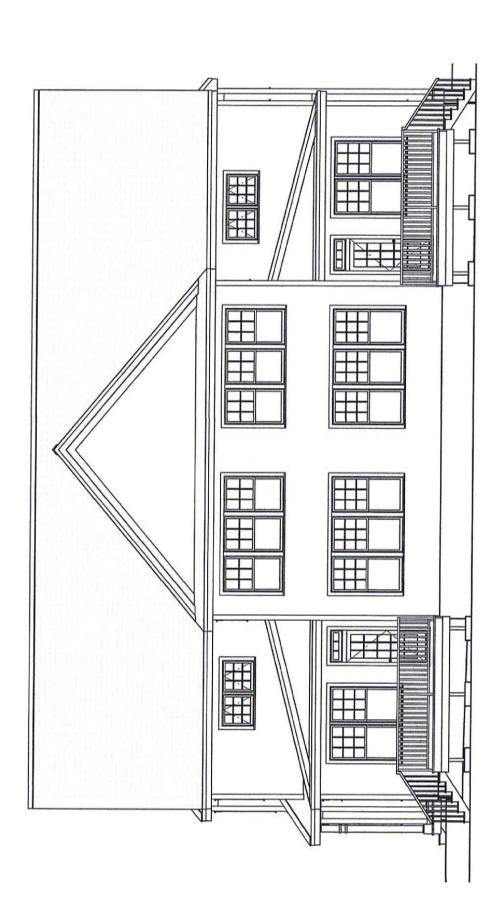




# Right Elevation Scale: 1/8" = 1'-0"

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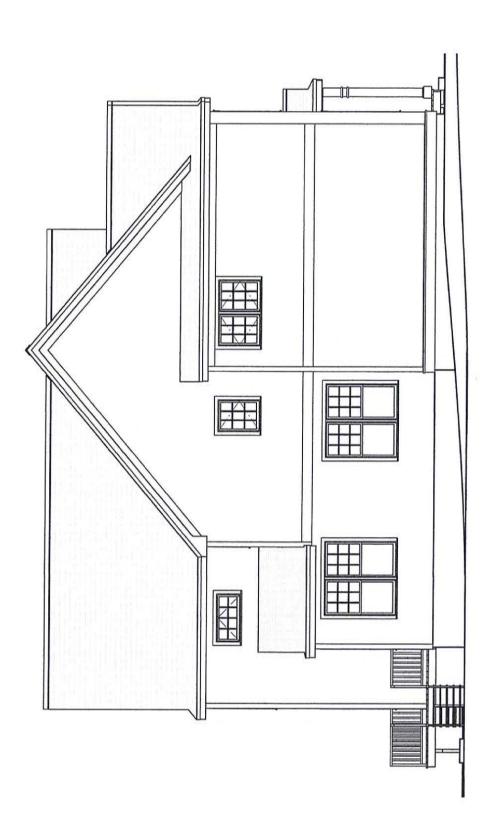
### Rear Elevation

Scale: 1/8" = 1'-0"

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### Left Elevation Scale: 1/8" = 1'-0"

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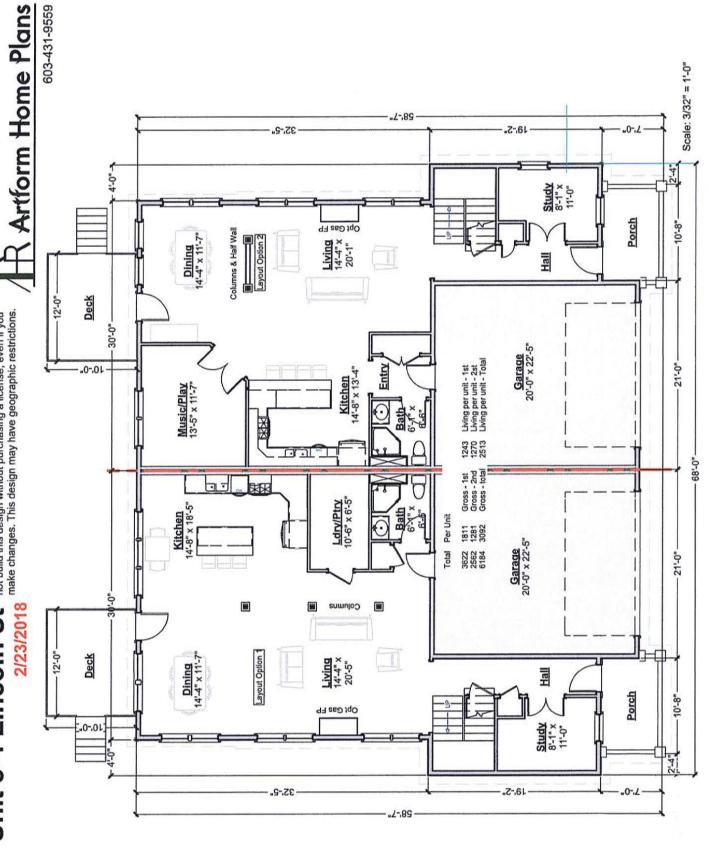
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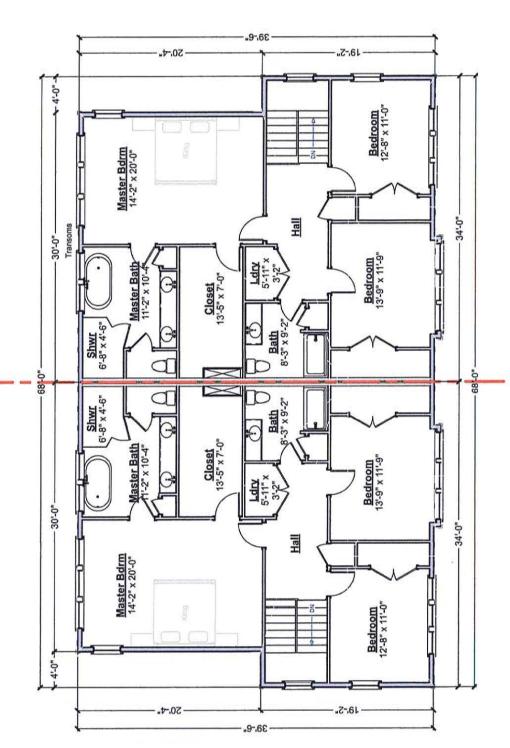
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R Artform Home Plans

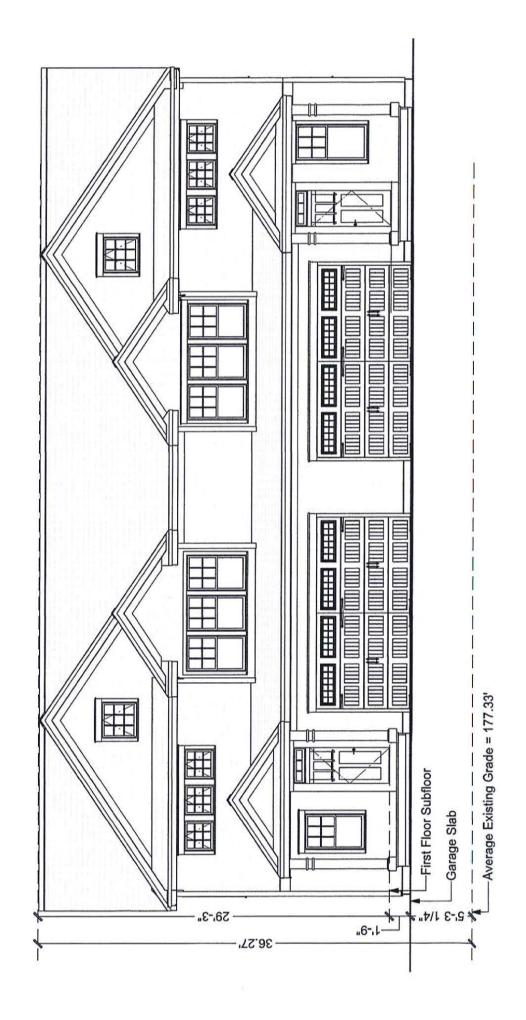
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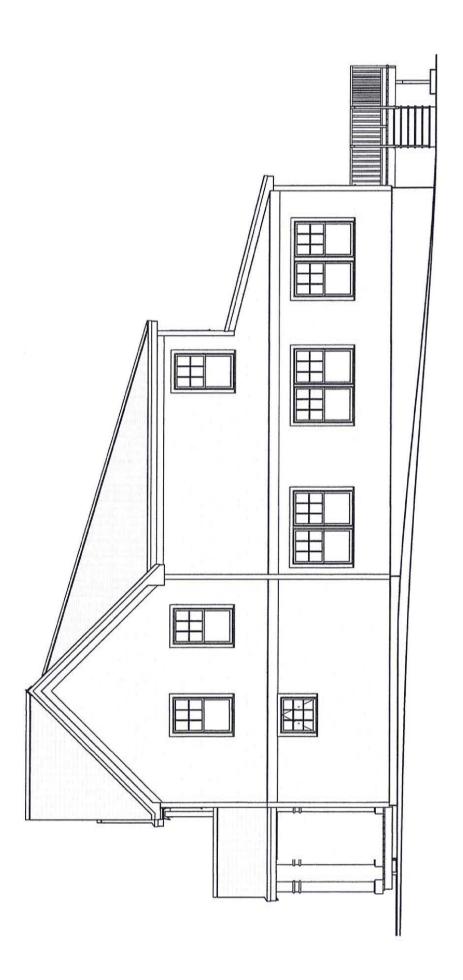
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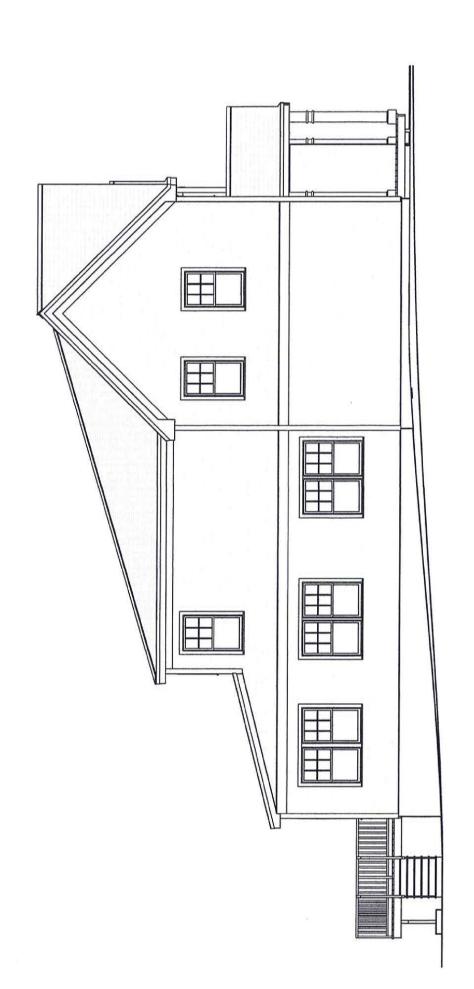




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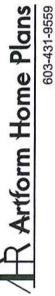
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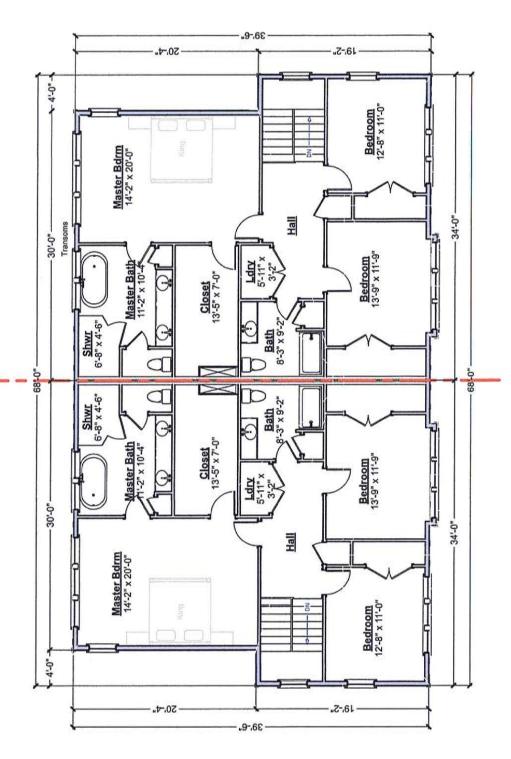
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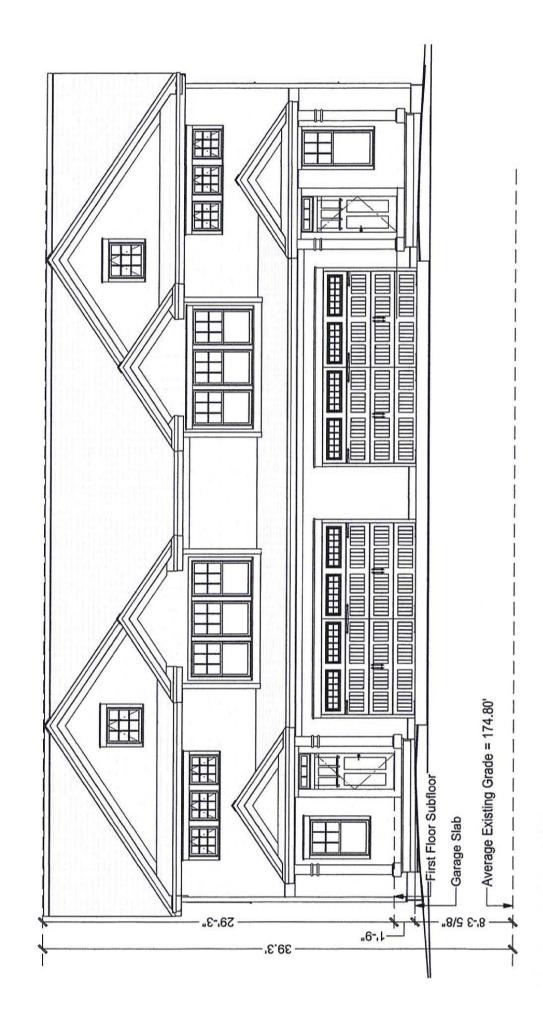


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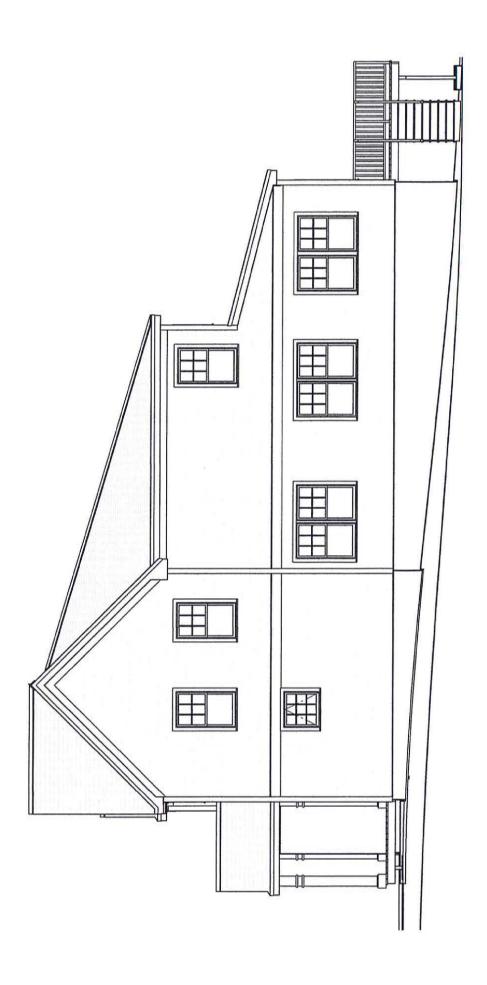
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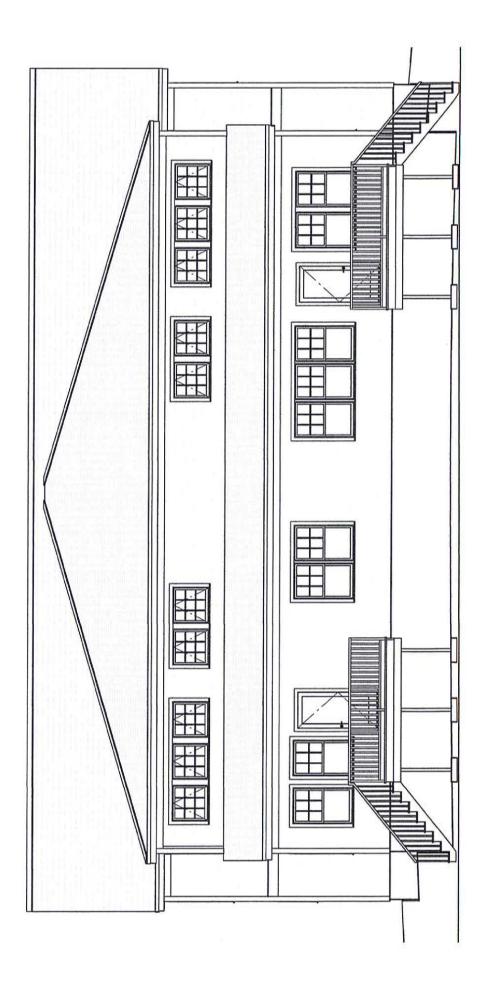
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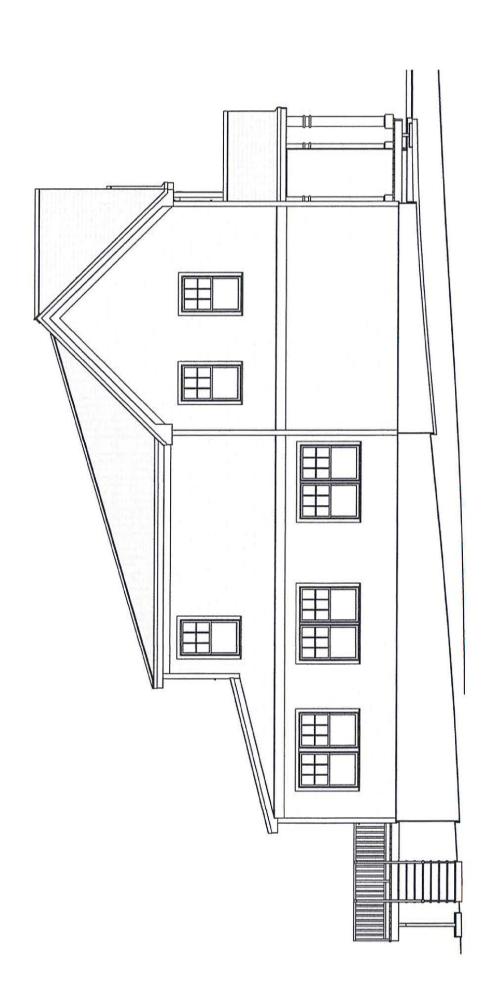




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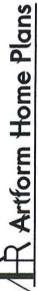


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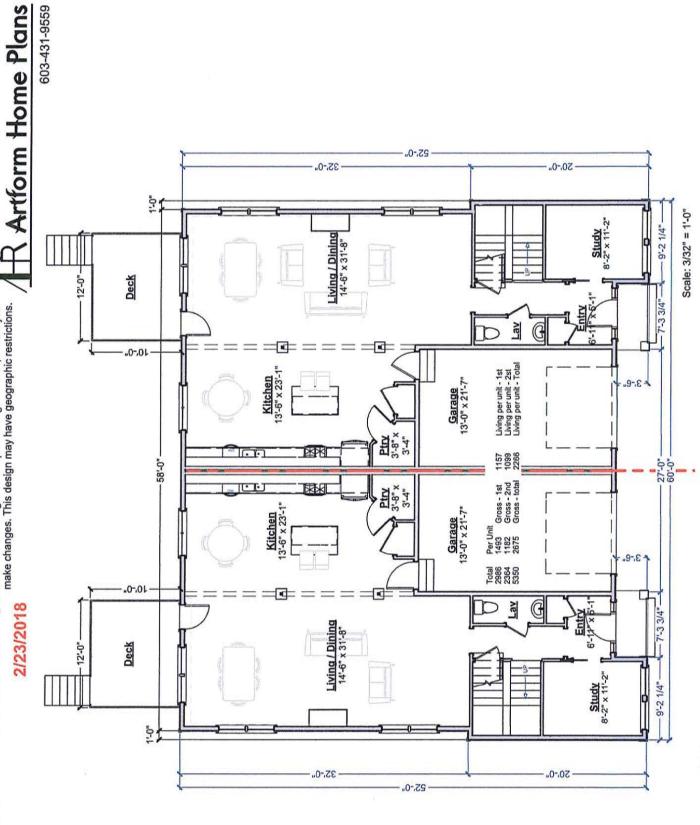
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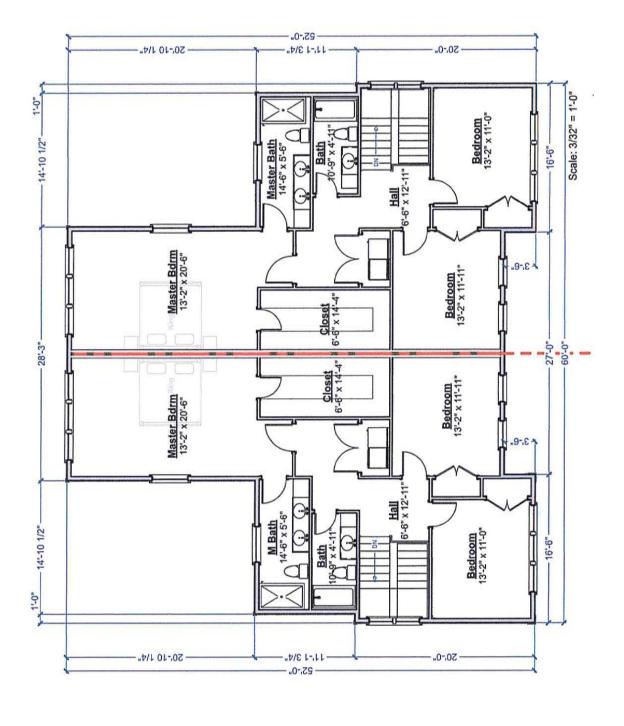


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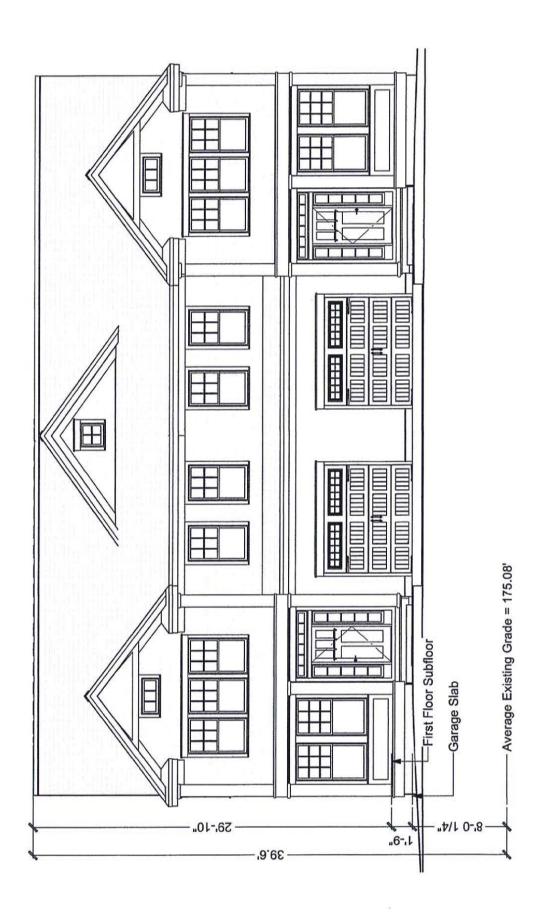
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Artform Home Plans

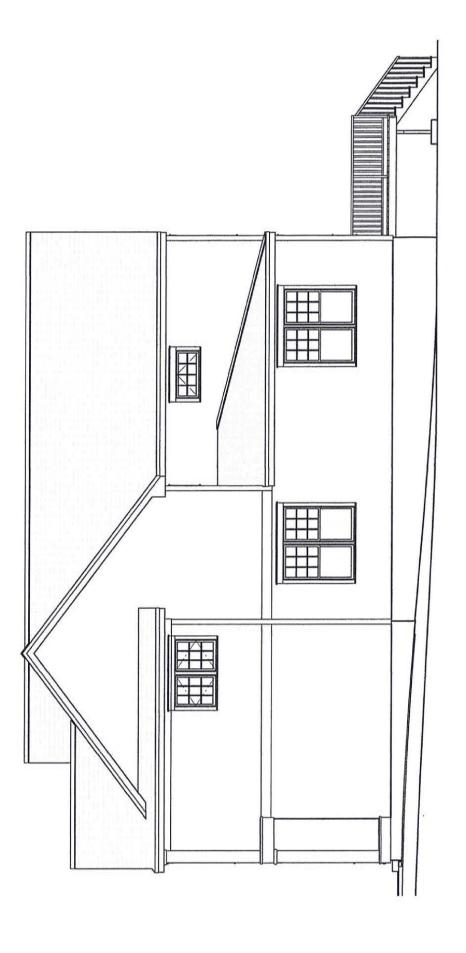






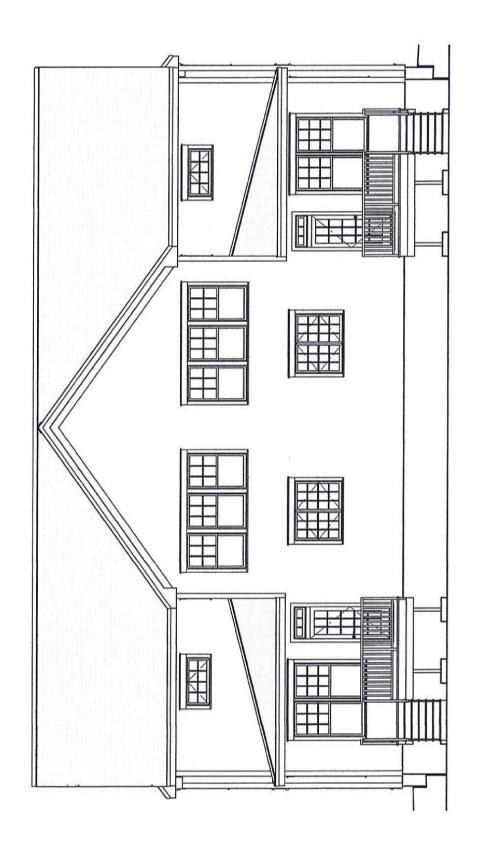
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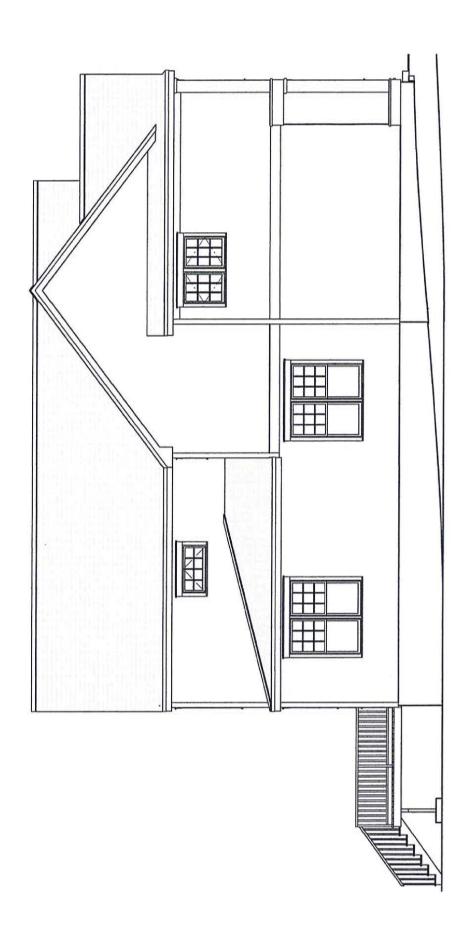




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2/23/2018







### HOMES AT HOBBS BROOK LANDSCAPE MAINTENANCE PLAN

### General

The Condominium Association (CA) shall be responsible for the maintenance of all landscaped open space, natural screens, and constructed screens within the property. Landscaping shall be maintained in good condition such that planting shall be vigorous and in good health at all times and that the parcel shall present a healthy, neat, and orderly appearance, free from refuse and debris.

### **Integrated Turf Management Plan**

Maintenance of lawn areas shall generally consist of watering, weeding, mowing and edging, replacement of dead sod, disease and insect control, repair of erosion, and any and all procedures consistent with good horticultural practice, as necessary to insure normal, vigorous and healthy growth of grass,

The CA shall provide the following maintenance activities as specified:

- Mowing: Once a week or more often as conditions warrant.
- Watering: by natural rainfall after establishment period. Seed to be kept moist during establishment period.
- 3. Fertilizing: Early spring and fall.
- Weeding: Once or twice a year.
- Pest and Disease Control: Only as needed
- De-thatching: spring and fall.
- Liming: Once a year, in the fall and as soil tests indicate need.
- 8. Raking, edging, debris removal, sod replacement, erosion repair: As needed.
- Soil testing shall be performed once every 3 years or more frequent if conditions warrant. Soil shall be amended as indicated by test for turf grass.
- 10. Lawns shall be aerated annually during late summer or early fall. Thinning lawns shall be over-seeded with a certified general turf blended seed mix and top-dressed with a compost/sand mixture ¼-1/2" in the late summer and early fall.

- Soil and seed shall be kept moist during seed establishment period. Late summer/early fall application of seed is preferable.
- Turf fertilizer (slow release) shall be applied mid to late fall according to recommended rates
  in coordination with Cambridge Water Dept. / Reservoir guidelines.
- Weeds shall be mechanically removed from the site as feasible and disposed of in a legal manner.
- 14. Grass clippings shall be left on turf areas using mulching mowers. Mowing patterns shall be alternated to avoid ruts and compaction. Care shall be taken to avoid damage to lawn areas.

### Shrub and Groundcover Management

The CA shall provide the following shrub and maintenance activities as specified:

- Mulching: Once each year in spring. Mulch shall be 2"-3" maximum depth and shall always
  be kept pulled 2"-3" away from tree trunk. Mulch shall be shredded bark, 100% organic and
  be free of any disease, pests, and insects. Mulch may be applied by manual or mechanical
  methods where appropriate.
- Weeding: Once or twice a year as needed. Weeds shall be removed and disposed of off site in a legal manner.
- Watering: weekly minimum during the establishment period. Long term watering typically only warranted by severe weather conditions.
- Pruning: To include cleaning, raising and reduction, spring to fall, dependent on accepted practice for each particular species.
  - Preventative pest/disease management: Avoid shrubs and groundcover known to be susceptible to various pests. Establish pest thresholds prior to treatment with acceptable pesticides. Pesticide application to be performed by certified applicator. See tree pest management below.
  - Fertilizer shall be phosphorus free.
  - 7. Once established, plantings shall be watered by natural rainfall. During excessive drought periods watering by hand or drip irrigation bags may be required.
  - 8. Shrubs shall be pruned in accordance with generally accepted standards for proper pruning. Shrubs shall be pruned to remove branches that are dead, broken, extending beyond the face of curbs (where applicable). Shrubs shall not be sheared into topiary shapes.

Known invasive plants shall be identified, removed from site as practicable, and disposed of in a legal manner.

### Tree Management

The CA shall provide the following tree maintenance activities as specified:

- Risk Management: this includes management of existing trees to minimize risk of tree failure and possible damage or injury. This includes:
  - Removal of trees that show significant decline or serious defects in their structure.
  - Hazard pruning to remove a dead or broken portion of the tree.
- Pruning: These include three different types of pruning as defined by the American National Standard for Tree Operations: Tree, <u>Shrub and Other Woody Plant Maintenance - Standard</u> Practices.
  - Crown Cleaning selective pruning to remove one or more of the following parts: dead, diseased, and/or broken branches
  - Crown Raising selective pruning to provide vertical clearance
  - Crown Reduction selective pruning to decrease height and/or spread
- 3. Mulching: Once each year In spring. Mulch shall be 2"-3" maximum depth and shall always be kept pulled 2"-3" away form tree trunk. Mulch shall be shredded bark, 100% organic and be free of any disease, pests, and insects. Mulch may be applied by manual or mechanical methods where appropriate.
- Pest and Disease Control: Only as needed. Dead or diseased branches shall be removed and disposed of off site in a legal manner.
- Watering: weekly minimum during the establishment period. Long term shall be by natural rainfall. During excessive drought periods watering by hand or drip irrigation bags may be required.
- Fertilization: early spring or fall. Formulation shall depend on soil test recommendations and plant variety. Granular type fertilizer to be used and watered in.
- Soil additives: Only as needed.
- Root crown excavation: This is required where excessive soil or mulch has been placed over the base of the tree.
- Only trees on slopes 2:1 or greater shall be staked. Stakes shall be removed after first growing season.
- 10. Preventative pest/disease management: Avoid trees known to be susceptible to various pests. Establish acceptable pest thresholds. Once monitoring, identification, and action thresholds indicate that pest control is required, and preventive methods are no longer effective or available, evaluate the proper control method both for effectiveness and risk. Effective, less risky pest controls are chosen first, including highly targeted chemicals, such as pheromones

to disrupt pest mating, or mechanical control, such as trapping or weeding. If further monitoring, identifications and action thresholds indicate that less risky controls are not working, then additional pest control methods would be employed, such as targeted spraying of pesticides. Broadcast spraying of non-specific pesticides is a last resort. Pesticides, if required, to be applied by a certified applicator.

- Replacement Trees: CA shall replace dead or missing trees according to the following:
  - Lost, dead or diseased trees shall be replaced with the same or similar species.
  - New trees shall be 3" in caliper for shade trees and to 2" in caliper for ornamental trees.

### Watering during establishment period

Water source shall consist of local water supply systems. At a minimum trees and shrubs shall be watered by flooding as follows:

Month 0-3: Once per week

Month 3-6: Twice per month

Month 6-12: Once per month.

Watering frequency may be increased or decreased depending upon excessive rainfall or drought conditions.

### Seasonal Maintenance

The CA shall maintain a plan for seasonal activities including raking, de thatching, removal of dead brush and flowers, fertilizing, watering, pruning, mowing, weeding, etc. for each of the following:

- 1. Spring Clean-up Plan
- 2. Fall Clean-up Plan
- 3. Leaf & Plant Debris Disposal
- 4. Winter Plowing: Prior to the start of each winter season, curb lines and planting beds should be stacked out with brightly colored wooden stakes to demarcate edges. Snow storage will be in designated open areas adjacent to parking and walks. During periods of extreme snowfall, portions of the common area may be utilized for storage of snow. Springtime cleanup will typically include repair of any turf damage related to plowing operations.
- Winter Deicing Plan: Minimize de-icing per Cambridge Water Dept. Guidelines. Mix 80% sand with calcium chloride for deicing.

### **Stormwater Management Permit Application**

For

Homes at Hobbs Brook 443 Lincoln Street Map 35 Parcel 2 Lexington, MA

February 20, 2018

Applicant:

Symes Development and Permitting, LLC.

50 Dodge Street Beverly, MA 01915

Owner:

The Gertrude M. Piantedosi Trust

443 Lincoln Street Lexington, MA 02421

Stamski And McNary, Inc. Engineering - Planning – Surveying 1000 Main Street; Acton, MA 01720 (978) 263-8585

SM-5676

File: 5676 SW Report Cover & TOC.doc

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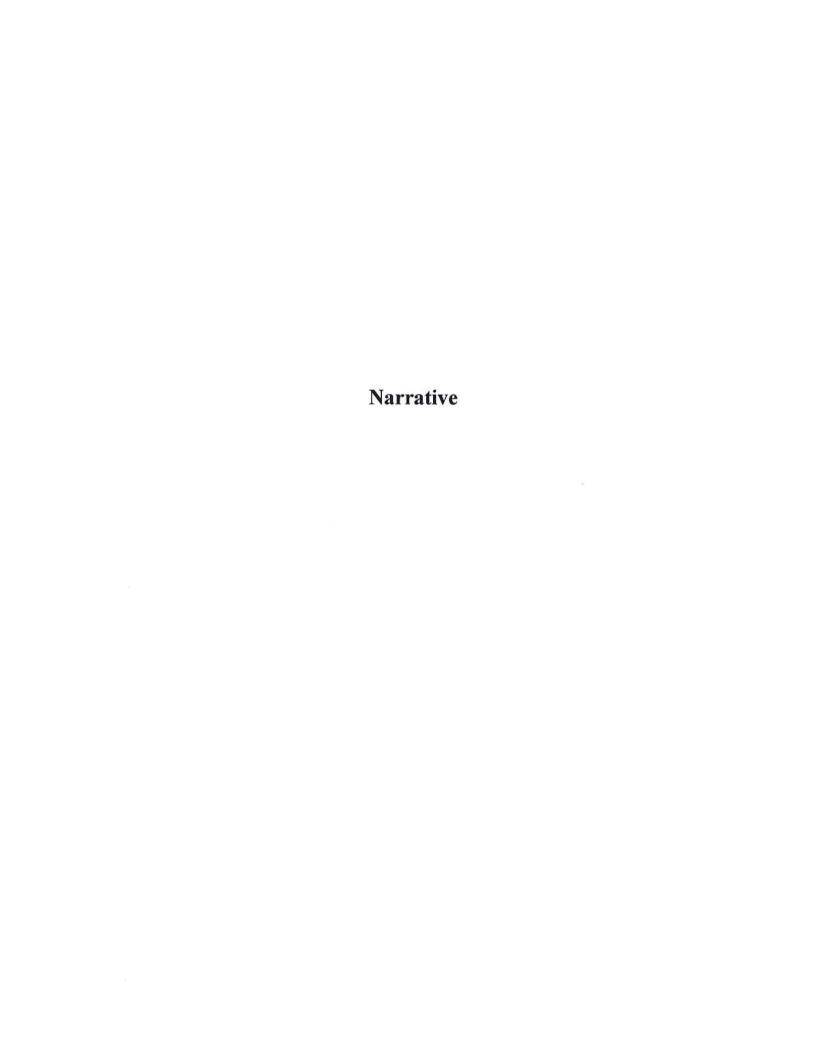
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### Stormwater Management

The proposed project is for an 8 unit Balanced Housing Development at 443 Lincoln Street.

### Pre Development

The existing site is approximately 4.13 ac and contains an existing dwelling and mechanics shop, a land use with higher potential pollutant loads, with associated gravel drive and paved areas. An existing cleared utility easement is present on the property. The site has been divided into 3 subcatchments as shown on the attached drainage map.

Subcatchment E-1 contains a portion of the existing dwelling, associated concrete patios, lawn, and brush vegetative cover within the utility easement. Subcatchment E-2 contains the existing mechanics shop, gravel drive, and some paved area; the vegetative cover is lawn and brush within the majority of the utility easement. Subcatchment E-3 is located on the western portion of the lot and is comprised of brush vegetative cover.

### Post Development

The proposed work is to remove the existing dwelling, service shop, and appurtenances and construct a cluster development containing 4 two-family dwellings. The proposed subcatchments are shown on the attached drainage map.

Subcatchment P-1 is located along the south side of the lot along the Lincoln Street right-of-way (ROW); the subcatchment compares to Subcatchment E-1. The subcatchment is entirely vegetated with brush and lawn. The subcatchment will be allowed to drain to the Lincoln Street ROW.

Subcatchment P-2A consists of the entirety of the paved area and area surrounding the proposed dwellings, up to the eastern lot line. Paved surface runoff will be captured by three catch basins and diverted to an infiltration basin containing a sediment forebay on the North side of the property.

Subcatchment P-2B comprises the largest portion of the site. The subcatchment surface area will be primarily brush with a smaller portion of grass cover. Runoff from the subcatchment will discharge to Hobbs Brook beyond the Northern property line, similarly to existing conditions within Subcatchment E-2.

Subcatchment P-3 is comprised of a small portion of the site along the Western lot line. This subcatchment is identical to Subcatchment E-3. No permanent disturbance is proposed within this subcatchment.

In accordance with the Town of Lexington Regulations, Chapter 181-73.A, Standards 1 through 10 of the Massachusetts Department of Environmental Protection Stormwater Management Standards have been met. In addition, the system design will not result in a

serious flood hazard during the 100-year storm event. The peak runoff rates have been summarized in the following tables.

### Compliance with MA DEP Stormwater Management Standards

Compliance with the Stormwater Management Standards is as follows:

### Standard 1: No Untreated Discharges

No untreated discharges to wetlands are proposed. Additional runoff from the site is to be treated with a sediment forebay and infiltrated in an infiltration basin. Roof runoff will be treated by roof drywells. Additional pervious paver areas are proposed for select parking spaces.

### Standard 2: Peak Rate Attenuation

The Post-Development peak discharge rates must not be increased from pre-development rates for the 1-year, 2-year, 10-year, and 100-year storm events. Also, offsite flood impact from the 100-year storm must not be increased. With a combination of infiltration and detention, the peak runoff rate and volume have been decreased. The peak runoff rates have been summarized in the following tables.

### **Discharge Summary Tables**

### Total Runoff - Subcatchment 1

1-year	1-year Storm 2-year Storm		10-yea	r Storm	100-year Storm		
Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)
0.000	0.000	0.000	0.000	0.001	0.001	0.016	0.014

### Total Runoff - Subcatchment 2

1-year	1-year Storm 2-year Storm		10-yea	r Storm	100-year Storm		
Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)
0.000	0.000	0.000	0.000	0.018	0.003	0.284	0.054

### Total Runoff - Subcatchment 3

1-year	ar Storm 2-year Storm			10-yea	r Storm	100-year Storm	
Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)
0.000	0.000	0.000	0.000	0.000	0.000	0.005	0.005

### Standard 3: Stormwater Recharge

The infiltration structures have been sized to infiltrate the required recharge volume resulting from the increase in impervious area on the site as specified in the Massachusetts Stormwater Handbook. The "Simple Dynamic" method was used in sizing the required storage volume to infiltrate the recharging runoff. Calculations were performed to insure drawdown within 72 hours to provide storage for the next storm event. Detailed calculations showing compliance with Standard 3 have been attached to this report.

### Standard 4: Water Quality

The required water quality volume for this project is 1" of runoff over the impervious area for the infiltration. This volume will be treated to meet the 80% TSS removal requirement of Standard 4. The area treated is greater than the amount of increased impervious surface on the site. Calculations showing treatment levels are attached.

### Standard 5: Land Uses with Higher Potential Pollutant Loads

The site proposed will not contain "land uses with higher potential pollutant loads." The project will remove the land uses with higher pollutant loads.

### Standard 6: Critical Areas

The site discharges runoff to critical areas associated with the City of Cambridge Reservoir.

### Standard 7: Redevelopment

The proposed project is not redevelopment relative to stormwater compliance.

### **Standard 8: Construction Period Controls**

The erosion and sedimentation control measures will be followed in accordance with the requirements of the NPDES Construction General Permit. The project will require coverage under the NPDES Construction General Permit.

### Standard 9: Operation and Maintenance Plan

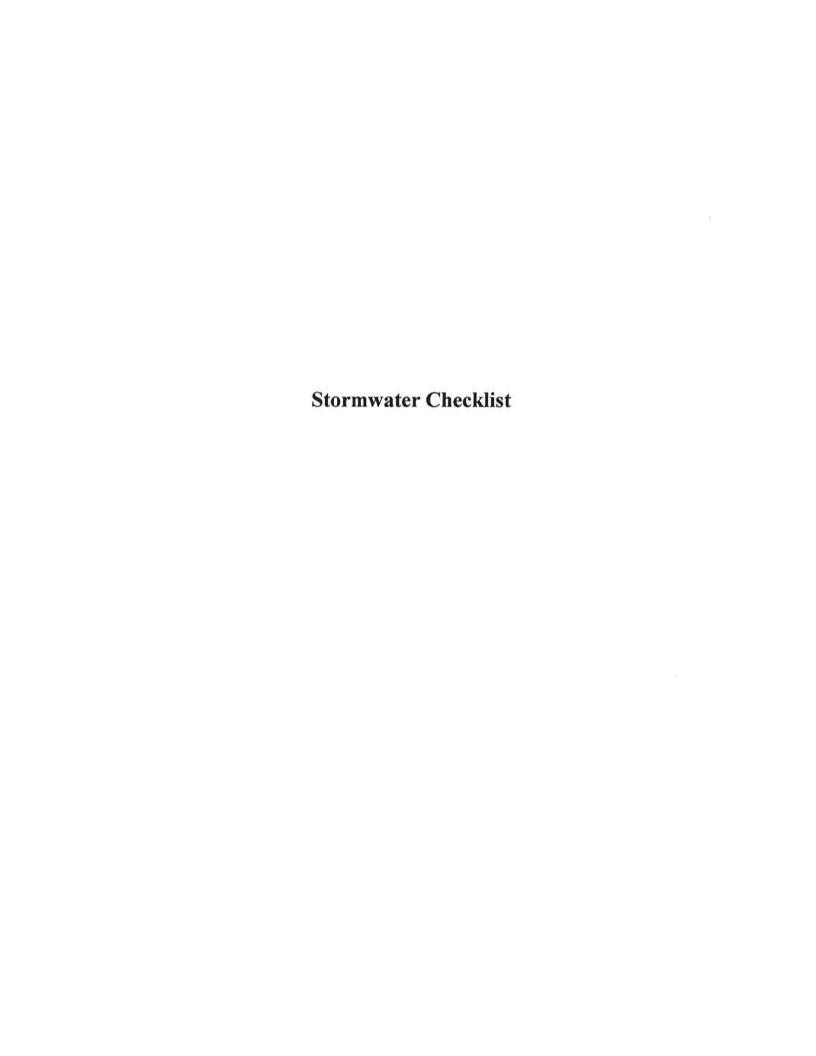
An Operation and Maintenance Plan is included in this report.

### Standard 10: Illicit Discharges to Drainage System

An Illicit Discharge Compliance will be provided prior to the discharge of stormwater runoff to the post-construction stormwater BMP's.

### **Design Basis**

- The United States Department of Agriculture Natural Resource Conservation Service (N.R.C.S.) TR55 methodology was used to determine offsite rates of runoff.
- 2. The twenty-four hour rainfall, taken from N.R.C.S. publications, is 6.4 inches for the 100-year storm, 4.5 inches for the 10-year storm, and 3.1 inches for the 2-year storm event.
- 3. The hydrologic calculations were performed using the computer program: "Hydraflow Hydrographs 2007" by Intelisolve.
- The soil types of the site were taken from the N.R.C.S. Soil Survey Map for Middlesex County.
- Soil conditions and estimated seasonal high groundwater table were based on on-site soil evaluations.
- 6. The Natural Resources Conservation Service (N.R.C.S.) soil survey indicated the presences of Scarboro mucky fine sandy loam, Charlton-Hollis-Rock outcrop, Windsor loamy sand, and Deerfield loamy sand. These soil groups rate as Hydrologic Group A, D, B, and B, respectively.





Bureau of Resource Protection - Wetlands Program

## **Checklist for Stormwater Report**

### A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.





A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.<sup>1</sup> This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8<sup>2</sup>
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

<sup>&</sup>lt;sup>1</sup> The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

<sup>&</sup>lt;sup>2</sup> For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



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## Checklist for Stormwater Report

### B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

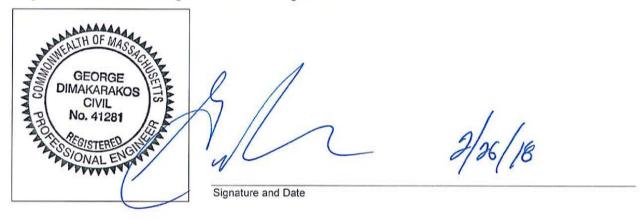
Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

### Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



### Checklist

	<b>pject Type:</b> Is the application for new development, redevelopment, or a mix of new and evelopment?
	New development
	Redevelopment
$\boxtimes$	Mix of New Development and Redevelopment



Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

### Checklist (continued)

en	• Measures: Stormwater Standards require LID measures to be considered. Document what vironmentally sensitive design and LID Techniques were considered during the planning and design of project:
	No disturbance to any Wetland Resource Areas
$\boxtimes$	Site Design Practices (e.g. clustered development, reduced frontage setbacks)
	Reduced Impervious Area (Redevelopment Only)
	Minimizing disturbance to existing trees and shrubs
	LID Site Design Credit Requested:
	Credit 1
	Credit 2
	☐ Credit 3
	Use of "country drainage" versus curb and gutter conveyance and pipe
	Bioretention Cells (includes Rain Gardens)
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
	Treebox Filter
	Water Quality Swale
	Grass Channel
	Green Roof
$\boxtimes$	Other (describe): Roof Drywells and Infiltration Basin
Sta	ndard 1: No New Untreated Discharges
$\boxtimes$	No new untreated discharges
$\boxtimes$	Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
$\boxtimes$	Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



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C	necklist (continued)	
Sta	ndard 2: Peak Rate Attenuation	
	Standard 2 waiver requested because the project is located in land subject to coastal storm flowar and stormwater discharge is to a wetland subject to coastal flooding.  Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.	•
$\boxtimes$	Calculations provided to show that post-development peak discharge rates do not exceed pre- development rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24 hour storm.	
Sta	ndard 3: Recharge	
$\boxtimes$	Soil Analysis provided.	
$\boxtimes$	Required Recharge Volume calculation provided.	
	Required Recharge volume reduced through use of the LID site Design Credits.	
$\boxtimes$	Sizing the infiltration, BMPs is based on the following method: Check the method used.	
	☐ Static ☐ Simple Dynamic ☐ Dynamic Field <sup>1</sup>	
$\boxtimes$	Runoff from all impervious areas at the site discharging to the infiltration BMP.	
	Runoff from all impervious areas at the site is <i>not</i> discharging to the infiltration BMP and calculation are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient generate the required recharge volume.	
$\boxtimes$	Recharge BMPs have been sized to infiltrate the Required Recharge Volume.	
	Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximun extent practicable for the following reason:	n
	☐ Site is comprised solely of C and D soils and/or bedrock at the land surface	
	☐ Solid Waste Landfill pursuant to 310 CMR 19.000	
	Project is otherwise subject to Stormwater Management Standards only to the maximum exterpracticable.	nt
$\boxtimes$	Calculations showing that the infiltration BMPs will drain in 72 hours are provided.	
	Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included	.k

<sup>&</sup>lt;sup>1</sup> 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Bureau of Resource Protection - Wetlands Program

## **Checklist for Stormwater Report**

Check	list (	(continued)	۱
OHOOK	100	continuca)	1

### Standard 3: Recharge (continued)

$\boxtimes$	The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
П	Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland

### Standard 4: Water Quality

resource areas.

The Long-Term Pollution Prevention Plan typically includes the following:

- · Good housekeeping practices;
- · Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
  - is within the Zone II or Interim Wellhead Protection Area
  - is near or to other critical areas
  - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
  - involves runoff from land uses with higher potential pollutant loads.
- ☐ The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- ☐ Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



# Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program

C	hecklist (continued)
Sta	andard 4: Water Quality (continued)
$\boxtimes$	The BMP is sized (and calculations provided) based on:
	☐ The ½" or 1" Water Quality Volume or
	The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
	The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
$\boxtimes$	A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Sta	ındard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
	The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.  The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prior to</i> the discharge of stormwater to the post-construction stormwater BMPs.
	The NPDES Multi-Sector General Permit does <i>not</i> cover the land use.
	LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
	All exposure has been eliminated.
	All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
	The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.
Sta	ndard 6: Critical Areas
$\boxtimes$	The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
$\boxtimes$	Critical areas and BMPs are identified in the Stormwater Report.



# Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program

C	hecklist (continued)
	andard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum tent practicable  The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:
	☐ Limited Project
	<ul> <li>Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.</li> <li>Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area</li> <li>Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff</li> </ul>
	☐ Bike Path and/or Foot Path
	Redevelopment Project
	Redevelopment portion of mix of new and redevelopment.
	Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report. The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.
Sta	andard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control
	Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the owing information:
	<ul> <li>Narrative;</li> <li>Construction Period Operation and Maintenance Plan;</li> <li>Names of Persons or Entity Responsible for Plan Compliance;</li> <li>Construction Period Pollution Prevention Measures;</li> <li>Erosion and Sedimentation Control Plan Drawings;</li> <li>Detail drawings and specifications for erosion control BMPs, including sizing calculations;</li> <li>Vegetation Planning;</li> <li>Site Development Plan;</li> <li>Construction Sequencing Plan;</li> <li>Sequencing of Erosion and Sedimentation Controls;</li> <li>Operation and Maintenance of Erosion and Sedimentation Controls;</li> <li>Inspection Schedule;</li> <li>Maintenance Schedule;</li> <li>Inspection and Maintenance Log Form.</li> </ul>
	A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



# Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program

C	hec	cklist (continued)
		ard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control
	it is Sec	e project is highly complex and information is included in the Stormwater Report that explains why is not possible to submit the Construction Period Pollution Prevention and Erosion and dimentation Control Plan with the application. A Construction Period Pollution Prevention and posion and Sedimentation Control has <i>not</i> been included in the Stormwater Report but will be pomitted <i>before</i> land disturbance begins.
	The	e project is <i>not</i> covered by a NPDES Construction General Permit.
	Sto	e project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the ormwater Report.  e project is covered by a NPDES Construction General Permit but no SWPPP been submitted.
-		e SWPPP will be submitted BEFORE land disturbance begins.
Sta	ında	ard 9: Operation and Maintenance Plan
$\boxtimes$		e Post Construction Operation and Maintenance Plan is included in the Stormwater Report and ludes the following information:
	$\boxtimes$	Name of the stormwater management system owners;
	$\boxtimes$	Party responsible for operation and maintenance;
	$\boxtimes$	Schedule for implementation of routine and non-routine maintenance tasks;
	$\boxtimes$	Plan showing the location of all stormwater BMPs maintenance access areas;
	$\boxtimes$	Description and delineation of public safety features;
	$\boxtimes$	Estimated operation and maintenance budget; and
	$\boxtimes$	Operation and Maintenance Log Form.
		e responsible party is <b>not</b> the owner of the parcel where the BMP is located and the Stormwater port includes the following submissions:
		A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
		A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.
Sta	nda	rd 10: Prohibition of Illicit Discharges
	The	Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
	An	Illicit Discharge Compliance Statement is attached;
$\boxtimes$		Illicit Discharge Compliance Statement is attached but will be submitted <i>prior to</i> the discharge of stormwater to post-construction BMPs



## **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisolve v9.2

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	0.000	2	n/a	o	ş <del></del> s	a <del>nanc</del> a		Sub. E-1
3	SCS Runoff	0.000	2	n/a	0	-			Sub. E-2
5	SCS Runoff	0.000	2	n/a	0	-			Sub. E-3
7	SCS Runoff	0.000	2	n/a	o				Sub. P-1
9	SCS Runoff	0.036	2	748	525			<u>4700.0030</u>	Sub. P-2A
10	Reservoir	0.000	2	760	0	9	174.81	23.4	Infil. Basin-1
12	SCS Runoff	0.000	2	n/a	0	-			Sub. P-2B
14	SCS Runoff	0.000	2	n/a	0				Sub. P-3
16	SCS Runoff	0.164	2	724	548		12/6/17/19		Dwelling A
17	Reservoir	0.065	2	736	548	16	176.56	67.4	Drywell A
19	SCS Runoff	0.213	2	724	710		<u> </u>	(40000000)	Dwellings B&C
20	Reservoir	0.082	2	736	710	19	176.59	91.3	Drywells B&C
22	SCS Runoff	0.177	2	724	591		**********	sant saves an	Dwelling D
23	Reservoir	0.066	2	736	591	22	176.61	78.9	Drywell D
5676	3 Drainage.g	pw			Return P	eriod: 1 Ye	ear	Friday, Feb	23, 2018

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	0.000	2	n/a	0	-	3 <del>11111</del> 1		Sub. E-1
3	SCS Runoff	0.000	2	n/a	0		( <del>1200-1</del> )		Sub. E-2
5	SCS Runoff	0.000	2	n/a	0	_			Sub. E-3
7	SCS Runoff	0.000	2	n/a	0				Sub. P-1
9	SCS Runoff	0.127	2	740	1,083	\ <u></u> >			Sub. P-2A
10	Reservoir	0.000	2	786	0	9	174.83	87.2	Infil. Basin-1
12	SCS Runoff	0.000	2	n/a	0	<del></del>			Sub. P-2B
14	SCS Runoff	0.000	2	n/a	0				Sub. P-3
16	SCS Runoff	0.197	2	724	664				Dwelling A
17	Reservoir	0.068	2	738	664	16	176.71	97.7	Drywell A
19	SCS Runoff	0.255	2	724	859				Dwellings B&C
20	Reservoir	0.087	2	738	859	19	0.74	131	Drywells B&C
22	SCS Runoff	0.213	2	724	715				Dwelling D
23	Reservoir	0.070	2	740	715	22	176.78	113	Drywell D
5676	Drainage.g	pw			Return P	eriod: 2 Ye	ear	Wednesday	y, Feb 21, 2018

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	0.001	2	1324	9	-			Sub. E-1
3	SCS Runoff	0.018	2	1324	322				Sub. E-2
5	SCS Runoff	0.000	2	n/a	0				Sub. E-3
7	SCS Runoff	0.001	2	1324	9	-			Sub. P-1
9	SCS Runoff	0.768	2	728	3,416		-		Sub. P-2A
10	Reservoir	0.000	2	750	0	9	174.96	444	Infil. Basin-1
12	SCS Runoff	0.003	2	1326	30	-			Sub. P-2B
14	SCS Runoff	0.000	2	n/a	0	****			Sub. P-3
16	SCS Runoff	0.288	2	724	987				Dwelling A
17	Reservoir	0.080	2	742	987	16	177.16	193	Drywell A
19	SCS Runoff	0.373	2	724	1,277		-		Dwellings B&C
20	Reservoir	0.102	2	744	1,277	19	1.21	255	Drywells B&C
22	SCS Runoff	0.311	2	724	1,064				Dwelling D
23	Reservoir	0.083	2	744	1,064	22	177.29	217	Drywell D
5676	6 Drainage.g	pw		- 200 HE STATE	Return P	eriod: 10 \	Year	Wednesda	y, Feb 21, 2018

# **Hydrograph Summary Report**

Hydraflow Hydrographs by Intelisolve v9.2

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	0.016	2	820	415	s <del></del>			Sub. E-1
3	SCS Runoff	0.284	2	744	3,639	1 <del></del>	(		Sub. E-2
5	SCS Runoff	0.005	2	902	131				Sub. E-3
7	SCS Runoff	0.014	2	818	373				Sub. P-1
9	SCS Runoff	2.108	2	728	7,847	_			Sub. P-2A
10	Reservoir	0.000	2	722	0	9	175.39	1,864	Infil. Basin-1
12	SCS Runoff	0.054	2	822	1,405	-			Sub. P-2B
14	SCS Runoff	0.005	2	902	131				Sub. P-3
16	SCS Runoff	0.411	2	724	1,426				Dwelling A
17	Reservoir	0.100	2	746	1,426	16	178.01	328	Drywell A
19	SCS Runoff	0.532	2	724	1,845				Dwellings B&C
20	Reservoir	0.132	2	744	1,845	19	2.12	428	Drywells B&C
22	SCS Runoff	0.443	2	724	1,537				Dwelling D
23	Reservoir	0.108	2	746	1,537	22	178.33	362	Drywell D
5676	B Drainage.g	pw			Return P	eriod: 100	Year	Wednesday	y, Feb 21, 2018

Worksheet	2: Runoff	curve number	and runoff

D-2

SM-5676

Project:	443 Lincoln St	By PFK	Date	1/12/18	_		
Location:	Lexington, MA Check	ed	Date		37 20		
Circle one:	Present Developed Subcat	chment E-1			<u> </u>		
1. Runoff curve n	umber (CN)						
Soil name and hydrologic	Cover description (cover type, treatment, and			CN 1/		Area	Product of CN x Area
group (appendix A)	hydrologic condition: percent impervious: unconnected/connected impervious area ratio)	,	Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
×	Impervious - Drive	0	98	8) (	929200	0.00	0.00
(*)	Impervious - Building	o	98	o (15%)	PS I SU	0.00	0.00
А	Woods and Brush Good Condition	18,788	30	Book!	10000	0.43	12.94
А	Open Space Good Condition	6,605	39	(No.)	penny	0.15	5.91
			Jeder I	EK-SAS	stryttl.	io in the la	
			dans	nipę, są	NI DESTR	Regar	
				restrat	sacris	NU SI	
			Party.	Blistin/	nectific	212	
1/ Use only one C	N source per line.				Totals =	0.58	18.85
CN	(weighted) = total product = 18.85 total area 0.58		32.34	; Use	ON =	32.3	 ]
2. Runoff	Storm #1 Storm #2	Storm #3					
Frequency	yr ///2/////10//	3(0)111113					
Rainfall, P (24-hou	in (13.1) (14.5)	17:17:6:4/17					
	in 0.06 0.00 th table 2-1, fig. 2-1,)	0.21					
	cf 125 10 (210-VI-TR-55, Second	449 Ed., June 1986)	)				

SM-5676

D-3

Project:	443 Lincoln St	_	Ву	PFK	Date	1/9/2018	_
Location:	Lexington, MA	_	Checked		Date		
Circle one: Circle one:	Present Developed Tc Tt	through subarea	Subcatchi	ment E-1	-		
Time of Co	ncentration 2						
Sheet flow (	Applicable to Tc only)		Segment ID	A-B	(PZ, KTPT)		1
1. Surface D	Description (table 3-1)			grass	PERMIT		
2. Mannings	roughness coeff., n (table 3-1)			0.4		SUCESAND.	
3. Flow leng	th, L (total L <= 300 ft)		ft	50	80% F 11%	Co.m. (1)	
4. Two-yr 24	-hr rainfall, P2		in	3.1	100000000		
5. Land Slop	pe, s		ft/ft	0.14		hi wa na	
6. Tt = 0.007	7 (nL)^0.8 / (P2^0.5 s^0.4)	Compute Tt	hr	0.10			0.10
Shallow con	centrated Flow		Segment ID	B-C	a side		
7. Surface D	escription (paved or unpaved)			UNPAVED			
8. Flow Leng	gth, L		ft	25		MESSA!	
9. Watercou	rse slope, s		ft/ft	0.07			
10. Average	Velocity, V (figure 3-1)		ft/s	4.27			
11. Tt = L / 3	8600V	Compute Tt	hr	0.00			0.00
Channel flow	/		Segment ID				
	ectional flow area, a perimeter, pw		sf ft				
Particular of Conference and Conference of C	c radius, r=a/wp	Compute r	ft				
15. Channel			ft/ft	MRELYE			
	's roughness coeff., n					sport of the	
	r^2/3 s^1/2 / n	Compute V	ft/s		2110/62/00		
18. Flow leng			ft		ETRICIE,		
19. Tt = L / 3	600V	Compute Tt	hr				0
20. Watersh	ed or subarea Tc or Tt (add Tt in step	s 6, 11, and	19)			hr min	0.10

(210-VI-TR-55, Second Ed., June 1986)

Hydraflow Hydrographs by Intelisolve v9.2

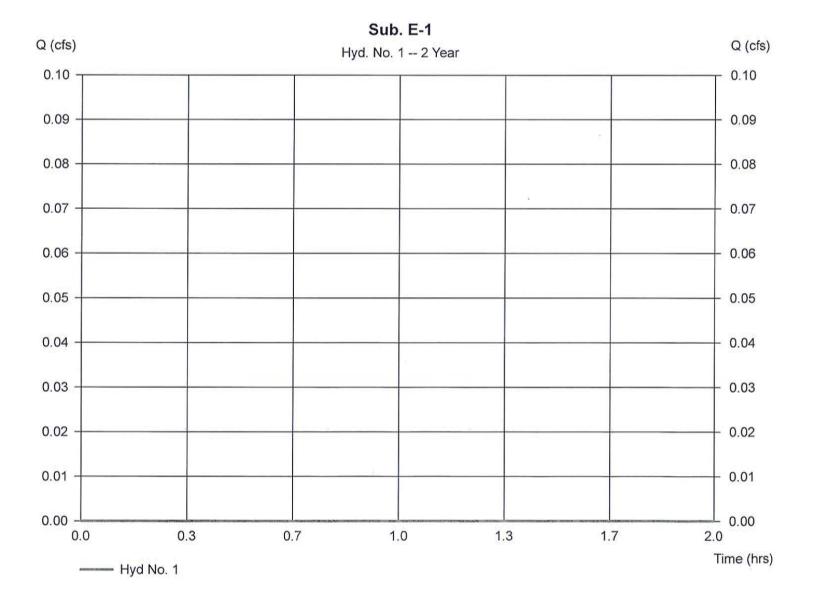
Tuesday, Jan 30, 2018

### Hyd. No. 1

Sub. E-1

Hydrograph type = SCS Runoff Storm frequency = 2 yrsTime interval = 2 min Drainage area = 0.580 acBasin Slope = 0.0 %Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.000 cfsTime to peak n/a Hyd. volume = 0 cuft Curve number = 32.3Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ Distribution = Type III Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

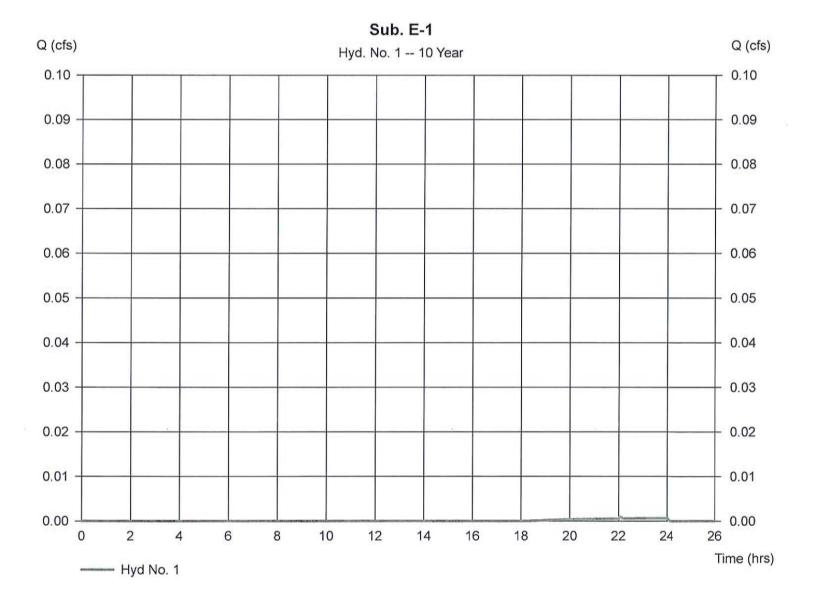
Tuesday, Jan 30, 2018

### Hyd. No. 1

Sub. E-1

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 min Drainage area = 0.580 acBasin Slope = 0.0 %Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.001 cfsTime to peak = 22.07 hrsHyd. volume = 9 cuft Curve number = 32.3Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ Distribution = Type III Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

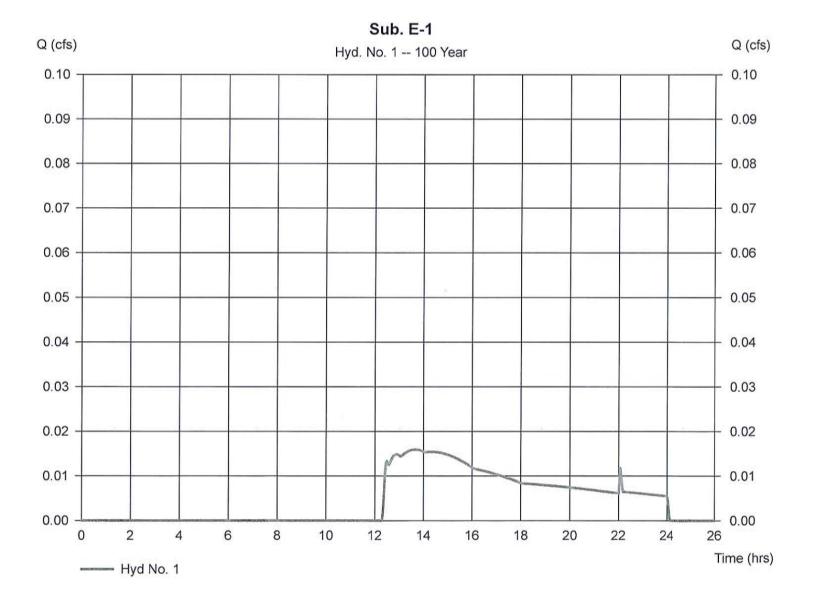
Tuesday, Jan 30, 2018

### Hyd. No. 1

Sub. E-1

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 0.580 acBasin Slope = 0.0 % Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 0.016 cfsTime to peak  $= 13.67 \, hrs$ Hyd. volume = 415 cuft Curve number = 32.3Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ Distribution = Type III Shape factor = 484



Project:	Worksheet 2: Runoff curve number and ru 443 Lincoln St	noff By PFK	Date	1/29/18		SM-5676	
Location:	Lexington, MA	Checked			=8		
Circle one:	Present Developed	Subcatchment E-2		0	70		
1. Runoff curve n	umber (CN)						
Soil name and hydrologic	Cover desc	CTLD COM		CN 1/		Area	Product of CN x Area
group (appendix A)	hydrologic co percent impe unconnected/connec area rat	ervious: cted impervious	Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
-	Impervious - Drive	o	98	golog	10000	0.00	0.00
*	Impervious - Building	o	98	elana)	decodu	0.00	0.00
A	Woods and Brush Good Condition	66,692	30	OF WA	The same of	1.53	45.93
Α	Open Space Good Condition	74,690	39	abeta	N. Palai	1.71	66.87
			indole	a State	10/10/1	nii hex	
		1		N 252531J	<b>JOSTITU</b>	jurus.	
			SUL D	estr	MADES	korija (v	
			V2"\	2775	SERVE AS	31.	
/ Use only one C	N source per line.				Totals =	3.25	112.80
1.736.02	(weighted) = total product = total area	112.80 = 3.25	34.75	; Use	WANW ETA	34.8	

		Storm #1	Storm #2	Storm #3
Frequency	yr	1113/11	11/10/11/1	1/100/
Rainfall, P (24-hour)	in	1773/07/	111/4:6/1/	1/6.4/
Runoff, Q (Use P and CN with table 2-1, fig. 2-1,) or eqs. 2-3 and 2-4.)	in	0.02	0.03	0.33
Runoff, Q	cf	279	335	3849

(210-VI-TR-55, Second Ed., June 1986)

SM-5676

D-3

Project: 443 Lincoln St	i .	Ву	PFK	Date	1/9/2018	
Location: Lexington, MA		Checked		Date		
Section Control of the Control of	through subarea	Subcatchi	ment E-2	-		
Time of Concentration 2						
Sheet flow (Applicable to Tc only)		Segment ID	A-B			
1. Surface Description (table 3-1)			grass			
2. Mannings roughness coeff., n (table 3-1)			0.4			
3. Flow length, L (total L <= 300 ft)		ft	50			
4. Two-yr 24-hr rainfall, P2		in	3.1		S and and	
5. Land Slope, s		ft/ft	No other			
6. Tt = 0.007 (nL)^0.8 / (P2^0.5 s^0.4)	Compute Tt	hr				0.00
Shallow concentrated Flow		Segment ID	B-C			
7. Surface Description (paved or unpaved)			UNPAVED			
3. Flow Length, L		ft	35.28	2 1 2 2 1 A 1	4 MARIE	
9. Watercourse slope, s		ft/ft	0.11			
10. Average Velocity, V (figure 3-1)		ft/s	5.35	O/W.	施設計響	
11. Tt = L / 3600V	Compute Tt	hr	0.00			0.00
Channel flow		Segment ID		A' I W		
12. Cross sectional flow area, a 13. Wetted perimeter, pw		sf	W 12 IX B9			
		ft	0 -0 1000		-655	
		ft				
15. Channel Slope, s	16	ft/ft	181. 34		1/1/18	
6. Manning's roughness coeff., n	2 29				in Maria	
	Compute V	1000 mm m			LECTE VIL	
8. Flow length, L		ft				
19. Tt = L / 3600V	Compute Tt	hr [				0
20. Watershed or subarea Tc or Tt (add Tt in steps	6, 11, and 1	19)		ŀ	nr nin	0.00

Hydraflow Hydrographs by Intelisolve v9.2

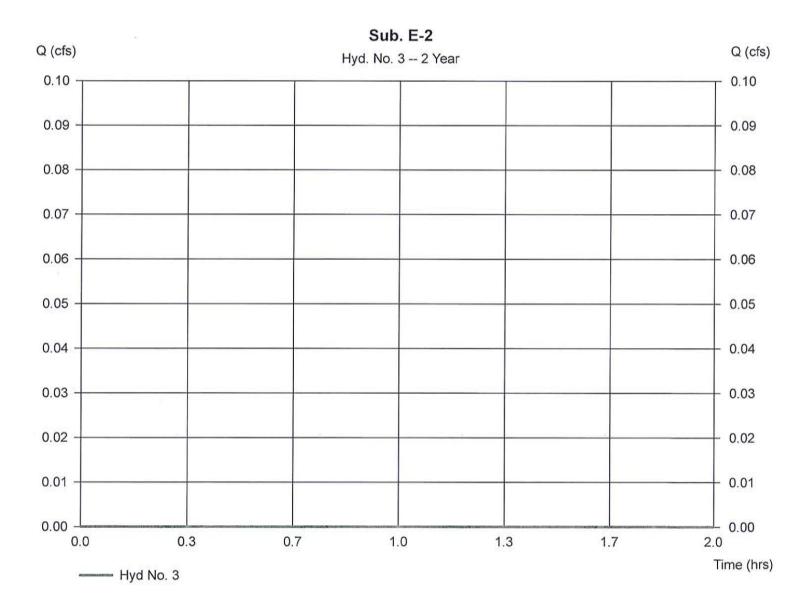
Tuesday, Jan 30, 2018

### Hyd. No. 3

Sub. E-2

Hydrograph type = SCS Runoff Storm frequency = 2 yrsTime interval = 2 min Drainage area = 3.250 acBasin Slope = 0.0 % Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.000 cfsTime to peak n/a Hyd. volume = 0 cuft Curve number = 34.8Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ Distribution = Type III Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

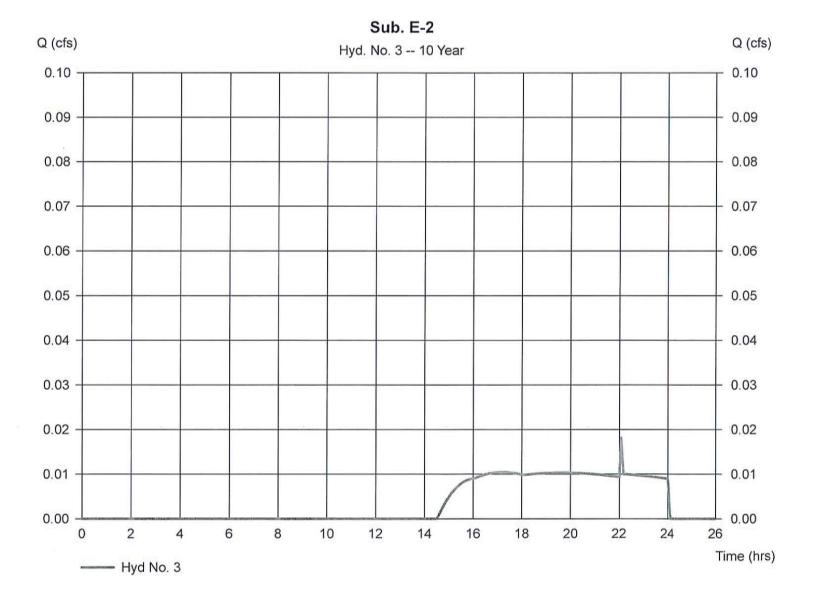
Tuesday, Jan 30, 2018

### Hyd. No. 3

Sub. E-2

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 min Drainage area = 3.250 acBasin Slope = 0.0 %Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.018 cfsTime to peak = 22.07 hrsHyd. volume = 322 cuft Curve number = 34.8Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ Distribution = Type III = 484 Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

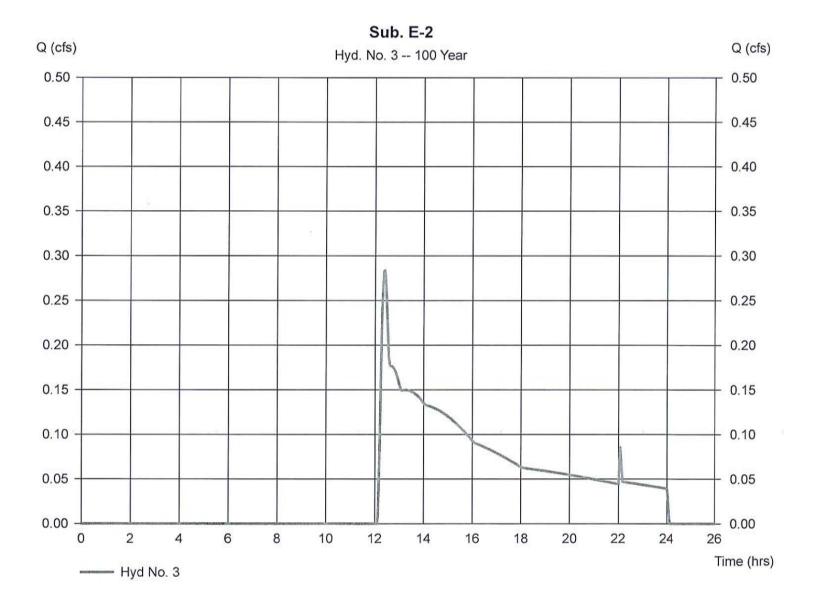
Tuesday, Jan 30, 2018

### Hyd. No. 3

Sub. E-2

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 3.250 acBasin Slope = 0.0 %Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 0.284 cfsTime to peak  $= 12.40 \, hrs$ Hyd. volume = 3,639 cuftCurve number = 34.8Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ Distribution = Type III Shape factor = 484



Project:	Worksheet 2: Runoff curve number and runo 443 Lincoln St	ff By PFK	Date	4/20/40		SM-5676	
Location:	Lexington, MA	244 11 2		1/29/18	2		
		Checked	Date		,		
Circle one:	Present Developed	Subcatchment E-3					
Runoff curve r	umber (CN)						
Soil name and hydrologic	Cover descripti (cover type, trealment, and	200		CN 1/		Area	Product of CN x Area
group (appendix A)	hydrologic condi percent impervic unconnected/connected area ratio)	ous:	Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
2	Impervious - Drive	0	98	A DESCRIPTION OF THE PERSON OF	311125717.	0.00	0.00
*	Impervious - Building	0	98	95.010	dista	0.00	0.00
Α	Woods and Brush Good Condition	13,225	30	otkayi	popper	0.30	9.11
Α	Open Space Good Condition	o	39	desto	33000	0.00	0.00
			strani	No.	bresti	danur	
			17,3/5/19	(COLUM	37,000	Djebal	
			1088	aki es	STREET	58 KG	
			QE PR		Datan.	3 F R P S	
1/ Use only one C	N source per line,				Totals =	0.30	9.11
CN	(weighted) = total product = total area	9.11 =	30.00	Use (	CN =	30.0	]
2. Runoff	479XXXXXX	Storm #2 Storm #3					

11/10

4.5

0.00

124 1 132 (210-VI-TR-55, Second Ed., June 1986)

100

6.4

0.12

Frequency.....

Rainfall, P (24-hour)....

Runoff, Q... (Use P and CN with table 2-1, fig. 2-1,) or eqs. 2-3 and 2-4.) Runoff, Q... D-2 уг

in

1/3:4/

0.11

SM-5676

7.3

D-3

min

Project: 443 Lincoln St		Ву	PFK_	Date	1/9/2018	_
Location: Lexington, MA		Checked	ı	Date		-
Part of a language and the form of the control of t	through subarea	Subcatch	ment E-3			
Time of Concentration 2						
Sheet flow (Applicable to Tc only)		Segment ID	A-B		merke.	
1. Surface Description (table 3-1)			grass		5 XED (1) ET	
2. Mannings roughness coeff., n (table 3-1)			0.4	My Jan	BJP, V	1
3. Flow length, L (total L <= 300 ft)		ft	50			1
4. Two-yr 24-hr rainfall, P2		in	3.1			
5. Land Slope, s		ft/ft	0.08			
6. Tt = 0.007 (nL)^0.8 / (P2^0.5 s^0.4)	Compute Tt	hr	0.12			0.12
Shallow concentrated Flow		Segment ID	B-C			1
7. Surface Description (paved or unpaved)			UNPAVED			
8. Flow Length, L		ft	35.28	SPINE.	Volta Dali	
9. Watercourse slope, s		ft/ft	0.11			
10. Average Velocity, V (figure 3-1)		ft/s	5.35	Thinks a		
11. Tt = L / 3600V	Compute Tt	hr	0.00			0.00
Channel flow		Segment ID			with the	1
12. Cross sectional flow area, a		sf	28052-013	MAN SAN TEN	_NSC(vasas)	
13. Wetted perimeter, pw		ft	#SHALL SHA			
14. Hydraulic radius, r=a/wp	Compute r	ft	JUNEAU	LIEVIE,		
15. Channel Slope, s		ft/ft	1000	A CONTRACT		1
16. Manning's roughness coeff., n				S LUCI		1
20 MB : 이 문제 " ^ 1 IP 이 이 프랑스 이 시간 1 IP 이 전 1 IP 이 전 1 IP 이 시간	Compute V	ft/s	TO WE IT	WILESTON		1
18. Flow length, L		ft				1
	Compute Tt	17				0
20. Watershed or subarea Tc or Tt (add Tt in steps	6, 11, and 1	9)			hr	0.12

(210-VI-TR-55, Second Ed., June 1986)

Hydraflow Hydrographs by Intelisolve v9.2

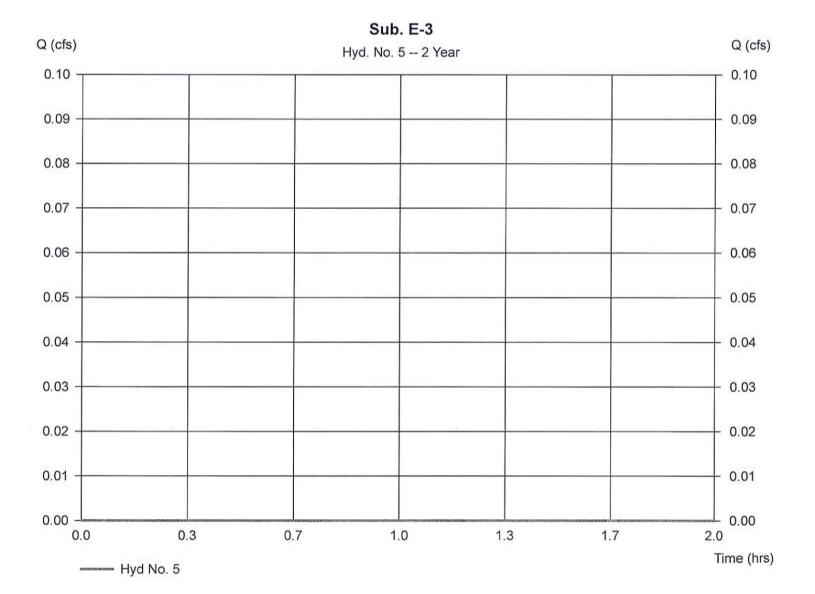
Tuesday, Jan 30, 2018

### Hyd. No. 5

Sub. E-3

Hydrograph type = SCS Runoff Storm frequency = 2 yrs Time interval = 2 min Drainage area = 0.300 acBasin Slope = 0.0 %Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.000 cfsTime to peak n/a Hyd. volume = 0 cuftCurve number = 30Hydraulic length = 0 ftTime of conc. (Tc)  $= 7.30 \, \text{min}$ Distribution = Type III = 484 Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

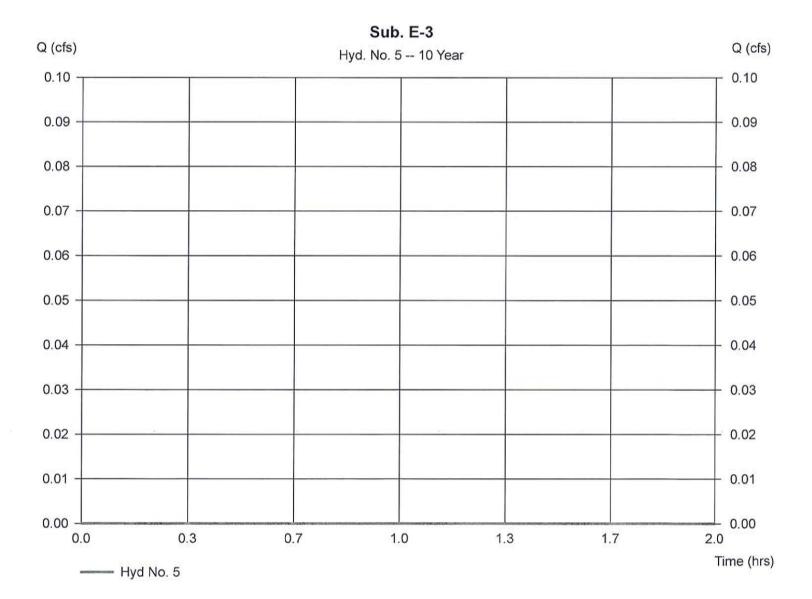
Tuesday, Jan 30, 2018

### Hyd. No. 5

Sub. E-3

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 min Drainage area = 0.300 acBasin Slope = 0.0 %Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.000 cfsTime to peak n/a Hyd. volume = 0 cuftCurve number = 30Hydraulic length = 0 ftTime of conc. (Tc)  $= 7.30 \, \text{min}$ Distribution = Type III Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

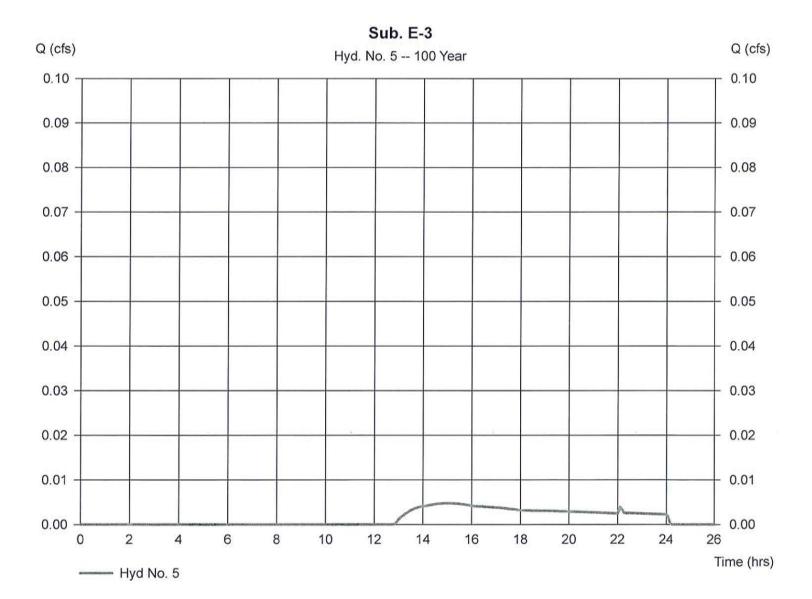
Tuesday, Jan 30, 2018

### Hyd. No. 5

Sub. E-3

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 0.300 acBasin Slope = 0.0 %Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

= 0.005 cfsPeak discharge Time to peak  $= 15.03 \, hrs$ Hyd. volume = 131 cuft Curve number = 30 Hydraulic length = 0 ftTime of conc. (Tc) = 7.30 minDistribution = Type III = 484 Shape factor





Project:	443 Lincoln St By PFK	Date	1/9/18	_		
Location:	Lexington, MA Checked					
Circle one:	Present Developed Subcatchment P-1					
1. Runoff curve n	umber (CN)					
Soil name and hydrologic	Cover description (cover type, treatment, and		CN 1/		Area	Product of CN x Area
group (appendix A)	hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
	Impervious - Drive 0	98	Silve	MUM	0.00	0.00
¥.	Impervious - Building 0	98	SUCLOY.	pagga	0.00	0.00
A	Woods and Brush Good Condition 16,437	30	ar raba	No.	0.38	11.32
А	Open Space Good Condition 5,908	39	0413(4)	, 8 (a B (a	0.14	5.29
		ibesiti	100	10000	sibulk	
		Kina Palifoni	861/CO	MOSE.	AND D	
		Sones	BHO.10	(fourth)	hadai	
		Becklo	12/8/57	5,000		
1/ Use only one C	N source per line.	30		Totals =	0.51	16.61
CN	(weighted) = total product = 16.61 = total area 0.51	32.38	; Use	CN =	32.4	]

Frequency.....

Rainfall, P (24-hour).....

Runoff, Q...(Use P and CN with table 2-1, fig. 2-1,) or eqs. 2-3 and 2-4.)
Runoff, Q.....

D-2

уг

in

cf

0.06

0.00

109 9 398 (210-VI-TR-55, Second Ed., June 1986)

0.21

SM-5676

Project: 443 Lincoln St		Ву	PFK_	Date	1/9/2018	3
Location: Lexington, MA		Checked		Date		
Control of the Contro	through subarea	Subcatchi	ment P-1			
Time of Concentration 2						
Sheet flow (Applicable to Tc only)		Segment ID	A-B	Maria Will		
1. Surface Description (table 3-1)			grass	The state of the s		19
2. Mannings roughness coeff., n (table 3-1)			0.4	yesee	post, in	
3. Flow length, L (total L <= 300 ft)		ft	50	E PSYME		
4. Two-yr 24-hr rainfall, P2		in	3.1			
5. Land Slope, s		ft/ft	0.14		F. 4.	
6. Tt = 0.007 (nL)^0.8 / (P2^0.5 s^0.4)	Compute Tt	hr	0.10			0.10
Shallow concentrated Flow		Segment ID	B-C	in (gravi)	N STUBBLE	VIII
7. Surface Description (paved or unpaved)			UNPAVED	CESTOWN.	MERLY	114
8. Flow Length, L		ft	25	ON MILES	To selb y d	FI
9. Watercourse slope, s		ft/ft	0.07		150000	
10. Average Velocity, V (figure 3-1)		ft/s	4.27		Saladah	100
11. Tt = L / 3600V	Compute Tt	hr	0.00			0.00
Channel flow		Segment ID	e ne i			
12. Cross sectional flow area, a 13. Wetted perimeter, pw	~	sf ft				
15. Channel Slope, s 16. Manning's roughness coeff., n	s parti e contre de contre esc. esc.	ft ft/ft				
18. Flow length, L	Compute V Compute Tt	ft			15,25 #5\. 10,13,611	0
20. Watershed or subarea Tc or Tt (add Tt in steps (210-VI-TR-55, Second Ed		10.110400			hr min	0.10 6.0 D-3

Hydraflow Hydrographs by Intelisolve v9.2

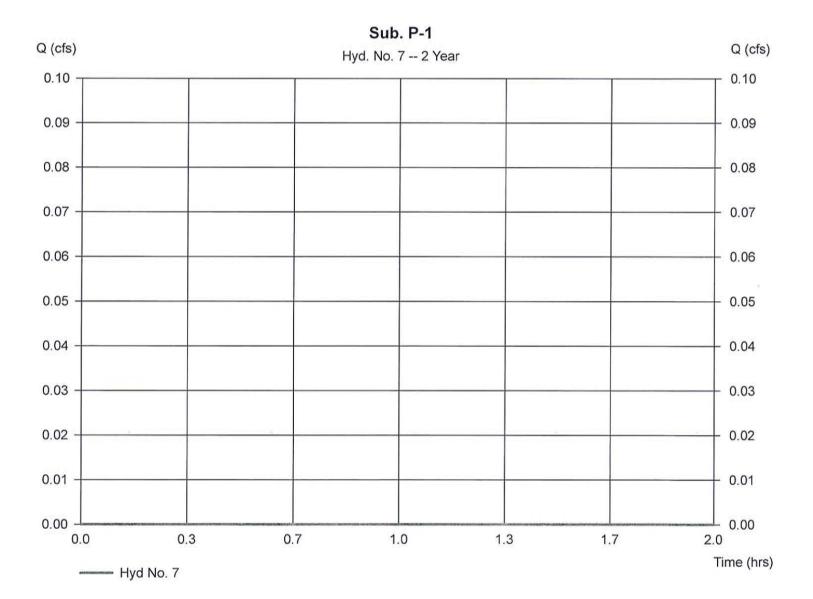
Tuesday, Jan 30, 2018

### Hyd. No. 7

Sub. P-1

Hydrograph type = SCS Runoff Storm frequency = 2 yrsTime interval = 2 min Drainage area = 0.510 acBasin Slope = 0.0 %Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.000 cfsTime to peak n/a Hyd. volume = 0 cuft Curve number = 32.4Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ Distribution = Type III Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

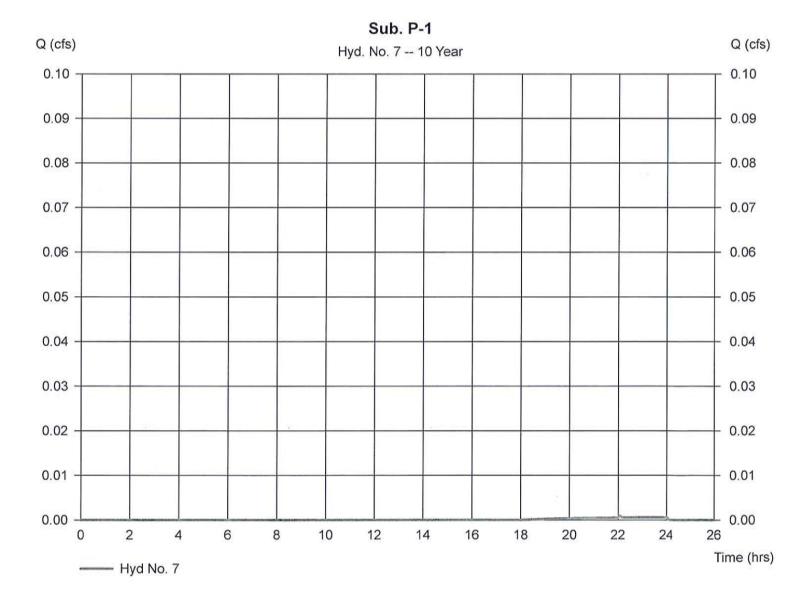
Tuesday, Jan 30, 2018

### Hyd. No. 7

Sub. P-1

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 min Drainage area = 0.510 acBasin Slope = 0.0 %Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.001 cfsTime to peak = 22.07 hrsHyd. volume = 9 cuft Curve number = 32.4Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ = Type III Distribution = 484 Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

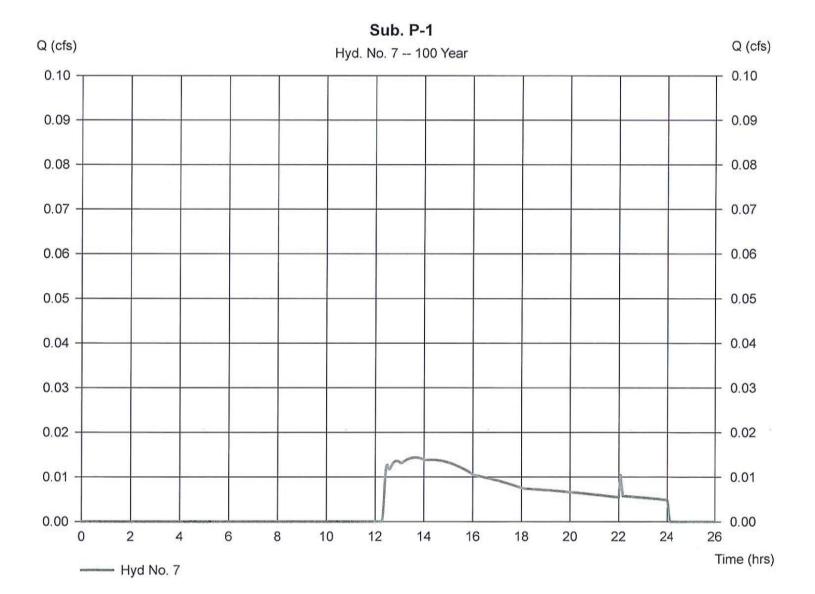
Tuesday, Jan 30, 2018

### Hyd. No. 7

Sub. P-1

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 0.510 acBasin Slope = 0.0 %Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 0.014 cfsTime to peak  $= 13.63 \, hrs$ Hyd. volume = 373 cuft Curve number = 32.4Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ Distribution = Type III Shape factor = 484



Project:	Worksheet 2: Runoff curve number and runo 443 Lincoln St	By PFK	Date	1/9/18		SM-5676	
Location	Lexington, MA	Checked			8		
Circle one	Present Developed	Subcatchment P-2A			•		
Runoff curve r	EXSENSION ( <del>Secondorde</del> ).	Subduter Ment 1 - 2/1					
Soil name	Cover descript	ion				Area	Product o
and hydrologic	(cover type, treatment, and			CN 1/		71100	CN x Area
group (appendix A)	hydrologic cond percent impervi unconnected/connected area ratio)	ous:	Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
	Impervious - Drive	14,768	98		MAN	0.34	33.22
0	Impervious - Building	0	98	QUILLY.	eastn.	0.00	0.00
Α	Woods and Brush Good Condition	o	30	-27.16	1000	0.00	0.00
Α	Open Space Good Condition	35,595	39	ÇOY (	20000	0.82	31.87
			080	er i de	HKG)	09.00	
			1000 A	co (C)	50,750	Solos.	
			SOUTH	dada	systems	major.	
			8868	nean	Cutto	1113.03	
I/ Use only one (	N source per line.			***	Totals =	1.16	65.09
CN	(weighted) = total product = total area	65.09 =	56.30	; Use (	ON =	56.3	]

		Storm #1	Storm #2	Storm #3
Frequency	уг	11/18/11	[]]/10///	11100
Rainfall, P (24-hour)	in	7/1/3/4/19	11/45/1	11/8,4/1
Runoff, Q	in	0.26	0.81	1.86
Runoff, Q D-2	cf	1080	3405	7822 Ed., June 19

SM-5676

D-3

Project: 443 Lincoln St	_	Ву	PFK	Date	1/9/2018	_
Location: Lexington, MA	_	Checked	9	Date		_
Circle one: Present Developed Circle one: Tc Tt	through subarea	Subcatchn	nent P-2A			
Time of Concentration 2						
Sheet flow (Applicable to Tc only)		Segment ID	A-B	Mark (H		1
1. Surface Description (table 3-1)			grass	- Mayor	743 F. F.	
2. Mannings roughness coeff., n (table 3-1)			0.24	Permi	Maria de la compansión de	
3. Flow length, L (total L <= 300 ft)		ft	50		HEATHER.	
4. Two-yr 24-hr rainfall, P2		in	3.1	Ten Majori	ment to a	
5. Land Slope, s		ft/ft	0.015			
6. Tt = 0.007 (nL)^0.8 / (P2^0.5 s^0.4)	Compute Tt	hr	0.16			0.16
Shallow concentrated Flow		Segment ID	B-C			Ī
7. Surface Description (paved or unpaved)			UNPAVED		1.20	
8. Flow Length, L		ft	45			
9. Watercourse slope, s		ft/ft	0.13	17.5 (S)/A		
10. Average Velocity, V (figure 3-1)		ft/s	5.82			
11. Tt = L / 3600V	Compute Tt	hr	0.00			0.00
Channel flow		Segment ID	170 30 2			ĺ
12. Cross sectional flow area, a 13. Wetted perimeter, pw		sf ft				
14. Hydraulic radius, r=a/wp	Compute r	ft				1
15. Channel Slope, s		ft/ft			L. Lunger	
16. Manning's roughness coeff., n		Len The	THE PERSON	The Total		1
17. V = 1.49 r^2/3 s^1/2 / n	Compute V	ft/s	OF BL			1
18. Flow length, L		ft	SEL PROJECTI	DEN JOHN ST		1
19. Tt = L / 3600V	Compute Tt	hr				0
20. Watershed or subarea Tc or Tt (add Tt in step	s 6, 11, and	19)			hr min	0.16 9.5

(210-VI-TR-55, Second Ed., June 1986)

Hydraflow Hydrographs by Intelisolve v9.2

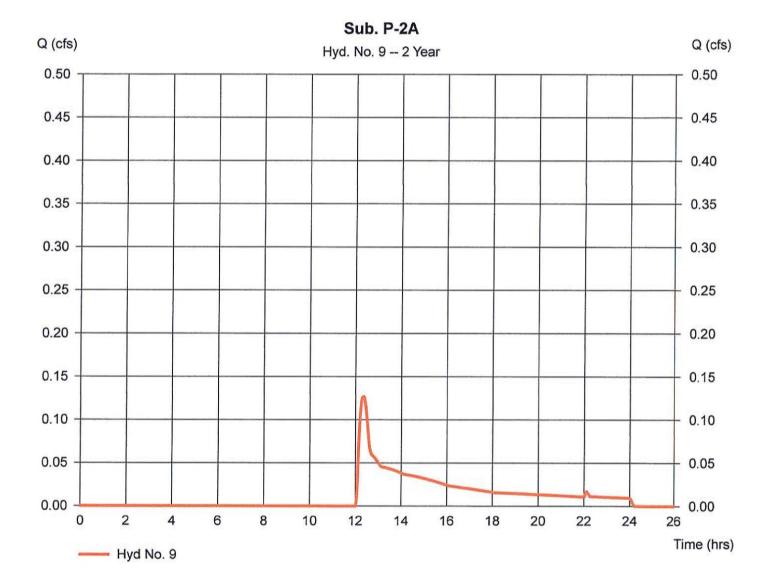
Wednesday, Feb 21, 2018

### Hyd. No. 9

Sub. P-2A

Hydrograph type = SCS Runoff Storm frequency = 2 yrs = 2 min Time interval Drainage area = 1.160 ac Basin Slope = 0.0 % Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.127 cfs
Time to peak = 12.33 hrs
Hyd. volume = 1,083 cuft
Curve number = 56.3
Hydraulic length = 0 ft
Time of conc. (Tc) = 9.50 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

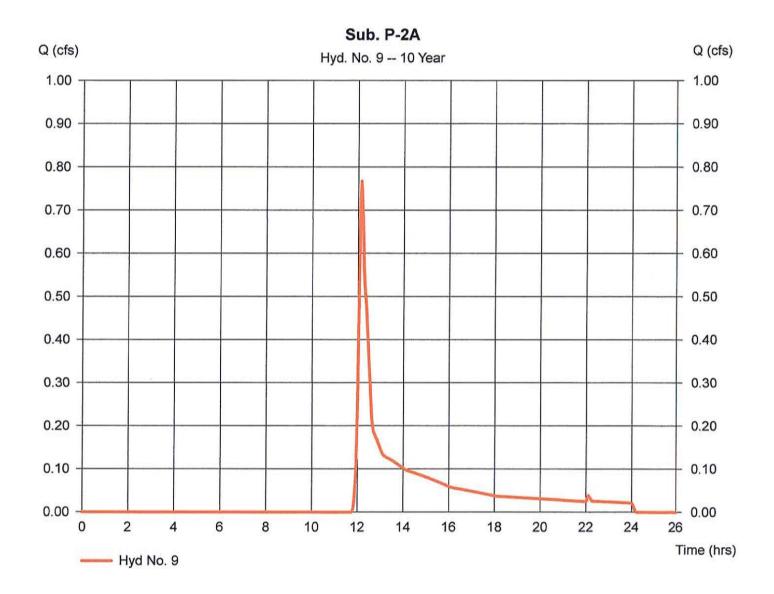
Wednesday, Feb 21, 2018

### Hyd. No. 9

Sub. P-2A

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 min = 1.160 acDrainage area Basin Slope = 0.0 %Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.768 cfs
Time to peak = 12.13 hrs
Hyd. volume = 3,416 cuft
Curve number = 56.3
Hydraulic length = 0 ft
Time of conc. (Tc) = 9.50 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

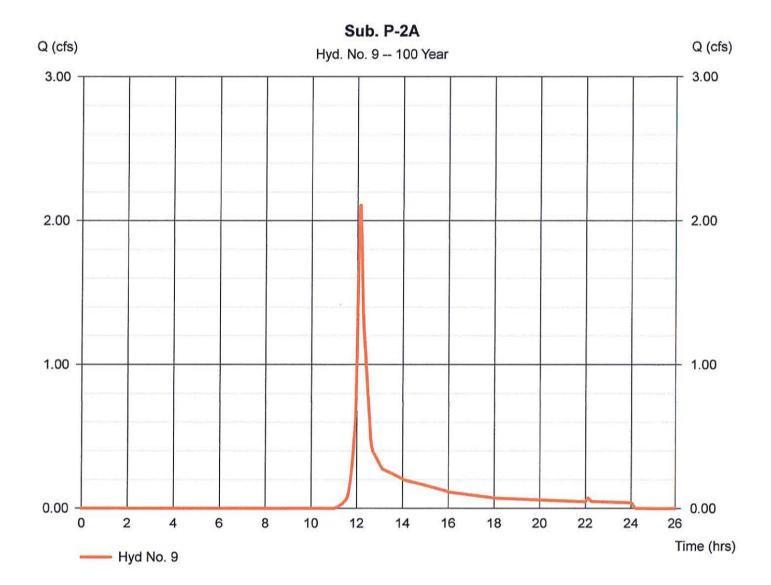
Wednesday, Feb 21, 2018

### Hyd. No. 9

Sub. P-2A

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 1.160 ac Basin Slope = 0.0 %Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 2.108 cfs
Time to peak = 12.13 hrs
Hyd. volume = 7,847 cuft
Curve number = 56.3
Hydraulic length = 0 ft
Time of conc. (Tc) = 9.50 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

Wednesday, Feb 21, 2018

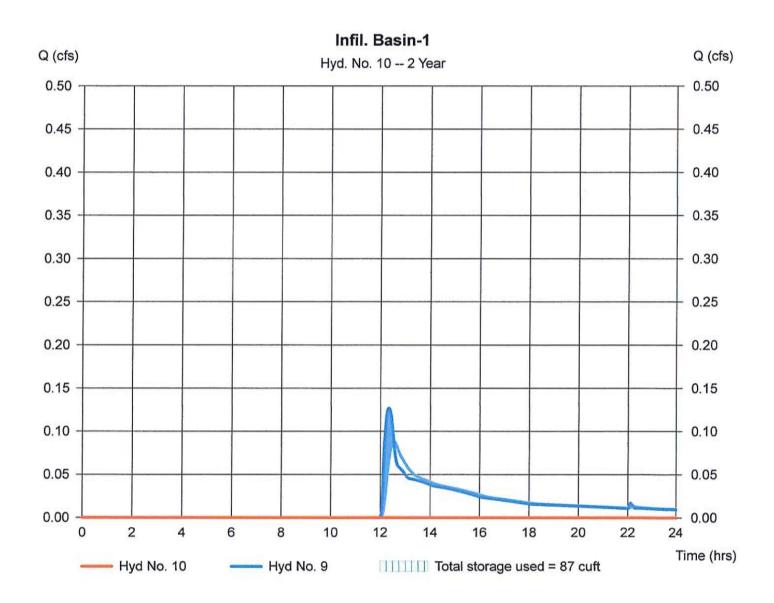
### Hyd. No. 10

Infil. Basin-1

Hydrograph type = Reservoir
Storm frequency = 2 yrs
Time interval = 2 min
Inflow hyd. No. = 9 - Sub. P-2A
Reservoir name = Infil. Basin-1

Peak discharge = 0.000 cfs
Time to peak = 13.10 hrs
Hyd. volume = 0 cuft
Max. Elevation = 174.83 ft
Max. Storage = 87 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs by Intelisolve v9.2

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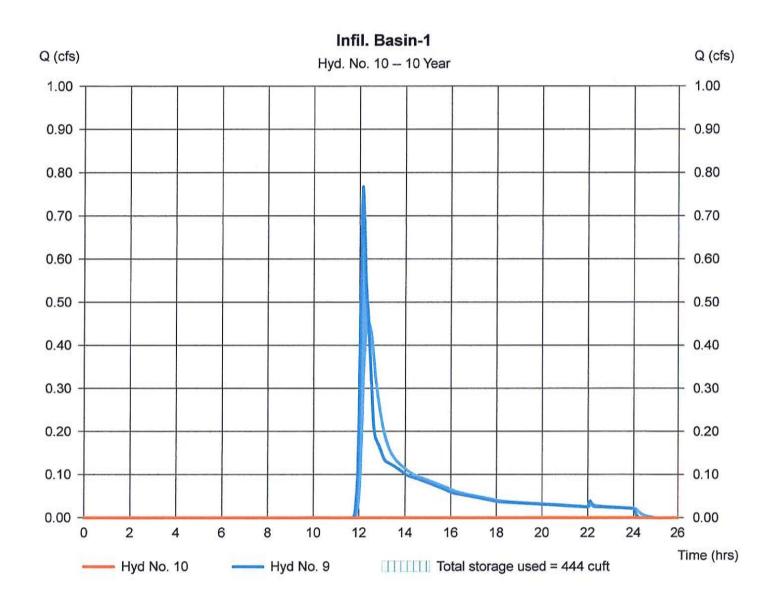
### Hyd. No. 10

Infil. Basin-1

Hydrograph type = Reservoir
Storm frequency = 10 yrs
Time interval = 2 min
Inflow hyd. No. = 9 - Sub. P-2A

Inflow hyd. No. = 9 - Sub. P-2A Reservoir name = Infil. Basin-1 Peak discharge = 0.000 cfs
Time to peak = 12.50 hrs
Hyd. volume = 0 cuft
Max. Elevation = 174.96 ft
Max. Storage = 444 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs by Intelisolve v9.2

Wednesday, Feb 21, 2018

= 0.000 cfs

= 12.03 hrs

 $= 175.39 \, ft$ 

= 1,864 cuft

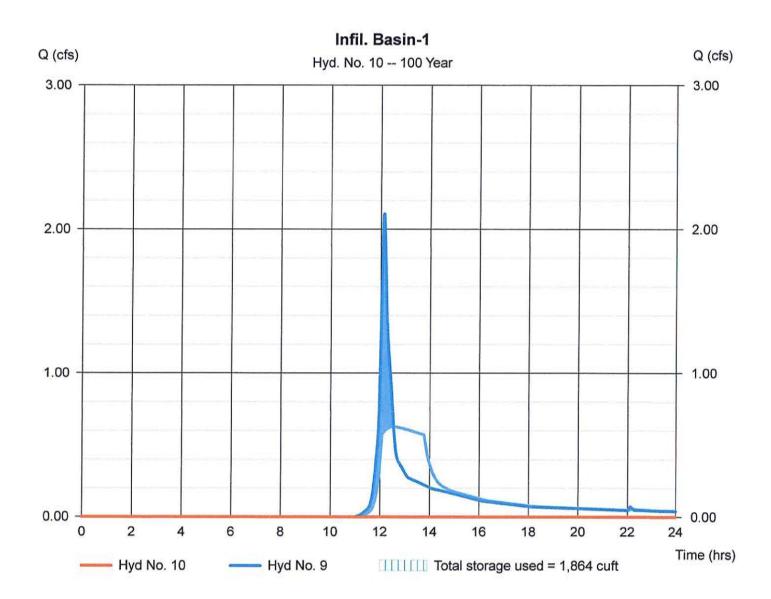
= 0 cuft

#### Hyd. No. 10

Infil. Basin-1

Hydrograph type= ReservoirPeak dischargeStorm frequency= 100 yrsTime to peakTime interval= 2 minHyd. volumeInflow hyd. No.= 9 - Sub. P-2AMax. ElevationReservoir name= Infil. Basin-1Max. Storage

Storage Indication method used. Exfiltration extracted from Outflow.



# **Pond Report**

Hydraflow Hydrographs by Intelisolve v9.2

Tuesday, Jan 30, 2018

Pond No. 1 - Infil. Basin-1

**Pond Data** 

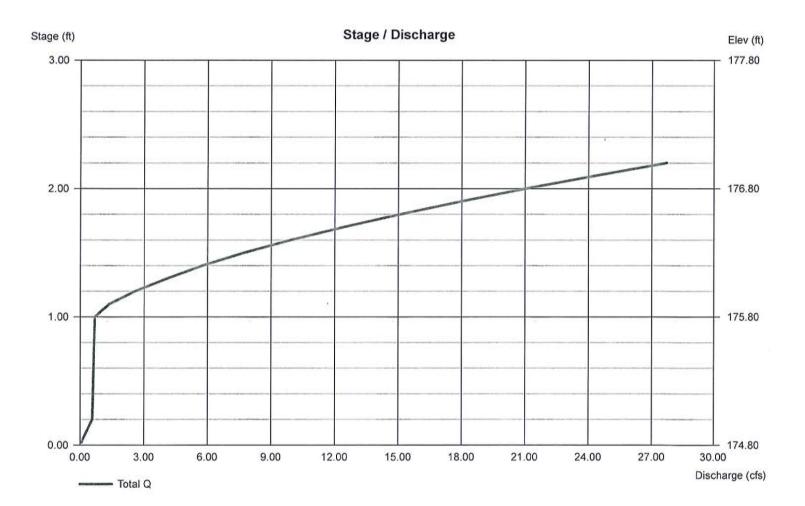
Contours - User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 174.80 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	174.80	2,635	0	0
0.20	175.00	2,990	562	562
1.20	176.00	3,741	3,358	3,920
2.20	177.00	5,270	4,483	8,404

Culvert / Orifice Structures					Weir Structures						
	[A]	[B]	[C]	[PrfRsr]			[A]	[B]	[C]	[D]	
Rise (in)	= 12.00	0.00	0.00	0.00	Crest Len (ft)	=	6.28	8.50	0.00	0.00	
Span (in)	= 12.00	0.00	0.00	0.00	Crest El. (ft)	=	175.80	176.00	0.00	0.00	
No. Barrels	= 1	1	1	0	Weir Coeff.	=	3.33	2.60	3.33	3.33	
Invert El. (ft)	= 175.00	0.00	0.00	0.00	Weir Type	=	Riser	Broad			
Length (ft)	= 94.00	0.00	0.00	0.00	Multi-Stage	=	Yes	No	No	No	
Slope (%)	= 1.00	0.00	0.00	n/a							
N-Value	= .010	.010	.010	n/a							
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	==	8.270 (by	Contour)			
Multi-Stage	= n/a	Yes	Yes	No	TW Elev. (ft)	=	0.00	. N			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



	Worksheet 2: Runoff curve number and runoff					SM-5676	
Project:	443 Lincoln St	By PFK	Date	1/29/18	_		
Location:	Lexington, MA	Checked	Date		-		
Circle one:	Present Developed	Subcatchment P-2B					
1. Runoff curve n	umber (CN)						
Soil name and hydrologic	Cover description (cover type, treatment, and			CN 1/	Area	Product of CN x Area	
group (appendix A)	hydrologic condition percent impervious unconnected/connected im area ratio)		Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
1K	Impervious - Drive	o	98	Tidani	isnami	0.00	0.00
45	Impervious - Building	o	98	90253	arceq	0.00	0.00
Α	Woods and Brush Good Condition	60,051	30	e Ambi	turnity.	1.38	41.36
Α	Open Space Good Condition	20,160	39	et e cu	senti-	0.46	18.05
			No mo	άψαρη	PERCON		
			el lisa	docum	Seklen	enter	
			eln la ()	Zerjeni.	THE LOCAL	63771	
			dato	arrest	BYSKE I	en gard	
1/ Use only one C	N source per line.				Totals =	1.84	59.41
CN	(weighted) = total product = total area	59.41 =	32.26	; Use	CN =	32.3	1

		Storm #1	Storm #2	Storm #3
Frequency	уг	31/3/11	11/10/11	1/1/100/
Rainfall, P (24-hour)	in	17/3/2//	11/45/11	1116,411
Runoff, Q (Use P and CN with table 2-1, fig. 2-1,) or eqs. 2-3 and 2-4.)	in	0.06	0.00	0.21
Runoff, Q	cf	406	28	1396

SM-5676

D-3

Project:	443 Lincoln St	_	Ву	PFK	Date	1/9/2018	_
Location:	Lexington, MA		Checked	l	Date		_
Circle one: Circle one:	Present Developed Tc Tt	through subarea	Subcatchn	nent P-2B			
Time of Co	ncentration 2						
Sheet flow (	Applicable to Tc only)		Segment ID	A-B			1
1. Surface E	Description (table 3-1)			grass	A PROPERTY.		
2. Mannings	roughness coeff., n (table 3-1)			0.4		Kitant	
3. Flow leng	th, L (total L <= 300 ft)		ft	50		rigion (S	1
4. Two-yr 24	-hr rainfall, P2		in	3.1	Rings II		
5. Land Slop	oe, s		ft/ft	0.1			
6. Tt = 0.007	7 (nL)^0.8 / (P2^0.5 s^0.4)	Compute Tt	hr	0.11			0.11
Shallow con	centrated Flow		Segment ID	B-C		的特点等人	1
7. Surface D	escription (paved or unpaved)			UNPAVED	301777	De Yorken	1
8. Flow Leng	gth, L		ft	332		-1691	
9. Watercou	rse slope, s		ft/ft	0.015	F5_64 (F16)		
10. Average	Velocity, V (figure 3-1)		ft/s	1.98	MELO, O		
11. Tt = L / 3	8600V	Compute Tt	hr	0.05			0.05
Channel flov	V		Segment ID				1
12. Cross se	ectional flow area, a		sf				1
	perimeter, pw		ft			tes linears	]
/ Control of the cont	c radius, r=a/wp	Compute r	ft	O PULL		West Trolls	
15. Channel			ft/ft	MALE PLAN			
1.77	's roughness coeff., n					(Designation)	
17. V = 1.49	r^2/3 s^1/2 / n	Compute V	ft/s				
18. Flow len			ft	MARCHARIA		DEVISED 18	
19. Tt = L / 3	600V	Compute Tt	hr				0
20. Watersh	ed or subarea Tc or Tt (add Tt in step	s 6, 11, and	19)			hr min	0.16 9.4

(210-VI-TR-55, Second Ed., June 1986)

Hydraflow Hydrographs by Intelisolve v9.2

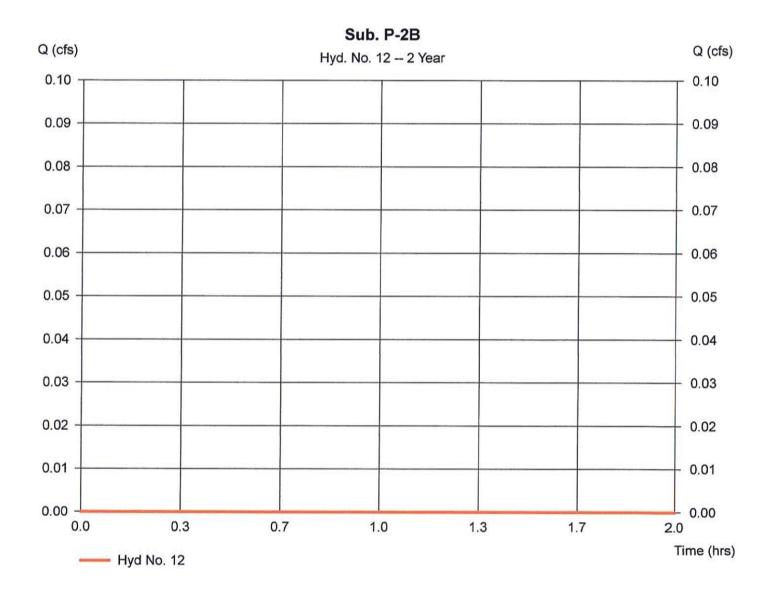
Wednesday, Feb 21, 2018

### Hyd. No. 12

Sub. P-2B

Hydrograph type = SCS Runoff Storm frequency = 2 yrs Time interval = 2 min Drainage area = 1.840 acBasin Slope = 0.0 %Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.000 cfs
Time to peak = n/a
Hyd. volume = 0 cuft
Curve number = 32.3
Hydraulic length = 0 ft
Time of conc. (Tc) = 9.40 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

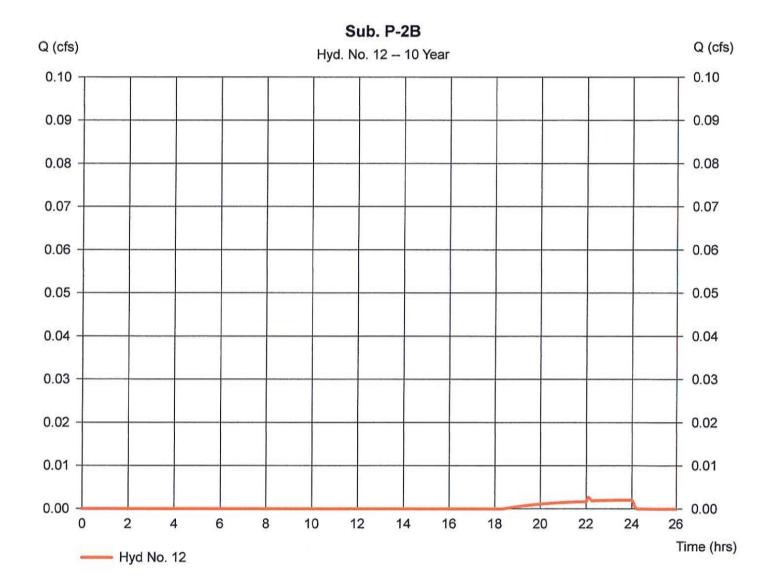
Wednesday, Feb 21, 2018

### Hyd. No. 12

Sub. P-2B

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 min Drainage area = 1.840 acBasin Slope = 0.0 %Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.003 cfs
Time to peak = 22.10 hrs
Hyd. volume = 30 cuft
Curve number = 32.3
Hydraulic length = 0 ft
Time of conc. (Tc) = 9.40 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

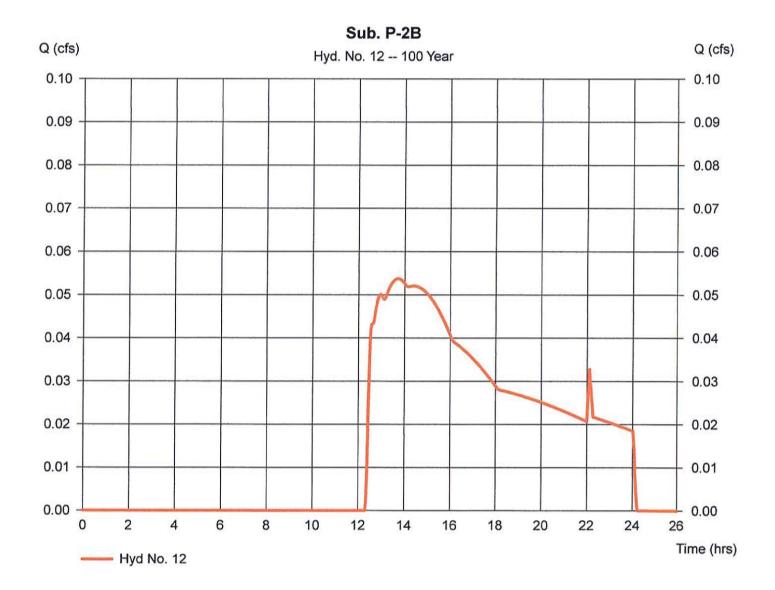
Wednesday, Feb 21, 2018

### Hyd. No. 12

Sub. P-2B

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 1.840 acBasin Slope = 0.0 %Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 0.054 cfs
Time to peak = 13.70 hrs
Hyd. volume = 1,405 cuft
Curve number = 32.3
Hydraulic length = 0 ft
Time of conc. (Tc) = 9.40 min
Distribution = Type III
Shape factor = 484



Project:	Worksheet 2: Runoff curve number and runoff  443 Lincoln St By PFK	Date	1/29/18		SM-5676	
Location:	Lexington, MA Checked					
Circle one:	Present Developed Subcatchment P-3					
1. Runoff curve n	umber (CN)					
Soil name and hydrologic	Cover description (cover type, treatment, and		CN 1/		Area	Product of CN x Area
group (appendix A)	hydrologic condition: percent impervious: unconnected/connected impervious area ratio)	Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
	Impervious - Drive 0	98	Nonne	W 1 1 1 1 1 1 1	0.00	0.00
27	Impervious - Building 0	98	911251		0.00	0.00
А	Woods and Brush Good Condition 13,225	30	2,5965	diplosi	0.30	9,11
A	Open Space Good Condition 0	39	0000	Nº 103	0.00	0.00
		No Copin	00001	Section.	8,500	
		Secretary.	elogia:		måen.	
		DEORO		10000	dues	
		101100	ķesa.	Take		
1/ Use only one C	N source per line.			Totals =	0.30	9,11
CN	(weighted) = total product = 9.11 = 10tal area = 0.30	30.00	; Use	CN =	30.0	]
2. Runoff	Storm #1 Storm #2 Storm #3					
Frequency	yr \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\					

in

11/3/1/

124 1 132 (210-VI-TR-55, Second Ed., June 1986)

Rainfall, P (24-hour).....

Runoff, Q....(Use P and CN with table 2-1, fig. 2-1,) or eqs. 2-3 and 2-4.)

Runoff, Q.....

D-2

#### Worksheet 4: Time of Concentration (Tc) or travel time (Tt)

SM-5676

Project:	443 Lincoln St	-	Ву	PFK	Date	1/9/2018	
Location:	Lexington, MA	_	Checked		Date		
Circle one: Circle one:	Present Developed Tc Tt	through subarea	Subcatchr	ment P-3			
Time of Co	ncentration 2						
Sheet flow (	Applicable to Tc only)		Segment ID	A-B	10000000		
1. Surface D	Description (table 3-1)			grass			
2. Mannings	roughness coeff., n (table 3-1)			0.4	(NEDEA JEWN		
3. Flow leng	th, L (total L <= 300 ft)		ft	50	W. Spring to		
4. Two-yr 24	-hr rainfall, P2		in	3,1			
5. Land Slop	pe, s		ft/ft	0.08		23,954	
6. Tt = 0.007	7 (nL)^0.8 / (P2^0.5 s^0.4)	Compute Tt	hr	0.12			0.12
Shallow con	centrated Flow		Segment ID	B-C			
7. Surface D	escription (paved or unpaved)			UNPAVED			
8. Flow Leng	gth, L		ft	35.28		Replied!	
9. Watercou	rse slope, s		ft/ft	0.11			
10. Average	Velocity, V (figure 3-1)		ft/s	5.35			
11. Tt = L / 3	3600V	Compute Tt	hr	0.00			0.00
Channel flow	<u> </u>		Segment ID	07/11/2010	MI DAMENT		
13. Wetted p	ectional flow area, a perimeter, pw c radius, r=a/wp	Compute r	sf ft ft	12.00			
15. Channel 16. Manning		Compute V	ft/ft				
18. Flow leng	gth, L	15	ft	MERRI			0
20. Watersh	ed or subarea Tc or Tt (add Tt in step (210-VI-TR-55, Second I					hr min	0.12 7.3 D-3

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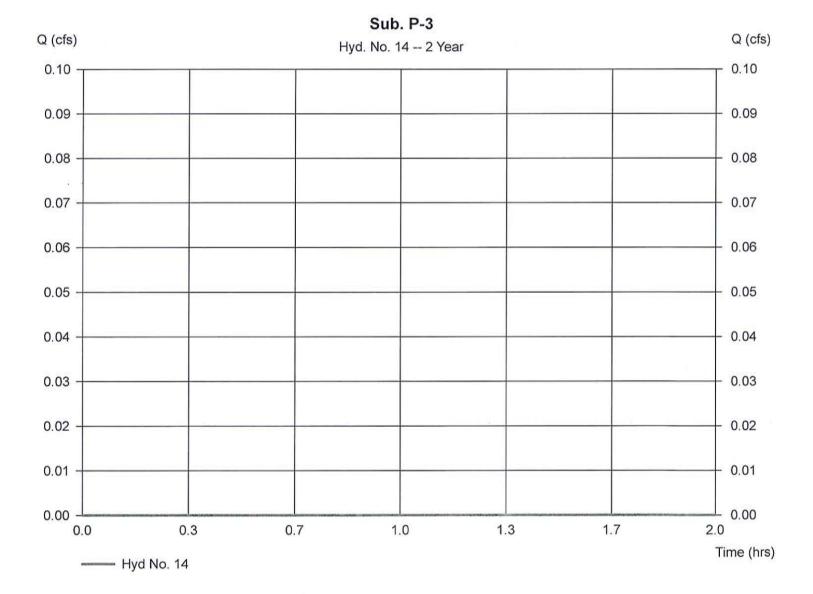
Tuesday, Jan 30, 2018

#### Hyd. No. 14

Sub. P-3

Hydrograph type = SCS Runoff Storm frequency = 2 yrsTime interval = 2 min Drainage area = 0.300 acBasin Slope = 0.0 %Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.000 cfsTime to peak n/a Hyd. volume = 0 cuftCurve number = 30Hydraulic length = 0 ftTime of conc. (Tc) = 7.30 minDistribution = Type III Shape factor = 484



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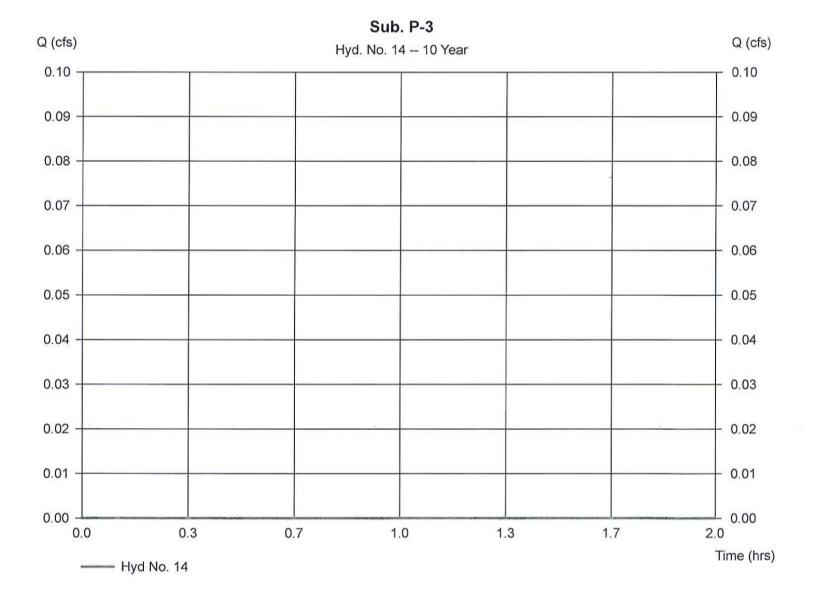
Tuesday, Jan 30, 2018

#### Hyd. No. 14

Sub. P-3

= SCS Runoff Hydrograph type Storm frequency = 10 yrsTime interval = 2 min Drainage area = 0.300 acBasin Slope = 0.0 %Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.000 cfsTime to peak n/a Hyd. volume = 0 cuftCurve number = 30Hydraulic length = 0 ftTime of conc. (Tc)  $= 7.30 \, \text{min}$ = Type III Distribution Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

Tuesday, Jan 30, 2018

### Hyd. No. 14

Sub. P-3

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 0.300 acBasin Slope = 0.0 %Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 0.005 cfsTime to peak  $= 15.03 \, hrs$ Hyd. volume = 131 cuft Curve number = 30Hydraulic length = 0 ftTime of conc. (Tc)  $= 7.30 \, \text{min}$ Distribution = Type III Shape factor = 484



	Worksheet 2: Runoff curve number and ru	inoff		SM-5676
Project:	443 Lincoln St	By PFK	Date 1/29/18	
Location:	Lexington, MA	Checked	Date	
Circle one:	Present Developed	Roof Drywell A		
1. Runoff curve	number (CN)			

Soil name and hydrologic	Cover description (cover type, treatment, and			CN 1/		Area	Product of CN x Area
group (appendix A)	hydrologic condition: percent impervious: unconnected/connected impervious area ratio)		Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
12	Impervious - Drive	o	98	nedika.	heur	0.00	0.00
(H)	Impervious - Building	2,967	98	War and		0.07	6.68
Α	Woods and Brush Good Condition	o	30	(SISN)	popci	0.00	0.00
A	Open Space Good Condition		39	notes.	VERSON	0.00	0.00
			1500	Mosk	SOMETIME	gages	
			odde	endol	Str scal	delalat	
			leads:	6,552	97050	Jan 1	
			2,000	F S KIK	STURM	eethig	
/ Use only one C	N source per line.				Totals =	0.07	6.68

CN (weighted) = total product = 6.68 = 98.00 Use CN = 98.0

2. Runoff				
		Storm #1	Storm #2	Storm #3
Frequency	yr	1115/11	11/10/11	///100//
Rainfall, P (24-hour)	in	113.41	4,5	11/1/6:4/17
Runoff, Q	in	2.87	4.26	6.16
Runoff, Q	cf	709 (210-VI-TR	1054 2-55, Second	1523 Ed., June 198

Hydraflow Hydrographs by Intelisolve v9.2

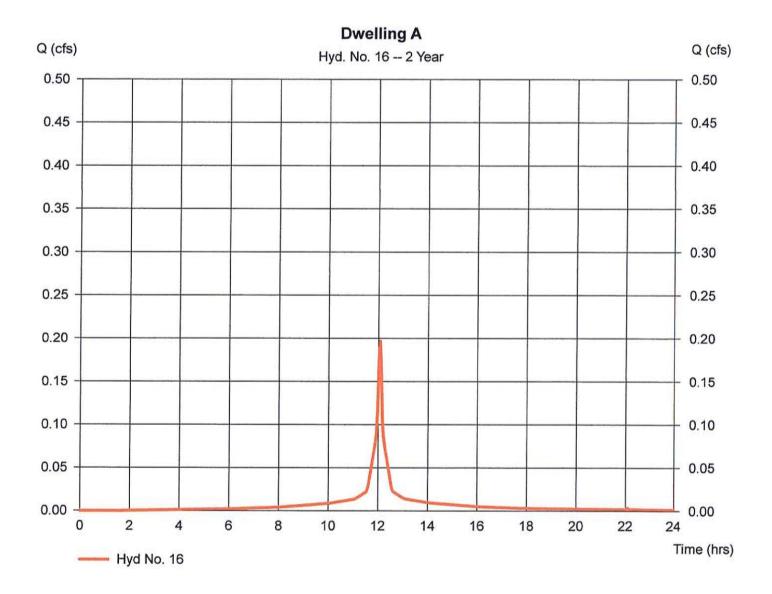
Wednesday, Feb 21, 2018

#### Hyd. No. 16

### Dwelling A

= SCS Runoff Hydrograph type = 2 yrs Storm frequency = 2 min Time interval Drainage area = 0.068 acBasin Slope = 0.0 %Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.197 cfs
Time to peak = 12.07 hrs
Hyd. volume = 664 cuft
Curve number = 98
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

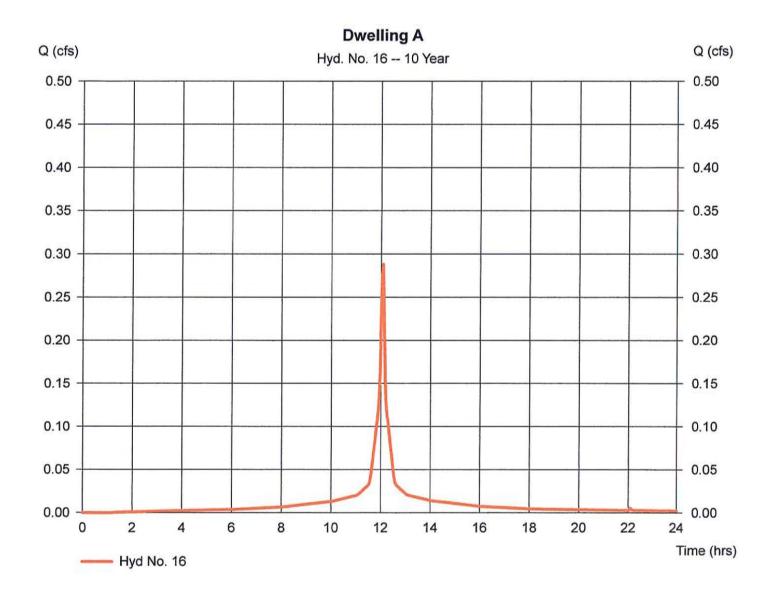
Wednesday, Feb 21, 2018

### Hyd. No. 16

### Dwelling A

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 min = 0.068 acDrainage area Basin Slope = 0.0 %Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.288 cfs
Time to peak = 12.07 hrs
Hyd. volume = 987 cuft
Curve number = 98
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

Wednesday, Feb 21, 2018

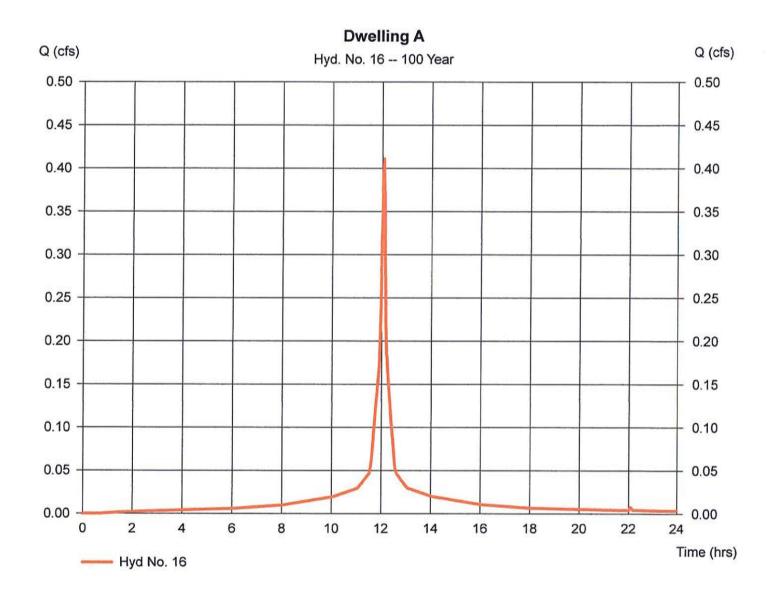
### Hyd. No. 16

### Dwelling A

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 0.068 acBasin Slope = 0.0 % Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 0.411 cfs Time to peak = 12.07 hrs Hyd. volume = 1,426 cuft

Curve number = 98
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

Wednesday, Feb 21, 2018

= 98 cuft

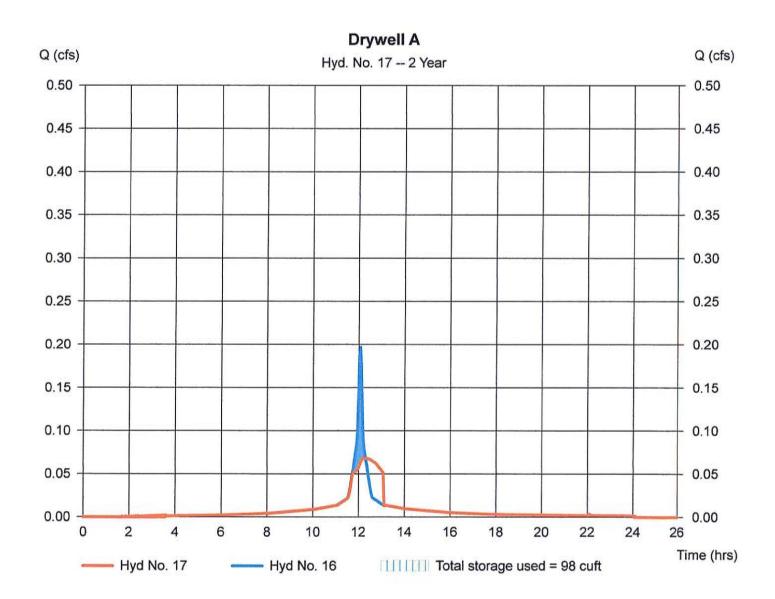
### Hyd. No. 17

Drywell A

Hydrograph type = Reservoir Storm frequency = 2 yrs Time interval = 2 min

Inflow hyd. No. = 16 - Dwelling A Reservoir name = Roof Drywell A Peak discharge = 0.068 cfs Time to peak = 12.30 hrs Hyd. volume = 664 cuft Max. Elevation = 176.71 ft

Max. Storage



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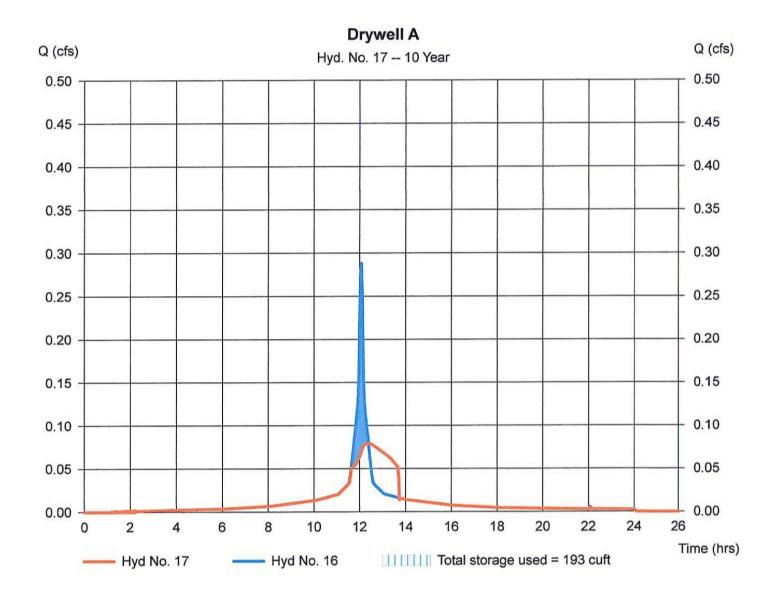
Wednesday, Feb 21, 2018

#### Hyd. No. 17

Drywell A

Hydrograph type = Reservoir
Storm frequency = 10 yrs
Time interval = 2 min
Inflow hyd. No. = 16 - Dwelling A
Reservoir name = Roof Drywell A

Peak discharge = 0.080 cfs
Time to peak = 12.37 hrs
Hyd. volume = 987 cuft
Max. Elevation = 177.16 ft
Max. Storage = 193 cuft



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Wednesday, Feb 21, 2018

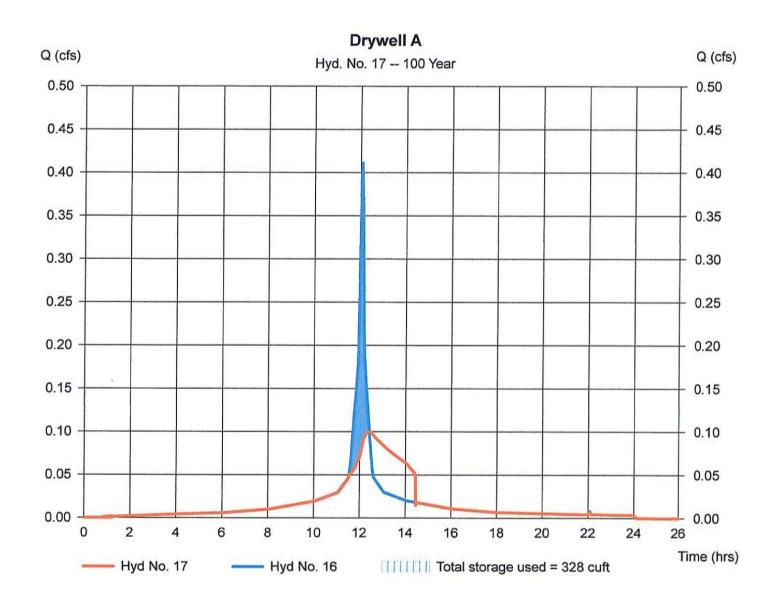
### Hyd. No. 17

Drywell A

Hydrograph type = Reservoir Storm frequency = 100 yrs Time interval = 2 min

Inflow hyd. No. = 16 - Dwelling A Reservoir name = Roof Drywell A Peak discharge = 0.100 cfs Time to peak = 12.43 hrs Hyd. volume = 1,426 cuft

Max. Elevation = 178.01 ft Max. Storage = 328 cuft



Hydraflow Hydrographs by Intelisolve v9.2

Friday, Feb 9, 2018

#### Pond No. 7 - Roof Drywell A

#### **Pond Data**

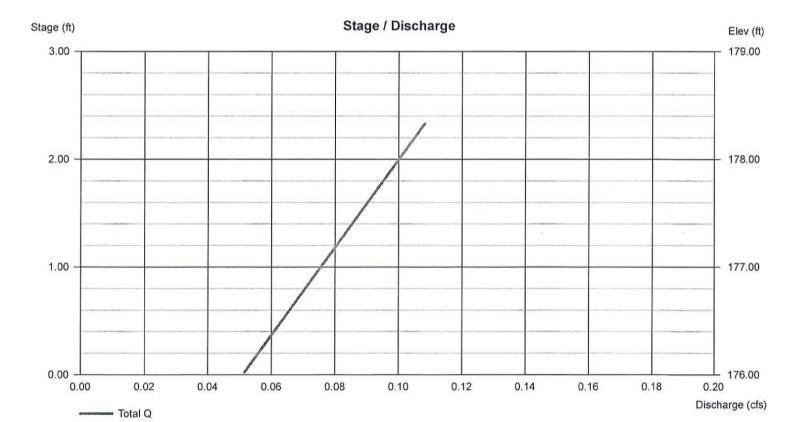
UG Chambers - Invert elev. = 176.50 ft, Rise x Span =  $1.33 \times 2.83$  ft, Barrel Len = 21.36 ft, No. Barrels = 3, Slope = 0.00%, Headers = No Encasement - Invert elev. = 176.00 ft, Width = 4.16 ft, Height = 2.33 ft, Voids = 40.00%

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	176.00	n/a	0	0
0.23	176.23	n/a	25	25
0.47	176.47	n/a	25	50
0.70	176.70	n/a	46	96
0.93	176.93	n/a	49	146
1.17	177.17	n/a	48	193
1.40	177.40	n/a	45	239
1.63	177.63	n/a	41	280
1.86	177.86	n/a	33	312
2.10	178.10	n/a	25	337
2.33	178.33	n/a	25	362

#### Culvert / Orifice Structures **Weir Structures** [A] [B] [C] [PrfRsr] [A] [B] [C] [D] = 0.000.00 0.00 0.00 0.00 0.00 Rise (in) Crest Len (ft) = 0.00Inactive Span (in) = 0.000.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels = 00 0 Weir Coeff. = 3.333.33 3.33 3.33 0.00 0.00 Invert El. (ft) 0.00 Weir Type = 0.00= ---Length (ft) = 0.000.00 0.00 0.00 Multi-Stage = No No No No Slope (%) = 0.000.00 0.00 n/a .013 .013 N-Value = .013n/a = 0.600.60 0.60 0.60 = 8.270 (by Wet area) Orifice Coeff. Exfil.(in/hr) Multi-Stage = 0.00= n/aNo No No TW Elev. (ft)

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



-	Worksheet 2: Runoff curve number and runoff	720 220	200			SM-5676	
Project:	443 Lincoln St	By PFK		1/29/18	ē.		
Location:	Lexington, MA	Checked	Date		Ť		
Circle one:	Present Developed	Roof Drywells B & C					
Runoff curve n	umber (CN)						
Soil name and hydrologic	Cover description (cover type, treatment, and			CN 1/		Area	Product of CN x Area
group (appendix A)	hydrologic conditio percent imperviou unconnected/connected in area ratio)	S:	Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
*	Impervious - Drive	0	98	DOM:	NUDUO:	0.00	0,00
(*)	Impervious - Building	3,848	98	ctobs	nha hii	0.09	8.66
А	Woods and Brush Good Condition	o	30		Madine II	0.00	0.00
Α	Open Space Good Condition		39	00008	Madda	0.00	0.00
			la page	4448	10000	40°0	
			(60000)	oppér	parties	ightable	
			8146	erbet	notes.	-3-3	
			2 (2.2)	2/0/12	2000	LINES.	
1/ Use only one C	N source per line.				Totals =	0.09	8.66
CN 2. Runoff	(weighted) = total product = total area	8.66 =	98.00	Use	CN =	98.0	]

11/3/1/1	11/10/11/	(1) 5,4
11/3/1/1/	///X5///	11/6,4/1
2.87	4.26	6,16
920	1367	1976
		920 1367 (210-VI-TR-55, Second E

Hydraflow Hydrographs by Intelisolve v9.2

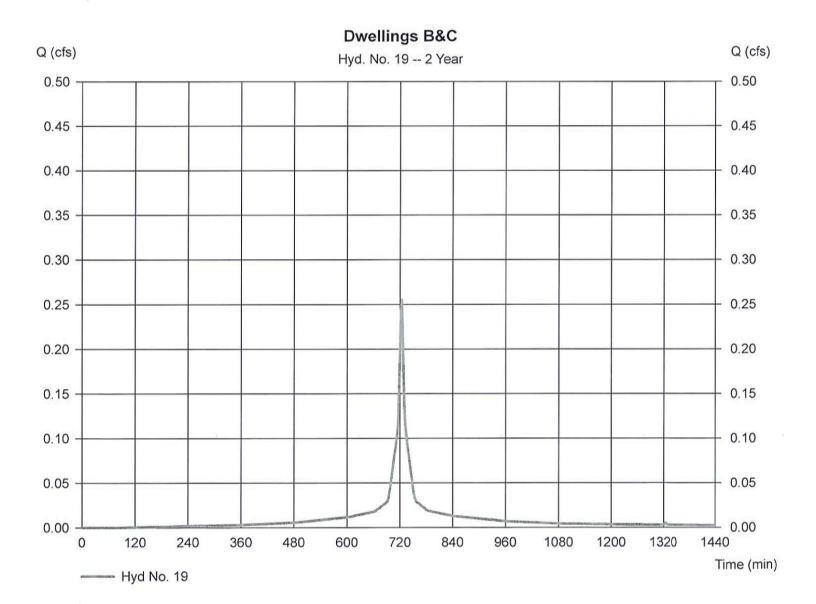
Friday, Feb 9, 2018

#### Hyd. No. 19

**Dwellings B&C** 

= SCS Runoff Hydrograph type Storm frequency = 2 yrs Time interval = 2 minDrainage area = 0.088 acBasin Slope = 0.0 %Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.255 cfsTime to peak 724 min Hyd. volume = 859 cuft Curve number = 98 Hydraulic length = 0 ftTime of conc. (Tc)  $= 6.00 \, \text{min}$ = Type III Distribution Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

Friday, Feb 9, 2018

#### Hyd. No. 19

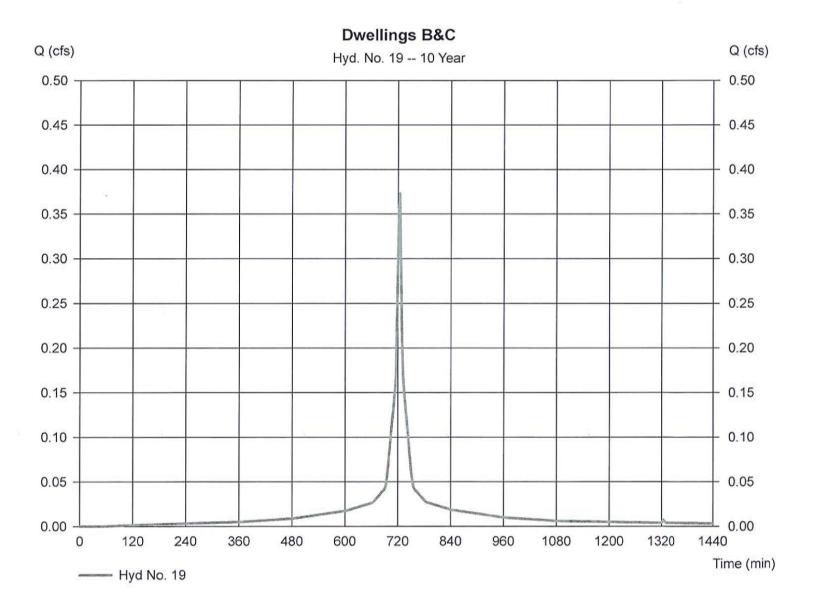
**Dwellings B&C** 

Hydrograph type = SCS Runoff Storm frequency = 10 yrs= 2 min Time interval Drainage area = 0.088 acBasin Slope = 0.0 %Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.373 cfs
Time to peak = 724 min
Hyd. volume = 1,277 cuft
Curve number = 98
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III

= 484

Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

Friday, Feb 9, 2018

#### Hyd. No. 19

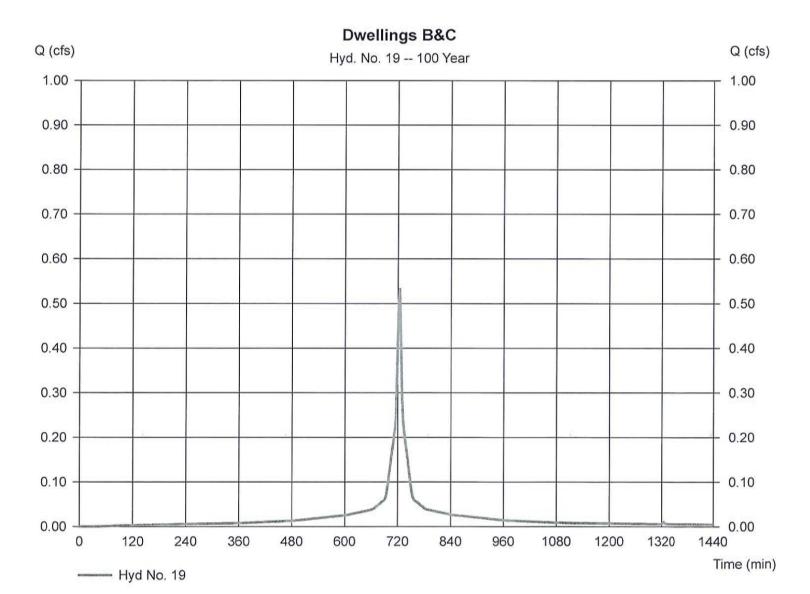
#### **Dwellings B&C**

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 2 min Drainage area = 0.088 acBasin Slope = 0.0 %Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 0.532 cfs
Time to peak = 724 min
Hyd. volume = 1,845 cuft
Curve number = 98
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III

= 484

Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

Friday, Feb 9, 2018

#### Hyd. No. 20

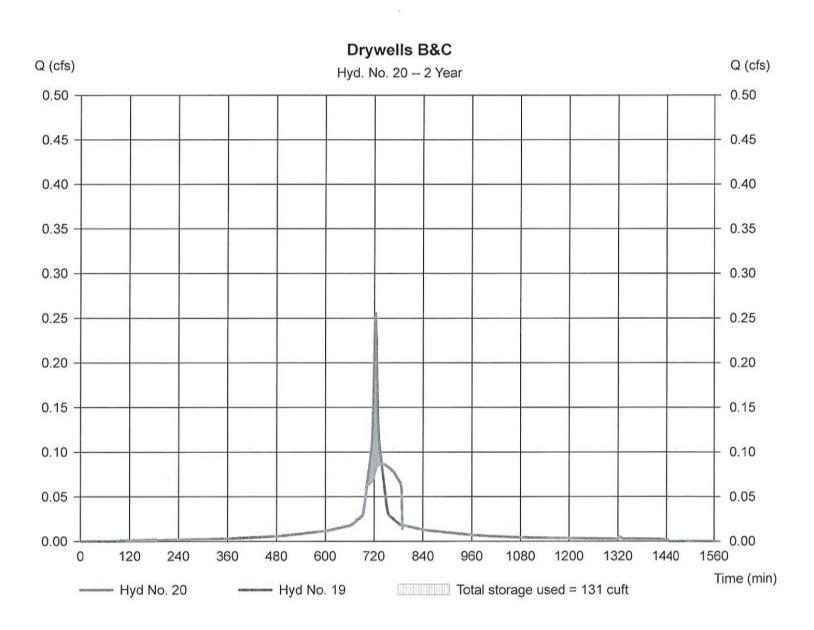
Drywells B&C

Hydrograph type = Reservoir Storm frequency = 2 yrs Time interval = 2 min

Inflow hyd. No. = 19 - Dwellings B&C
Reservoir name = Roof Drywell B

Peak discharge = 0.087 cfs
Time to peak = 738 min
Hyd. volume = 859 cuft
Max. Elevation = 0.74 ft

Max. Storage = 131 cuft



Hydraflow Hydrographs by Intelisolve v9.2

Friday, Feb 9, 2018

#### Hyd. No. 20

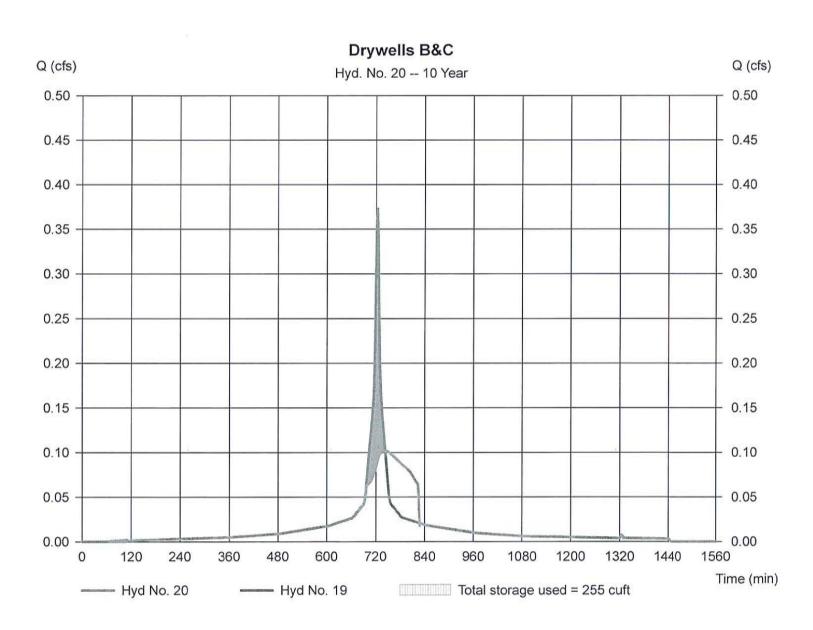
Drywells B&C

Hydrograph type = Reservoir Storm frequency = 10 yrs Time interval = 2 min

Inflow hyd. No. = 19 - Dwellings B&C
Reservoir name = Roof Drywell B

Peak discharge = 0.102 cfs Time to peak = 744 min Hyd. volume = 1,277 cuft

Max. Elevation = 1.21 ft Max. Storage = 255 cuft



Hydraflow Hydrographs by Intelisolve v9.2

Friday, Feb 9, 2018

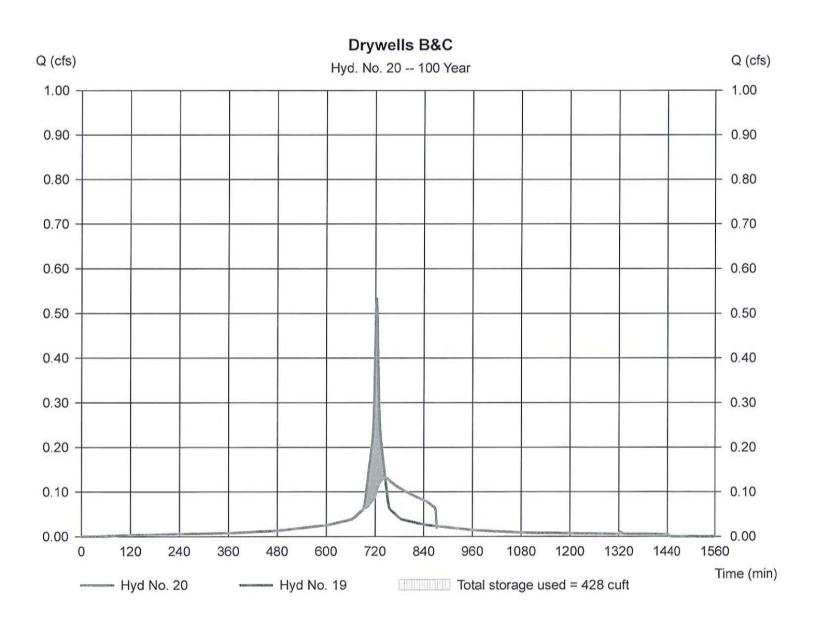
#### Hyd. No. 20

Drywells B&C

Hydrograph type = Reservoir Storm frequency = 100 yrs Time interval = 2 min

Inflow hyd. No. = 19 - Dwellings B&C Reservoir name = Roof Drywell B Peak discharge = 0.132 cfs
Time to peak = 744 min
Hyd. volume = 1,845 cuft
Max. Elevation = 2.12 ft

Max. Storage = 428 cuft



#### Pond No. 5 - Roof Drywells B&C

#### **Pond Data**

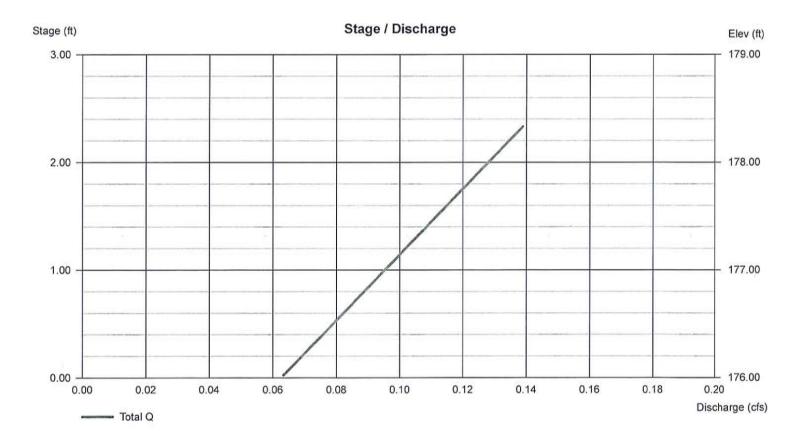
 $\textbf{UG Chambers - Invert elev.} = 176.50 \ \text{ft}, \ \text{Rise x Span} = 1.33 \ \text{x} \ 2.83 \ \text{ft}, \ \text{Barrel Len} = 28.48 \ \text{ft}, \ \text{No. Barrels} = 3, \ \text{Slope} = 0.00\%, \ \text{Headers} = \text{No Encasement - Invert elev.} = 176.00 \ \text{ft}, \ \text{Width} = 3.83 \ \text{ft}, \ \text{Height} = 2.33 \ \text{ft}, \ \text{Voids} = 40.00\%$ 

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	176.00	n/a	0	0
0.23	176.23	n/a	31	31
0.47	176.47	n/a	31	61
0.70	176.70	n/a	59	120
0.93	176.93	n/a	63	184
1.17	177.17	n/a	61	245
1.40	177.40	n/a	58	303
1.63	177.63	n/a	52	355
1.86	177.86	n/a	41	396
2.10	178.10	n/a	31	426
2.33	178.33	n/a	31	457

Culvert / Ori	fice Structu	res			Weir Structu	ires				
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]	
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00	
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00	
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33	
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	=				
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No	
Slope (%)	= 0.00	0.00	0.00	n/a						
N-Value	= .013	.013	.013	n/a						
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 8.270 (by	Wet area)			
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00				

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



	Worksheet 2: Runoff curve number and ru	unoff		SM-5676
Project:	443 Lincoln St	By PFK	Date 1/29/18	
Location:	Lexington, MA	Checked	Date	
Circle one:	Present Developed	Roof Drywell D		
1. Runoff curve	number (CN)			¥.
Soil name	Cover desc	cription		Area

Soil name and hydrologic	Cover description (cover type, treatment, and		CN 1/		Area	Product of CN x Area
group appendix A)	hydrologic condition: percent impervious: unconnected/connected impervious area ratio)	Table 2-2	Fig. 2-3	Fig. 2-4	Acres	
(4)	Impervious - Drive 0	98	ary her	destan	0.00	0.00
H <del>e</del> l	Impervious - Building 3,194	98	101120	1939	0.07	7.19
Α	Woods and Brush Good Condition 0	30	0000	opersi	0.00	0.00
A	Open Space Good Condition	39	ketai	2000 P	0.00	0.00
		90000	pools	росули	100	
		čen sta		51850	r de la co	
		interts	19 LUX	8,100.00		
		0.8834	SIDE!	BOULESE.	E 9.0	
/ Use only one CI	N source per line.			Totals =	0.07	7.19

CN (weighted) =	total	product	=	7.19	=	98.00	_3	Use CN =	98.0
ettere and a property and a second second	total	oron		0.07					

2. Runoff		Storm #1	Storm #2	Storm #3
Frequency	yr	11/18/11/	11/10/11/	1100
Rainfall, P (24-hour)	in	11/3/1/	11/4.5/1/	(1) 6,4
Runoff, Q	in	2.87	4.26	6,16
Runoff, Q	cf	763	1135 2-55 Second F	1640

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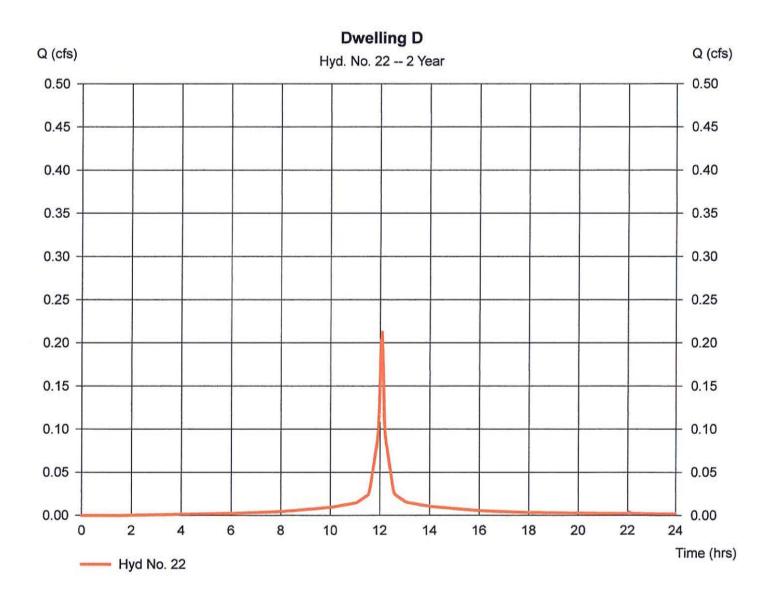
Wednesday, Feb 21, 2018

### Hyd. No. 22

Dwelling D

Hydrograph type = SCS Runoff Storm frequency = 2 yrs Time interval = 2 min Drainage area = 0.073 acBasin Slope = 0.0 %Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.213 cfs
Time to peak = 12.07 hrs
Hyd. volume = 715 cuft
Curve number = 98
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

Wednesday, Feb 21, 2018

### Hyd. No. 22

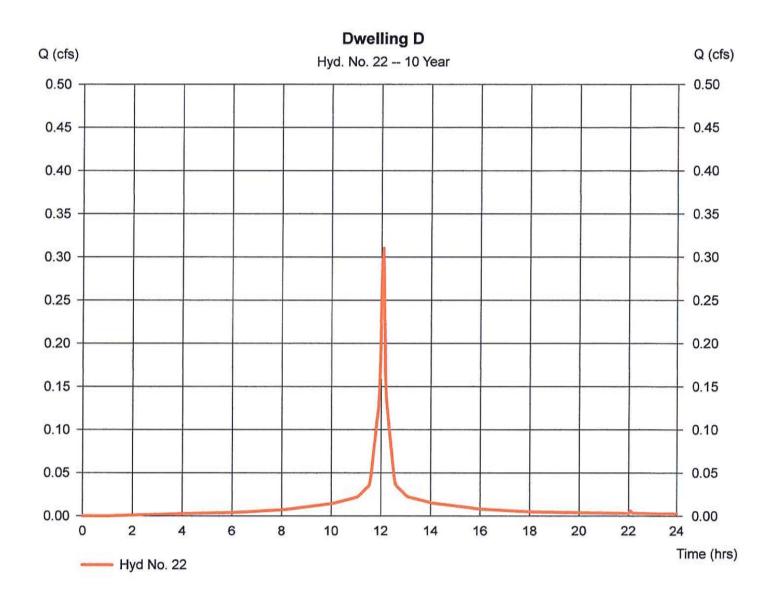
Dwelling D

Hydrograph type = SCS Runoff Storm frequency = 10 yrsTime interval = 2 min Drainage area = 0.073 acBasin Slope = 0.0 % Tc method = USER Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.311 cfsTime to peak = 12.07 hrsHyd. volume = 1,064 cuft Curve number = 98 Hydraulic length = 0 ftTime of conc. (Tc) =  $6.00 \, \text{min}$ 

= Type III Shape factor = 484

Distribution



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Wednesday, Feb 21, 2018

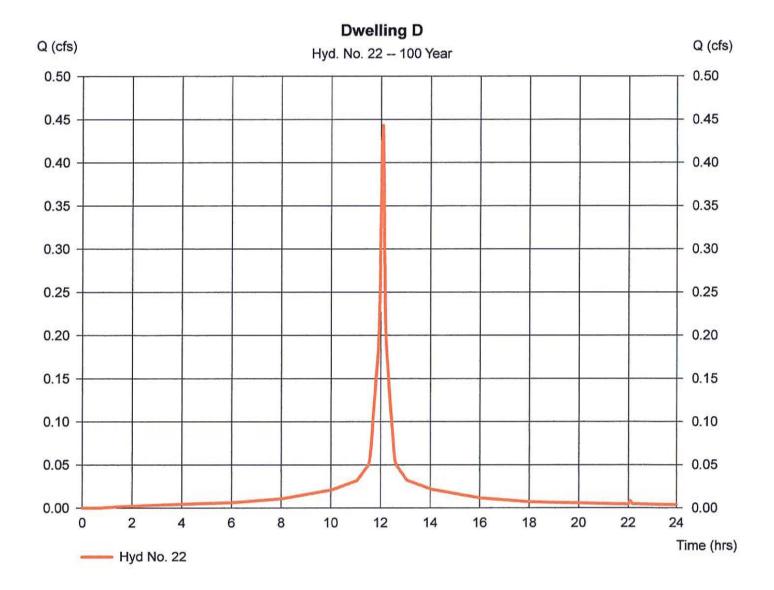
#### Hyd. No. 22

Dwelling D

= SCS Runoff Hydrograph type = 100 yrsStorm frequency Time interval = 2 min = 0.073 acDrainage area Basin Slope = 0.0 % Tc method = USER Total precip. = 6.40 inStorm duration = 24 hrs

Peak discharge = 0.443 cfs
Time to peak = 12.07 hrs
Hyd. volume = 1,537 cuft
Curve number = 98

Curve number = 98
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs by Intelisolve v9.2

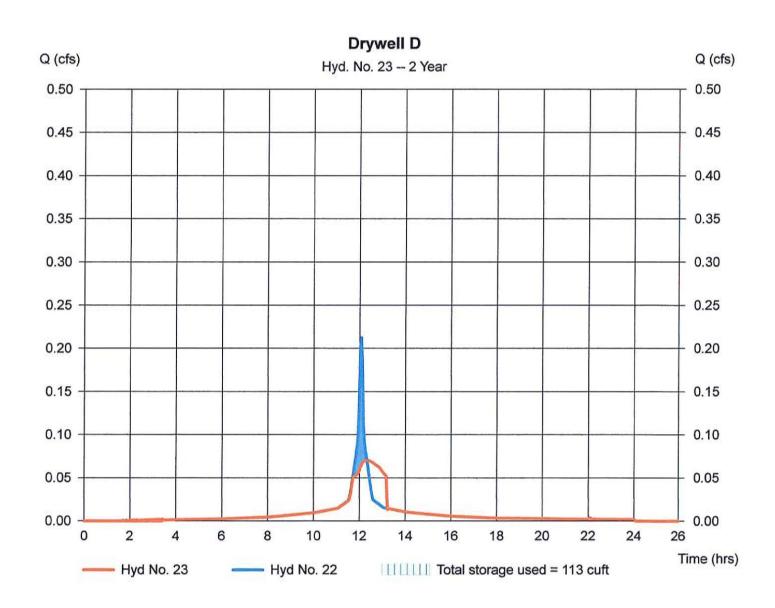
Wednesday, Feb 21, 2018

#### Hyd. No. 23

Drywell D

Hydrograph type = Reservoir
Storm frequency = 2 yrs
Time interval = 2 min
Inflow hyd. No. = 22 - Dwelling D
Reservoir name = Rood Drywell D

Peak discharge = 0.070 cfs
Time to peak = 12.33 hrs
Hyd. volume = 715 cuft
Max. Elevation = 176.78 ft
Max. Storage = 113 cuft



Hydraflow Hydrographs by Intelisolve v9.2

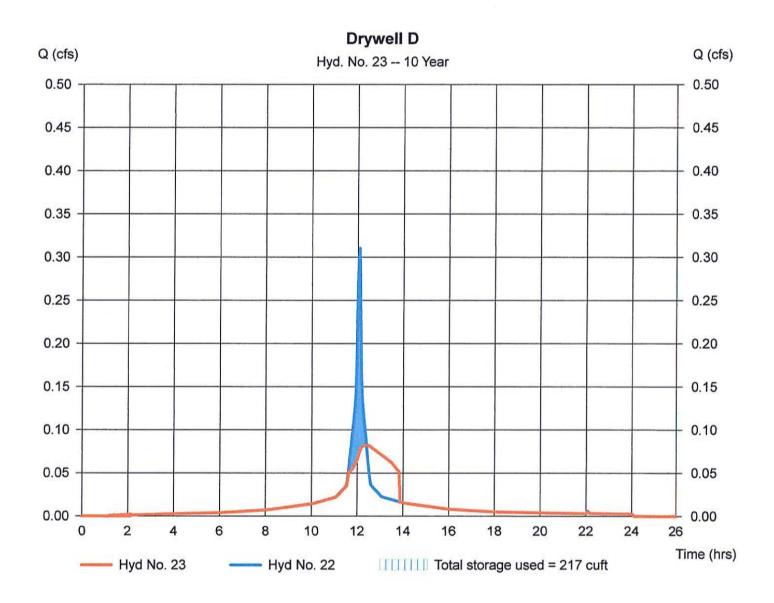
Wednesday, Feb 21, 2018

#### Hyd. No. 23

Drywell D

Hydrograph type = Reservoir Storm frequency = 10 yrs Time interval = 2 min

Inflow hyd. No. = 22 - Dwelling D Reservoir name = Rood Drywell D Peak discharge = 0.083 cfs
Time to peak = 12.40 hrs
Hyd. volume = 1,064 cuft
Max. Elevation = 177.29 ft
Max. Storage = 217 cuft



Hydraflow Hydrographs by Intelisolve v9.2

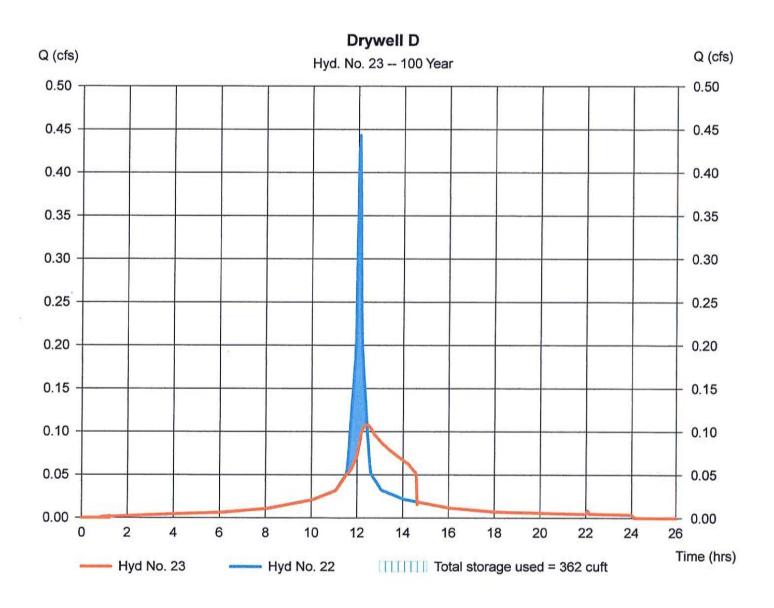
Wednesday, Feb 21, 2018

### Hyd. No. 23

Drywell D

Hydrograph type = Reservoir Storm frequency = 100 yrs Time interval = 2 min

Inflow hyd. No. = 22 - Dwelling D Reservoir name = Rood Drywell D Peak discharge = 0.108 cfs
Time to peak = 12.43 hrs
Hyd. volume = 1,537 cuft
Max. Elevation = 178.33 ft
Max. Storage = 362 cuft



Hydraflow Hydrographs by Intelisolve v9.2

Friday, Feb 9, 2018

#### Pond No. 9 - Rood Drywell D

#### **Pond Data**

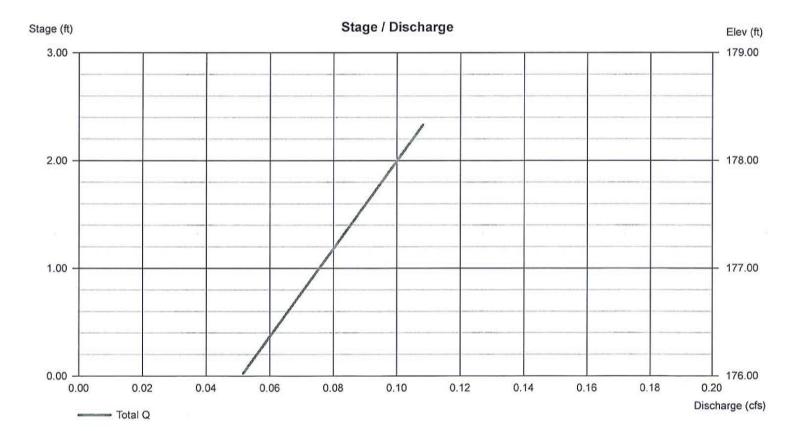
 $\begin{tabular}{ll} \textbf{UG Chambers - Invert elev.} = 176.50 \ ft, & Rise x Span = 1.33 x 2.83 \ ft, & Barrel Len = 21.36 \ ft, & No. Barrels = 3, & Slope = 0.00\%, & Headers = No Encasement - Invert elev. = 176.00 \ ft, & Width = 4.16 \ ft, & Height = 2.33 \ ft, & Voids = 40.00\% \end{tabular}$ 

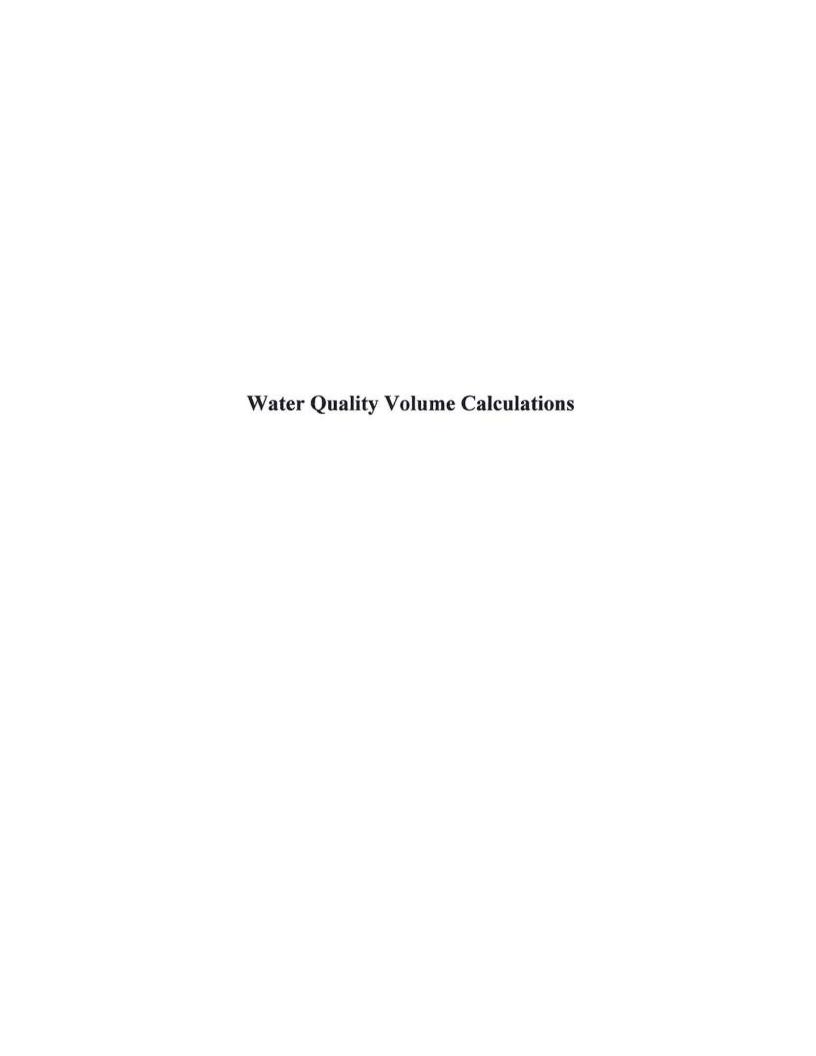
#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	176.00	n/a	0	0
0.23	176.23	n/a	25	25
0.47	176.47	n/a	25	50
0.70	176.70	n/a	46	96
0.93	176.93	n/a	49	146
1.17	177.17	n/a	48	193
1.40	177.40	n/a	45	239
1.63	177.63	n/a	41	280
1.86	177.86	n/a	33	312
2.10	178.10	n/a	25	337
2.33	178.33	n/a	25	362

Culvert / Ori	fice Structu	res			Weir Structu	ires				
	[A]	[B]	[C]	[PrfRsr]			[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	=	0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	=	0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	=	3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	=				
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	=	No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a	and the second second second					
N-Value	= .013	.013	.013	n/a						
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	=	8.270 (by	(Wet area)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	=	0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).





#### **Water Quality Volume Calculations**

Job: 5676

Calculated by: DJC Date: 2/21/2018

Infiltration Basin 1

Soils:

Hydrologic Group: A Required First Flush Volume

1 inch of runoff x impervious area

Impervious area:

0.34 acres

14,768 s.f.

Elev.	Change	Area	Inc.	
(FT)	Elev. (FT)	(SF)	Volume (CF)	
174.8	o	2635		
175	0.2	2990	562.5	
175.8	0.8	3741	2692.4	3254.9

Required Water Quality Volume

V= 14,768

s.f. x

<u>1</u> =

1,231 c.f.

Volume Provided

3,255 c.f.

3,255 c.f. > 1,231 c.f. O.K.

			į.
			*
Groundwater Red	charge Calculations		
			a a
		*	

#### **Recharge Volume Calculations**

Job: SM-5676 Calculated by: DJC

2/21/2018 Date:

Infiltration Basin 1 from Sub P-2A

Soils:

Hydrologic Group: Required Recharge Volume

0.6 inches of runoff x impervious area

Impervious area:

0.34 acres

14,768 s.f.

Required Recharge Volume (Rv)

Rv = 14,768 s.f. x 0.6 738 c.f.

12

Simple Dynamic Method

A=Rv / (D+KT)

Rv=A(D+kT)

D (depth of infiltration facility):

2.2 ft

K (saturated hydraulic conductivity): 8.27 inches/hour

0.69 feet/hour

T (time): 2 hours

> A= 2,635 s.f.

Voids= 1.00

> Rv= 9,429 c.f. 738 c.f.

72 Hour Drawdown

Rv/(K x Bottom Area)= 0.11 Hours

0.11 < 72 hours O.K.

#### **Recharge Volume Calculations**

Job: SM-5676 Calculated by: DJC

Date:

2/21/2018

Roof Drywell D

Soils:

Hydrologic Group: A Required Recharge Volume

0.6 inches of runoff x impervious area

Impervious area:

0.07 acres

2,967 s.f.

Required Recharge Volume (Rv)

Rv = 2,967 s.f. x 0.6 = 148 c.f.

12

Simple Dynamic Method

A=Rv / (D+KT)

Rv=A(D+kT)

D (depth of infiltration facility): 2.3

2.33 ft

K (saturated hydraulic conductivity): 8.27 inches/hour

0.69 feet/hour

0.69 leet/flou

T (time): 2 hours

A= 292 s.f. ids= 0.40

Voids= 0.40 Volume of Chambers= 132

Rv= 807 c.f. > 148 c.f.

72 Hour Drawdown

Rv/(K x Bottom Area)= 0.27 Hours

0.27 < 72 hours O.K.

## **Recharge Volume Calculations**

Job: SM-5676 Calculated by: DJC

Date: 2/21/2018

Roof Drywell B & C

Soils:

Hydrologic Group: A Required Recharge Volume

0.6 inches of runoff x impervious area

Impervious area:

0.09 acres

3,847 s.f.

Required Recharge Volume (Rv)

Rv = 3,847 s.f. x 0.6 = 192 c.f.

12

Simple Dynamic Method

A=Rv / (D+KT)

Rv=A(D+kT)

D (depth of infiltration facility): 2.3

2.33 ft

K (saturated hydraulic conductivity): 8.27 inches/hour

0.27 inches/nour

0.69 feet/hour

T (time): 2 hours

A= 351 s.f.

Voids= 0.40

Volume of Chambers= 176

Rv= 986 c.f. > 192 c.f.

72 Hour Drawdown

Rv/(K x Bottom Area)= 0.28 Hours

0.28 < 72 hours O.K.

## **Recharge Volume Calculations**

Job: SM-5676 Calculated by: DJC

Date: 2/21/2018

Roof Drywell A

Soils:

Hydrologic Group: A Required Recharge Volume

0.6 inches of runoff x impervious area

Impervious area:

0.06 acres

2,669 s.f.

Required Recharge Volume (Rv)

Rv = 2,669 s.f. x 0.6 = 133 c.f.

12

Simple Dynamic Method

A=Rv/(D+KT)

Rv=A(D+kT)

D (depth of infiltration facility): 2.33 ft

K (saturated hydraulic conductivity): 8.27 inches/hour

0.69 feet/hour

T (time): 2 hours

A= 292 s.f. Voids= 0.40

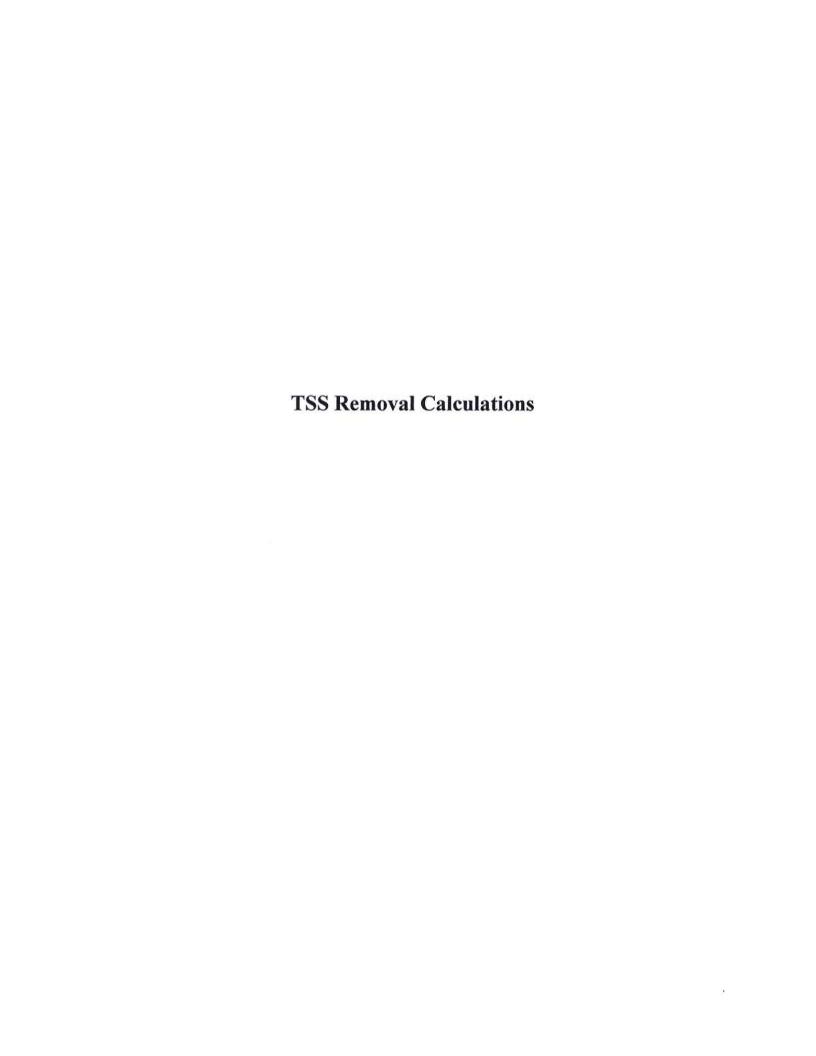
Volume of Chambers= 132

Rv= 806 c.f. > 133 c.f.

72 Hour Drawdown

Rv/(K x Bottom Area)= 0.24 Hours

0.24 < 72 hours O.K.



# INSTRUCTIONS:

- 1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table
  - 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
    - 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row
- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
  - 5. Total TSS Removal = Sum All Values in Column D

	Ш	Remaining	0.75	0.56				Separate Form Needs to be Completed for Each Outlet or BMP Train	n previous BMP (E)
	۵	Amount Removed (B*C)	0.25	0.19				44%	*Equals remaining load from previous BMP (E)
% Removal)	O	Starting TSS Load*	1.00	0.75				Total TSS Removal =	
Infiltration Basin (44% Removal)	В	TSS Removal Rate <sup>1</sup>	25%	25%				Total T	oject: 5676 d By: PFK Date: 2/20/2018
Location:	Ą	BMP <sup>1</sup>	Deep Sump Hooded Catch Basin	Sediment Forebay				,	Project: 5676 Prepared By: PFK Date: 2/20/
			, jəəu	orksl			ls2		
				levoi	Rem	SST			

# INSTRUCTIONS:

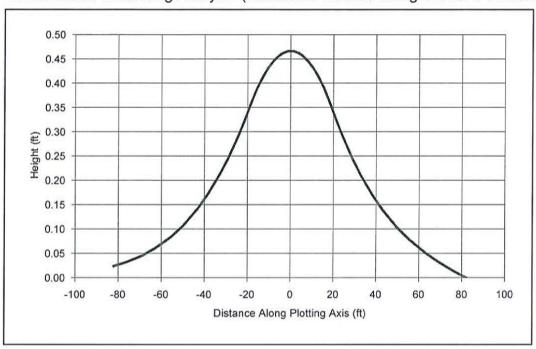
- 1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table
  - 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
    - 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row
      - 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
        - 5. Total TSS Removal = Sum All Values in Column D

				1	1	II .	1	77			
	Ш	Remaining Load (C-D)	0.75	0.15				Separate Form Needs to be Completed for Each Outlet or BMP Train	7	m previous BMP (E)	
	۵	Amount Removed (B*C)	0.25	9.0				85%		*Equals remaining load from previous BMP (E)	which enters the BMP
	O	Starting TSS Load*	1.00	0.75				Total TSS Removal =			
Subcatchment P-2A	В	TSS Removal Rate <sup>1</sup>	25%	80%				Total T	5676	PFK	Date: 2/20/2018
Location:	۷	BMP¹	Deep Sump Hooded Catch Basin	Infiltration Basin (with Sediment Forebay)					Project: 5676	Prepared By: PFK	Date:
			วูออน	orks			Cal				
				Ibvoi	Rem	SST					



# INFILTRATION BASIN 1

## Groundwater Mounding Analysis (Hantush's Method using Glover's Solution)



COMPANY:	Stamski and McNary,	Inc.
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PROJECT: 5676

ANALYST: PFK

DATE: 2/21/2018 TIME: 8:47:46 AM

**INPUT PARAMETERS** 

Application rate: 0.28 c.ft/day/sq. ft Duration of application: 1 days

Fillable porosity: 0.24

Hydraulic conductivity: 39 ft/day Initial saturated thickness: 7 ft Length of application area: 75 ft Width of application area: 38 ft Constant head boundary used at: 82 ft Plotting axis from Y-Axis: 90 degrees Edge of recharge area:

positive X: 19 ft positive Y: 0 ft

Total volume applied: 798 c.ft

## MODEL RESULTS

X (ft)	Y (ft)	Plot Axis (ft)	Mound Height (ft)
-82	0	-82	0.02
-69	Ö	-69	0.04
-55.9	Ö	-56	0.08
-42.9	O	-43	0.14
-32.6	0	-33	0.21
-24.7	0	-25	0.29
-18.2	0	-18	0.36
-12.7	0	-13	0.42
-7.9	0	-8	0.45
-4.8	0	-5	0.46
-2.6	0	-3	0.46
0	0		0.47
2.6	0	0 3 5	0.46
4.8	0	. 5	0.46
7.9	0	8	0.45
12.7	0	13	0.42
18.2	0	18	0.36
24.7	0	25	0.29
32.6	0	33	0.21
42.9	0	43	0.14
55.9	0	56	0.08
69	0	69	0.03
82	0	82	0
	0		



DESIGN STORM: 100 YEAR

DATE:

2/12/2018

DONE BY: FILE:

PFK

5676 RATIONAL METHOD

PROJECT:

SM-5676

LOCATION: Lexington, MA

			TRIBUTA	RY AREA	TIME	_		DRA	AIN INV.	GRO	UND
	0.000				TO	ANHOLE		ELE	VATION	SUR	FACE
FROM	то	LENGTH (FT)	INCR. (ACRES)	TOTAL (ACRES)	UPPER END (MIN)	NVERT DROP (FT)	FALL IN PIPE (FT)	UPPER END	LOWER END	UPPER END	LOWER END
CB-1	DMH-1	182	0.28	0.28	10		0.91	176.23	175.32	178.80	182.40
CB-3	DMH-1	76	0.15	0.15	10		1.31	176.63	175.32	180.80	182.40
CB-2	DMH-1	37	0.2	0.20	10	M	0.74	176.06	175.32	180.80	182.40

1 of 3

Project:

443 Lincoln St

Ву

PFK Date

2/12/2018

Location:

Lexington, MA

Checked

Date

## **Rational Method**

Q = peak flow rate, (cfs)

i = rainfall intensity inches/hour

C = runoff coefficient,

A = area (ac)

C = 0.90 impervious

C = 0.20 landscaped / grass

C = 0.15 woods

## CB-1 to DMH-1

Surface Cover		A (ac)	С		Product A x C
impervious		0.14	0.9		0.126
lands/grass		0.14	0.2		0.028
woods	<u>.</u>	0.00	0.15		0
	sum =	0.28		sum =	0.154
	C =	0.55	= total product / total	area	

Project:

443 Lincoln St

Ву

PFK Date

2/12/2018

Location:

Lexington, MA

Checked

Date

## **Rational Method**

Q = peak flow rate, (cfs)

i = rainfall intensity inches/hour

C = runoff coefficient,

A = area (ac)

C = 0.90 impervious

C = 0.20 landscaped / grass

C = 0.15 woods

## CB-3 TO DMH-1

Surface Cover		A (ac)	C	Product A x C
impervious		0.07	0.9	0.063
lands/grass		0.08	0.2	0.016
woods			0.15	0
	sum =	0.15	sum =	0.079
	c _	0.52	total avaduat / total avaa	

C = 0.53 = total product / total area

3 of 3

Project:

443 Lincoln St

Ву

PFK Date

2/12/2018

Location:

Lexington, MA

Checked

Date

## **Rational Method**

Q = peak flow rate, (cfs)

i = rainfall intensity inches/hour

C = runoff coefficient,

A = area (ac)

C = 0.90 impervious

C = 0.20 landscaped / grass

C = 0.15 woods

## CB-2 TO DMH-1

Surface Cover		A (ac)	С		Product A x C
impervious		0.13	0.9		0.117
lands/grass		0.07	0.2		0.014
woods			0.15		0
	sum =	0.2		sum =	0.131

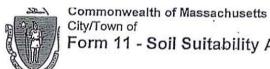
0.66

= total product / total area



# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

	C. C	Observatio		・ (minimum で 1子・		2 1520	9777 V 4		Sun	1 500x	
	1. Loc		10.00		Da	ite	Time		Weathe	1	
*	20	Ground Elevation	on at Surfa	ce of Hole				v*			
	1	Location (Identi	fy on Plan	<u> </u>	443	LINC	OLN.	STYLE	een.		
		III a a a a la l				EK		-			*
	z. Lai	(e.g. woo	dland, agricu	illural field, vacan	nt lot, etc.)	— <u>-'</u> ' - <u>-</u>	<u>z</u> -	Surface Stones		Slope (%)	
		Vegetatio		_ ±	5	Landform			Position on lan	dscape (allach shee	et)
	3. Dista	ances from: O	pen Water	Body	Drain	nage Way	Possil	ble Wet Area	3		•
(*)		, P	roperty Lin	feet	Drinking V	Vater Well	Othe	er (O	OFF SH	FO	
0	4 Pero	nt Material:	Popal.	acim					with the same and	No. 200	×
								•	esent: Yes		
	II Yes	s: Disturbed 8	SOIL F	III Material	Impervio	ous Layer(s)	Weathere	d/Fractured	Rock☐ Bedro	ock_	
	5. Grou	ndwater Observ	/ed: Yes		. 4 3	-		*	*		
	· If Yes	: Depth We	eping from	Pit_100	_ Dept	th Standing Wa	ter in Hole_				
	Ection	ated Death to I	lich Crous	duator							
	LSUIT	ated Depth to F	ngii Grout	idwater.							
		eated Depth to F	ngii Gioui	idwater	٠.			•			
		iated Depth to F	ngir Grour	iowater		· ·				*	*
		* # # * # #		7		•			*	e A	e e
Deep		ation Hole Nu		7	7-1	· ·		i	*	e n	* 1
Depth		Soll Matrix:	ımber:	7		Soil Texture	Coarse I	Fragments Volume	Soil Structure	Soil Consistence	Oth
G: G:	p Observa	ation Hole Nu	ımber:	· · · · · · · · · · · · · · · · · · ·		Texture (USDA)	Coarse F % by Gravel	Fragments Volume Cobbles & Stones	Soil Structure		Oth
Depth	p Observa	Soll Matrix:	Imber:Redo	oximorphic Fe	atures	Texture (USDA)	% by	Volume Cobbles	Soil Structure	Consistence	Oth
Depth (In:)	p Observa	Soll Matrix: Color-Moist (Munsell)	Redo	oximorphic Fer (mottles)	Percent	Texture (USDA)	% by	Volume Cobbles	Soil Structure	Consistence	Oth
Depth (In:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  Gran	Redo Depth	oximorphic Fer (mottles)  Color  RANG	Percent	Texture (USDA)	% by	Volume Cobbles	Soil Structure	Consistence (Moist)	Oth
Depth (In:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)	Depth	oximorphic Fer (mottles)	Percent	Texture (USDA)	% by T	Volume Cobbles	Soil Structure	Consistence (Moist)	2
Depth (In:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  GRAN  2154  2154	Depth	oximorphic Fer (mottles)  Color  RAMA  GEN  Pagh	Percent	Texture (USDA)	% by T	Volume Cobbles & Stones	Soil Structure	VERY FRIARY	£
Depth (In:)	Soil Horizon/Layer  Fill  C  C  C  C  C  C  C  C  C  C  C  C	Soli Matrix: Color-Moist (Munsell)  Gran  Gran  2154  2154  2154  2154	Depth	oximorphic Fer (mottles)  Color  RAMA  GEN  Pagh	Percent	Texture (USDA)	% by T	Cobbles & Stones	M	Consistence (Moist)  VERY FREAR	£
Depth (In:)	Soil Horizon/Layer	Soll Matrix: Color-Moist (Munsell)  GRAN  2154  2154	Depth	oximorphic Fer (mottles)  Color  RAMA  GEN  Pagh	Percent	Texture (USDA)	% by T	Cobbles & Stones	M	VERY FRIARY	£
Depth (In:)	Soil Horizon/Layer  Fill  C  C  C  C  C  C  C  C  C  C  C  C	Soli Matrix: Color-Moist (Munsell)  Gran  Gran  2154  2154  2154  2154	Depth	oximorphic Fer (mottles)  Color  RAMA  GEN  Pagh	Percent	Texture (USDA)	% by T	Cobbles & Stones	M	VERY FRIARY	£
Depth (In:)	Soil Horizon/Layer  Fill  C  C  C  C  C  C  C  C  C  C  C  C	Soli Matrix: Color-Moist (Munsell)  Gran  Gran  2154  2154  2154  2154	Depth	oximorphic Fer (mottles)  Color  RAMA  GEN  Pagh	Percent	Texture (USDA)	% by T	Cobbles & Stones	M	VERY FRIARY	£
Depth (In:)	Soil Horizon/Layer  Fill  C  C  C  C  C  C  C  C  C  C  C  C	Soli Matrix: Color-Moist (Munsell)  Gran  Gran  2154  2154  2154  2154	Depth	oximorphic Fer (mottles)  Color  RAMA  GEN  Pagh	Percent	Texture (USDA)	% by T	Cobbles & Stones	M	VERY FRIARY	£



# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

	1. Loc	ation			Da	te	Time		* Weather		
5	. 0	Ground Elevation	on at Surfa	ace of Hole			8 (f)				
	L	ocation (Identi	fy on Plan	<u> </u>	443	LINC	OLN.	STYLE	een .		ň
						756		W.			
	z. Lan	d Use:(e.g. woo	dland, agricu	ultural field, vacan	nt lot, etc.)	— i, - i,	<u> </u>	Surface Stones		Slope (%)	-
		Vegetatio	in :	<u>+</u>	. •	Landform			Position on land	dscape (allach sheel	1
0	3. Dista	ances from: O	pen Water	Body	_ Drain	age Way	Possi	ble Wet Area		oscope (alloca arree)	
		Р	roperty Lir	feet ne	Drinking W	Vater Well feet	Othe				
		A)'	192								
	4. Parer	nt Material:	4109	Jacobi	<u> </u>		Unsuitable	Materials Pr	esent: Yes 🗌	No 🗌	*
3	If Yes	: Disturbed	Soil F	ill Material□	Impervio	ous Layer(s) 🗌	Weathere	d/Fractured	Rock Bedroo	ck[	8
		ndwater Obser			i i				8		
× .		: Depth We				(h Gt" te:					
		ated Depth to I				th Standing Wa		•	TO FIL	, MAG	Z1 ().
	· ·····	eted Deptin to r	ngn Groui	nowater: _		The inertain	MARON.	000	TO FIL	· Consti	SCK.
						LONGE	( Criv Tru	( 5 > 1	11 Color 1 50	6 m	=0
			¥							1 1 1 1	Court of
• • • •		4 1 1	¥					TA	ST. PI	73	
Dee	p Observa	ation Hole Nu	umber:	TP 1			···	. 73	ST. PI	73	
Dee		ation Hole Nu		,	76			. 73	ST. PI	73	
Depth	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)		oximorphic Fe	76	Soli Texture	Coarse	· · · · · · · · · · · · · · · · · · ·	Soil Structure	Soil Consistence	
	Soil Horizon/	Soll Matrix: Color-Moist		oximorphic Fe	76	Soli Texture (USDA)	Coarse	Fragments Volume	ST. PI	Soil	
Depth (In:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist	Red	oximorphic Fe (mottles)	7- 6	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure	Soil Consistence (Moist)	Ott
Depth (in:)	Soil Horizon/	Soll Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	7- 6	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)	Oth
Depth (In:)	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	atures Percent	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure	Soil Consistence (Moist)	Ott
Depth (In:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	7- 6	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)	Ott
Depth (In:)	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	atures Percent	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)	Ott
Depth (In:)	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	atures Percent	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)	Ott
Depth (In:)	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	atures Percent	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)	Ott
Depth (In:)	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	Percent	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)	Ott
Depth (In:)	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	Percent	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)	Ott
Depth (In:)	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	Percent	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)	Ott
Depth (In:)	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	Percent	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)	Ott
Depth (In:)	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)	Red	oximorphic Fe (mottles)	Percent	Soli Texture (USDA)	Coarse I	Fragments Volume	Soil Structure  Boucer	Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)  Soil Consistence (Moist)	Ott

	Deep	Observatio		W 17	3 13	2 15 20	17		SW	2000	
	1. Loc	ation			Dat	e	Time		Weather	V.	
5.	(	Ground Elevation	on at Surfa	ce of Hole				·*			
		ocation (Identi			443	LINC	1410	Z 54 8	a property		2
								31120	mate Pathy at 1		
	2. Lan	d Use:(e.g. woo	dland ander	llural field wasan	t let ele l		٤.				
					t lot, etc.)			Surface-Stones		Slope (%)	
		Vegetatio			W 81	Landform			Position on land	dscape (allach sheel	)
	<ol><li>Dista</li></ol>	ances from: O	pen Water	Body	_ Draina	age Way	Possil	ble Wet Area			•
(2)		. P	roperty Lin	e [	Drinking W	ater Well [eet	Othe	er-			
					4	1777/1776					
	4. Parer	nt Material:	10:	glacia	<u> </u>		Unsuitable !	Materials Pre	esent: Yes 🗌	No 🗌	
	If Yes	: Disturbed	Soil F	ill Material	Impervio	us Layer(s) 🗌	Weathere	d/Fractured	Rock Bedro	ck[	
	· F . C			A =							
		ndwater Observ				÷					
		: Depth We		. 1	_ Depti	h Standing Wa	ter in Hole_		3		
	Estim	ated Depth to I	ligh Grour	ndwater:	50						ž.
						3	1997	*		*	
			- 2								
* **					***********						
* **		• • •			*********				8 0		160
Dee	p Observa	ation Hole Nu	ımber:	TP I	7-7		•••••••••••••••••••••••••••••••••••••••	) #			
Dee	Q1			*					3		
	Soil Horizon/	Soll Matrix:		oximorphic Fea		Soll	Coarse F	Fragments	Soil Structure	Soil	· ·
epth	Soil	Soll Matrix:	Red	oximorphic Fea (mottles)	atures	Soli Texture (USDA)	% by"	Volume	Soil Structure	Soil Consistence (Moist)	Oth
epth	Soil Horizon/	Soll Matrix: Color-Moist		oximorphic Fea		Texture	Coarse F % by '	Fragments Volume Cobbles & Stones	Soil Structure	Consistence	Oth
epth (In:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist	Red	oximorphic Fea (mottles)	atures	Texture (USDA)	% by"	Volume	Soil Structure	Consistence	
epth (in:)	Soil Horizon/	Soll Matrix: Color-Moist	Red	oximorphic Fee (mottles)	atures	Texture	% by"	Volume		Consistence (Moist)	Oth
epth (in:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist	Red	Color	Percent	Texture (USDA)  FILL SAMO	% by"	Volume		Consistence (Moist)	
epth (in:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist	Red	oximorphic Fee (mottles)	atures	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	eric
epth (in:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	eryc
epth (in:)	Soil Horizon/Layer	Soll Matrix; Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	eric
Pepth (In:)	Soil Horizon/ Layer	Soll Matrix; Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	eryc
Pepth (In:)	Soil Horizon/Layer	Soll Matrix; Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	eryc
lepth (In:)	Soil Horizon/Layer	Soll Matrix; Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	eryc
Pepth (In:)	Soil Horizon/Layer	Soll Matrix; Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	eryc
lepth (In:)	Soil Horizon/Layer	Soll Matrix; Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	eryc
Pepth (In:)	Soil Horizon/Layer	Soll Matrix; Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	2 Mc
lepth (In:)	Soil Horizon/Layer	Soll Matrix; Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	2 Mc
Pepth (In:)	Soil Horizon/Layer	Soll Matrix; Color-Moist (Munsell)	Red	Color	Percent	FILL SAVO WLOW	% by"	Volume		Consistence (Moist)	2 Mc

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

	1. Loc	Observatio	ii noie i	vamber: _	H 13	-	Time	<del></del>	Weather	2005	
		Ground Elevation	n at Surfa	ice of Hole				*			
	*	ocation (Identi		/ -	443	LING	O	5 500	ou gaintpropers		2
		Location (locities	y on rian	/		Cinco	CON.	STYLE	三位.	W	
	2. Lar	d Use:(e.g. woo	dland, agricu	illural field, vacan	t lot, etc.)		<u>د</u> ج	urface-Stones		Slope (%)	
		Vegetatio	L.	<u>+</u>		Landform					
	3. Dista	ances from: O	oen Water	Body -	Draina	age Way	Possib	ole Wet Area		dscape (allach shee	
		P	operty Lin	feet le(	– Drinking W	ater Well	Othe				
			100			feet	•				
	4. Parei	nt Material:	KVO:	g live or	1		Unsuitable N	Materials Pre	esent: Yes 🗌	No 📋	
	If Yes	: Disturbed	Soil□ F	ill Material□	Impervio	us Layer(s) 🗌	Weathered	d/Fractured	Rock Bedroo	ck 🗀	
-	5. Groui	ndwater Observ	ed: Yes	□ No □				8			
	If Yes			Pit_ 80	Depti	h Standing Wa	ter in Hole				
	Estim	ated Depth to F	O-Million Million College		70	1		•	•		
		0.0					3				
٠		* 4 *	×						9		9
p	Observa	ation Hole Nu	ımber:	TÖ 1	Lal			3	9		# 124
p		ation Hole Nu	ımber:	TP 1	7-6	_		,	e IX		
Т	Soil Horizon/	Soll Matrix: Color-Moist		eximorphic Feat (mottles)	7 L	Soli Texture	Coarse F % by \	ragments /olume	Soil Structure	Soil Consistence	Othe
Т	Soil	Soll Matrix:		oximorphic Fea	7 - Lo	Texture (USDA)	Coarse F % by \	/olume Cobbles	Soil Structure		Othe
Т	Soil Horizon/	Soll Matrix: Color-Moist	Redo	oximorphic Fea (mottles)		Texture (USDA)	% by \	/olume	Soil Structure	Consistence	Othe
Т	Soil Horizon/	Soli Matrix: Color-Moist (Munsell)	Redo	oximorphic Fea (mottles)		Texture (USDA)	% by \	/olume Cobbles	Soil Structure	Consistence	Othe
Т	Soil Horizon/	Soli Matrix: Color-Moist (Munsell)	Redo	oximorphic Fee (mottles)  Color		SL LS	% by \	Cobbles & Stones	Soil Structure  M  M	Consistence (Moist)	Othe
Т	Soil Horizon/ Layer	Soli Matrix: Color-Moist (Munsell)  IOUR 3/2  IOUR 4/4  Z-54	Redo	oximorphic Fer (mottles)	Percent	SL LS SACO MEO	% by \	Cobbles & Stones	M	Consistence (Moist)	Othe
Т	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1042 312 1042 4/4 2.54 6/1	Redo	oximorphic Fee (mottles)  Color	Percent	SL LS SANO MEO	% by \	Cobbles & Stones	M	Consistence (Moist)	Othe
Т	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1042 312 1042 4/4 2.54 6/1	Redo	oximorphic Fee (mottles)  Color	Percent	SL LS SANO MEO	% by \	Cobbles & Stones	M	Consistence (Moist)	Othe
Т	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1042 312 1042 4/4 2.54 6/1	Redo	oximorphic Fee (mottles)  Color	Percent	SL LS SANO MEO	% by \	Cobbles & Stones	M	Consistence (Moist)	Othe
Т	Soil Horizon/Layer	Soll Matrix: Color-Moist (Munsell)  1042 312 1042 4/4 2.54 6/1	Redo	oximorphic Fee (mottles)  Color	Percent	SL LS SANO MEO	% by \	Cobbles & Stones	M	Consistence (Moist)	Othe

	_										
		On-Site Re		70 17.		es recondate		sed disposal	area)	- 47	
	Dee	p Observatio	n Hole I	Number: _	2 13 Dat	2/15/20		<u> </u>	SW	2005	
	1. Lo	cation			Dat	16	Time		Weathe	r	
5		Ground Elevation						120			
		Location (Identi	fy on Plan	<u> </u>	443	LINC	OLN.	STYLE	E E		
	2. La	and Use:				FA F	٠.		S		*
		(e.g. woo	odland, agricu	ultural field, vacan	nt lot, etc.)		= 5	Surface Stones		Slope (%)	
		Vegetatio	in :	_ +	,	Landform		·	Position on lan	dscape (allach sheel	
	3. Dis	tances from: O	pen Water	Body	_ Draina	age Way	Possit	ole Wet Area		boope (allacii siree)	ž
		Р	roperty Lin	feet feet	Drinking W	leet Vater Well	Othe				
		*		27		feet					
	4. Pare	ent Material:	LVi	59/44	r_		Unsuitable N	Materials Pre	esent: Yes 🗌	No 🗗	8
	If Y∈	es: Disturbed	Soil F	ill Material□	Impervio				Rock☐ Bedro		
							*	enc management B	Se contra de la contra del la contra del la contra del la contra de la contra del la c		
		indwater Obser				VW Or Japan Agenty					
	· If Ye	s: Depth We	epina from	Pit man	Depti	h Standing Wa	ter in Hole	*Arriban	2		
		SALTECT AND AND AN AN ANALOGO SERVICES							2.7		
	Estin	nated Depth to I							wins	12706	*
	Estin	SALTECT AND AND AN AN ANALOGO SERVICES							non	· ~ 7 06	**
•		nated Depth to I	High Grour	ndwater:					Lower	×20%	:#: * *
eep		SALTECT AND AND AN AN ANALOGO SERVICES	High Grour	ndwater:					Lower	12706	85 15 15
- 	Observ	nated Depth to I	ligh Grour	TP 1	7-5	\\	6W. D	<u> 26 40</u> LESEA	*		: :
h	Observ	ration Hole Nu	ligh Grour	ndwater:	7-5	Soil Texture	Coarse F		Soil Structure	Soil Consistence	Other
	Observ	ration Hole Nu Soll Matrix: Color-Moist (Munsell)	ligh Grour	oximorphic Fe	7-5	Soll Texture (USDA)	Coarse F	UE SEA	*	Soil	Other
1	Observ	ration Hole Nu Soll Matrix: Color-Moist (Munsell)	Jimber:	oximorphic Fer	7-5	Soli Texture (USDA)	Coarse F % by \	TE SEA	Soil Structure	Soil Consistence	Other
1	Observ	sation Hole Nu Soll Matrix: Color-Moist (Munsell)	Jimber:	oximorphic Fer	7-5	Soll Texture (USDA)	Coarse F % by \	TE SEA	*	Soil Consistence	Other
1	Observ	ration Hole Nu Soll Matrix: Color-Moist (Munsell)	Jimber:	oximorphic Fer	7-5	Soll Texture (USDA)	Coarse F % by \	TE SEA	Soil Structure	Soil Consistence (Moist)	Other
1	Soil Horizon/ Layer	ation Hole Nu Soll Matrix: Color-Moist (Munsell)	Jmber: Redo Depth	oximorphic Fer (mottles)	7-5	Soil Texture (USDA)	Coarse F % by V	TE SEA	Soil Structure	Soil Consistence (Moist)	Other
	Soil Horizon/ Layer	sation Hole Number of Soli Matrix: Color-Moist (Munsell)  104/C 31/Z  104/C 4/4  VAraguita	Jmber: Redo	oximorphic Fer (mottles)	7-5 atures	Soil Texture (USDA)  SL  LS	Coarse F % by V	TE SEA	Soil Structure  M	Soil Consistence (Moist)	Other
	Soil Horizon/ Layer	sation Hole Number of Soli Matrix: Color-Moist (Munsell)  104/C 31/Z  104/C 4/4  VAraguita	Jmber: Redo	oximorphic Fer (mottles)	7-5 atures	Soil Texture (USDA)	Coarse F % by V	TE SEA	Soil Structure  M  M	Soil Consistence (Moist)	Other
	Soil Horizon/ Layer	ation Hole Nu Soll Matrix: Color-Moist (Munsell)	Jmber: Redo	oximorphic Fer (mottles)	7-5 atures	Soll Texture (USDA)  SL  LS  SAVO WEGIMA	Coarse F % by V	TE SEA	Soil Structure  M	Soil Consistence (Moist)	Other
	Soil Horizon/ Layer	sation Hole Number of Soll Matrix: Color-Moist (Munsell)  104/C 31/Z  Loy/C 4/4  VAragains Loy/C Colors Loy/C	Jmber: Redo	oximorphic Fer (mottles)	75 atures  Percent	Soll Texture (USDA)  SL  LS  SAVO  WEGINA  SAVO	Coarse F % by V	TE SEA	Soil Structure  M  M	Soil Consistence (Moist)	Other
	Soil Horizon/ Layer	sation Hole Number of Soli Matrix: Color-Moist (Munsell)  104/C 31/Z  104/C 4/4  VAraguita	Jmber: Redo	oximorphic Fer (mottles)	75 atures  Percent	Soll Texture (USDA)  SL  LS  SAVO  WEGINA  SAVO	Coarse F % by V	TE SEA	Soil Structure  M  M	Soil Consistence (Moist)	Other
	Soil Horizon/ Layer	sation Hole Number of Soll Matrix: Color-Moist (Munsell)  104/C 31/Z  Loy/C 4/4  VAragains Loy/C Colors Loy/C	Jmber: Redo	oximorphic Fer (mottles)	75 atures  Percent	Soll Texture (USDA)  SL  LS  SAVO  WEGINA  SAVO	Coarse F % by V	TE SEA	Soil Structure  M  M	Soil Consistence (Moist)	Other
	Soil Horizon/ Layer	sation Hole Number of Soll Matrix: Color-Moist (Munsell)  104/C 31/Z  Loy/C 4/4  VAragains Loy/C Colors Loy/C	Jmber: Redo	oximorphic Fer (mottles)	75 atures  Percent	Soll Texture (USDA)  SL  LS  SAVO  WEGINA  SAVO	Coarse F % by V	TE SEA	Soil Structure  M  M	Soil Consistence (Moist)	Other
1	Soil Horizon/ Layer	sation Hole Number of Soll Matrix: Color-Moist (Munsell)  104/C 31/Z  Loy/C 4/4  VAragains Loy/C Colors Loy/C	Jmber: Redo	oximorphic Fer (mottles)	75 atures  Percent	Soll Texture (USDA)  SL  LS  SAVO  WEGINA  SAVO	Coarse F % by V	TE SEA	Soil Structure  M  M	Soil Consistence (Moist)	Other

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

	1. Lo	p <sub>.</sub> Observatio	again 19-12-12-12-12-12-12-12-12-12-12-12-12-12-		Dat	te	Time		Weathe	ar .	
-		Ground Elevation					» - 2				
		Location (Identi	fy on Plan	)	443	LING	OLN.	STRE	E E		ü
	2. La	nd Use;	WOO	MANO	0.59	De					1.
		(e.g. woo	dland, agricu	llural field, vacan	it lot, etc.)		= 1	Surface Stones		Slope (%)	
		Vegetatio	in :-	_ ±		Landform		•	Position on lar	ndscape (allach sheel	1)
	3. Dist	ances from: O	pen Water	Body	_ Drain	age Way	Possi	ble Wet Area			,
2.80		. Р	roperty Lin	e I	Drinking W	/ater Well	Othe	er.			
		¥.	122	lagraz		37,70	84 A 24 1				
		nt Material:					and the second second		esent: Yes		
	If Ye	s: Disturbed	Soll F	ill Material	Impervio	us Layer(s) 🗌	Weathere	ed/Fractured	Rock□, Bedro	ock[	
	5. Grou	indwater Observ	ved: Yes	□ . No □		1		, ,	8		
•	· If Ye	s: Depth We	eping from	Pit	_ Dept	h Standing Wa	ter in Ḥole _		i		
	Estin	nated Depth to H	ligh Groun	ndwater:	26				senvec		
			20			L	Kery	012	our c		,
		* * *					no x			Acres .	12
5.00					***************************************		Darton	UN T	some c	1.60	
Dee	o Observ	ation Hole Nu	umber:	TP I	7-:lo				JOHR .		
Deep	W. 11-4-11-2	ation Hole Nu		**************************************	7-6					.4-	
Deep	Soil Horizon/	Soll Matrix; Color-Moist		Oximorphic Fea (mottles)			(Coarse I	SEN.		Soil	Oth
	Soil	Soll Matrix:		oximorphic Fea		Soli Texture (USDA)	(Coarse I	SEN	SIVOU		Othe
Depth (In:)	Soil Horizon/	Soli Matrix; Color-Moist (Munsell)	Redo	eximorphic Fea (mottles)	atures	Soil Texture (USDA)	Coarse I	SEA.	SIVOU	Soil Consistence	Othe
Depth	Soil Horizon/	Soll Matrix; Color-Moist	Redo	eximorphic Fea (mottles)	atures	Soli Texture (USDA)	Coarse I	Fragments Volume	SIVOU	Soil Consistence	Othe
Depth (In:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)	Redo	eximorphic Fea (mottles)	atures	Soil Texture (USDA)	Coarse I	Fragments Volume	SIVOU	Soil Consistence	Othe
Depth (In:)	Soil Horizon/	Soll Matrix: Color-Moist (Munsell)	Redo	eximorphic Fea (mottles)	atures	Soli Texture (USDA)	Coarse I	Fragments Volume Cobbles & Stones	SIVOU	Soil Consistence	Othe
Depth (In:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1042 312  WYR 414  Z-S41	Depth 2	Color	Percent	Soli Texture (USDA)  104K 312 104R 414 5AM	Coarse I	Fragments Volume Cobbles & Stones	Soil Structure	Soil Consistence (Moist)	Oth
Depth (In:)	Soll Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1047  312  W17  414  2.54  (a 3)	Depth 2	oximorphic Fer (mottles) Color	atures	Soll Texture (USDA)  104/4 312 194/2 194/2 414 5AM COANSE	Coarse I % by	Fragments Volume Cobbles & Stones	Soil Structure	Soil Consistence (Moist)	Othe
Depth (In:)	Soil Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1042 312  WYR 414  Z-S41	Depth 2	Color	Percent	Soll Texture (USDA)  LOYK 312  LOYK 312  LOYK 312  LOYK 312  LOYK 312  SAMO COANSE  SANO	Coarse I % by	Fragments Volume Cobbles & Stones	Soil Structure	Soil Consistence (Moist)	Oth
Depth (In:)	Soll Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1047 312  WYR 414  254  63  254  615	Depth 36	Color	Percent 715	Soll Texture (USDA)  104/4 312 194/2 194/2 414 5AM COANSE	Coarse I % by	Fragments Volume Cobbles & Stones	Soil Structure	Soil Consistence (Moist)	Othe
Depth (In:)	Soll Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1047  312  W17  414  2-54  6-13	Redo Depth	Color	Percent 715	Soll Texture (USDA)  LOYK 312  LOYK 312  LOYK 312  LOYK 312  LOYK 312  SAMO COANSE  SANO	Coarse I % by	Fragments Volume Cobbles & Stones	Soil Structure	Soil Consistence (Moist)	Othe
Depth (In:)	Soll Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1042 312  WAR 414  254  613  254  616	Redo Depth	Color	Percent 715	Soll Texture (USDA)  LOYK 312  LOYK 312  LOYK 312  LOYK 312  LOYK 312  SAMO COANSE  SANO	Coarse I % by	Fragments Volume Cobbles & Stones	Soil Structure	Soil Consistence (Moist)	Othe
Depth (In:)	Soll Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1042 312  WAR 414  254  613  254  616	Redo Depth	Color	Percent 715	Soll Texture (USDA)  LOYK 312  LOYK 312  LOYK 312  LOYK 312  LOYK 312  SAMO COANSE  SAMO COANSE	Coarse I % by	Fragments Volume Cobbles & Stones	Soil Structure	Soil Consistence (Moist)	Oth
Depth (In:)	Soll Horizon/ Layer	Soll Matrix: Color-Moist (Munsell)  1042 312  WAR 414  254  613  254  616	Redo Depth	Color	Percent 715	Soll Texture (USDA)  LOYK 312  LOYK 312  LOYK 312  LOYK 312  LOYK 312  SAMO COANSE  SAMO COANSE	Coarse I % by	Fragments Volume Cobbles & Stones	Soil Structure	Soil Consistence (Moist)	Othe

200 001249		n Hole I	Number: _	7 1 Da	2/15/20	Time	<del></del> -	Weather	5000	
1. Loc			15.			2				
				IUZ		, .				
,	_ocation (Identii	fy on Plan	)	47.7	CINC	<u> </u>	STYLE	2层不		
2. Lar	nd Use:	odland, agrice	ultural field, vacan	t lot, etc.)	— ∹ - <u>⊼</u> .	ي ج	Surface Stones	l library and	Slope (%)	
			4		Inadless				1000	
3. Dist			Body —	Drain		Possi	ble Wet Ares		dscape (allach sheel)	)
	Р	roperty Lir	feet ne	– Drinking W	feet Vater Well			1		
			(27)			2				
4. Pare	nt Material:	pro	glacim	_		Unsuitable	Materials Pre	esent: Yes	No 🗌	<b>:</b>
							The second second			
		35		Y						
5. Grou	ndwater Observ	ved: Yes	□ No ⓓ Ì		,					
5. Groui	ndwater Observ	ved: Yes	□ No @ ] Pit_34	_ Dept	th Standing Wa	ter in Hole_	1 -P -O			
5. Groui	ndwater Observ	ved: Yes	□ No @ ] Pit_34	_ Dept	th Standing Wa	ter in Hole_ 35E-A	ven			מינב)
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# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

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Additional Notes

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

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Stormwater Operation and Maintenance Manual

# Stamski And McNary, Inc. Engineering - Planning – Surveying 1000 Main Street; Acton, MA 01720 (978) 263-8585 www.stamskiandmcnary.com

## **Stormwater Operation and Maintenance Manual**

For

## Symes Development and Permitting, LLC

Homes at Hobbs Brook 443 Lincoln Street Lexington, MA 02421

February 20, 2018

## Responsible Party:

Applicant:

Symes Development and Permitting, LLC 60 Dodge Street Beverly, MA 01915

SM-5676

# **Table of Contents**

Long Term Operation and Maintenance Plan

Operation and Maintenance Sample Inspection Log

Long Term Operation and Maintenance Plan

## Schedule for Inspection and Maintenance:

## **Driveway Sweeping:**

It is recommended that the pavement shall be properly swept twice a year, with concentrations in the spring and the fall.

## Deep Sump Hooded Catch Basins and Drain Manholes:

During construction, catch basin grates shall be wrapped with filter fabric. Catch basins shall be cleaned upon the completion of construction. After construction, the deep sumps for all catch basins and drain manholes shall be inspected four times a year and cleaned four times a year. Sediment removed shall be disposed of in accordance with applicable local, state, and federal guidelines and regulations. The depth of the sediment in a basin shall not exceed a depth of 18 inches as determined by probing with a stick. If the stick hits the bottom within 30 inches of the water level, more than 18 inches of sediment has accumulated and must be removed. Licensed persons should remove and dispose of the contents of the sump in accordance with applicable regulations.

## **Roof Drywells:**

Inspect the system after every major storm (1" in 24 hours) for the first 3 months to ensure proper stabilization and function. Thereafter, inspect and clean it at least twice per year. Water levels should be recorded over several days to check the structures drainage. Also, mosquito controls may be necessary.

## Sediment Forebay: (Infiltration Basin 1)

The floor and sidewalls of the sediment forebay must be stabilized before use. Sediment forebays shall be inspected monthly and cleaned a minimum of four times per year and when sediment depth is between 3-6 inches. After sediment removal, any damaged vegetation must be replaced. Grass in the forebay shall not exceed 6 inches in length and any scouring and gullying shall be repaired as necessary.

## **Infiltration Basin:** (Infiltration Basin 1)

Preventative maintenance should be performed at least twice a year, and ideally sediment should be removed from the sediment forebay after every major storm event. Sediment shall be disposed of in accordance with applicable local, state, and federal guidelines and regulations.

Once online, the basin shall be inspected after every major storm event (1" in 24 hours), for the first 3 months. Thereafter, the basin should be inspected at least twice per year. Important items to check for include: differential settlement, cracking, erosion, leakage, or tree growth on the embankments, condition of riprap, sediment accumulation and the health of the turf.

At least twice a year, the buffer area and side slopes of the basin should be mowed. Grass clippings and accumulated organic matter should be removed to prevent the formation of an impervious organic mat. Trash and debris should also be removed at this time. Scarify bottom area and add additional sand if necessary.

Sediment should be removed from the basin as necessary. Removal procedures should not take place until the floor of the basin is thoroughly dry. Pretreatment devises associated with basins should be inspected and cleaned at least twice a year and ideally every other month.

## **Emergency Contacts:**

In the event of a hazardous materials spill on the site the following parties shall be contacted:

Fire Department: ph: 781-862-0272

## Records:

The Condominium Association shall maintain an inspection log of all elements of the storm water management plan. The Condominium Association shall maintain a maintenance log documenting the inspection and maintenance of the drainage structures. A copy of the erosion control and storm water maintenance plan and inspection logs shall be kept onsite at all times.

## Responsible Party:

The Condominium Association shall be responsible for the inspection and maintenance of the street sweeping, snow removal, catch basins, drainage manholes, infiltration basins, and drywells.

Budget: The estimated a	annual operation and maintenance budget is \$3,000.	
Illicit Discharges: THE	RE WILL BE NO ILLICIT DISCHARGES ON SITE.	
Name:		
Signature:		
Date:		

	8			
Operation a	nd Maintena	nce Sample I	nspection Log	

## **Homes at Hobbs Brook**

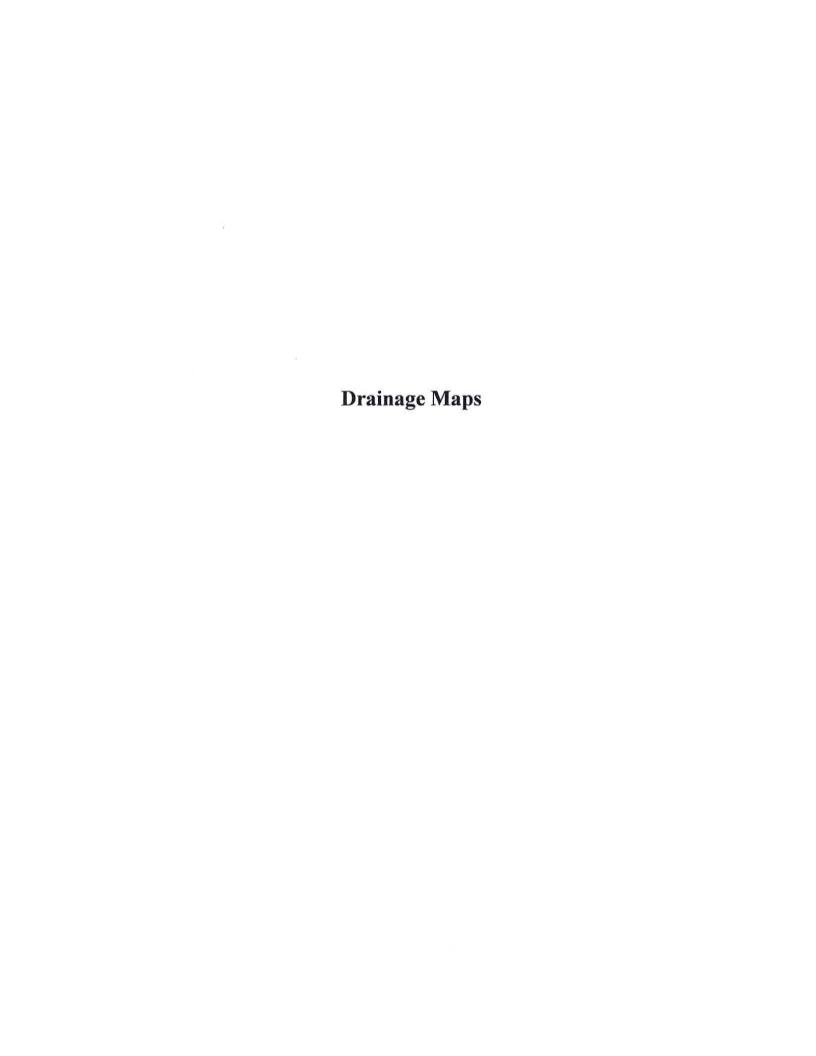
Operation and Maintenance Inspection Log

Year: \_\_\_\_\_

Inspection Items: Street Sweeping Catch Basins Drywells Sediment Forebay Infiltration Basin	Frequency: Two times per year Four times per year Once per year Monthly Monthly	
Street Sweeping:		
Previous Inspection Date: Inspection Date: Inspector Name: Comments:		
Action Required:		
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Previous Inspection Date: Inspection Date: Inspector Name: Sediment Depth: Comments:		(Remove if depth greater than 18")
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Catch Basin 2 (CB-2):		
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Inspector Name:	
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Erosion in Basin:	
Outlet Structure:	
Comments:	
Action Required:	







# TOWN OF LEXINGTON PLANNING OFFICE

1625 Massachusetts Avenue Lexington, Massachusetts 02420 Tel: 781-698-4560 www.lexingtonma.gov/planning Aaron Henry, Director David Kucharsky, Assistant Director David Fields, Planner

## AGENDA ITEM SUMMARY & STAFF RECOMMENDATION

**Item Name/Description:** 443 Lincoln Street Definitive Special Permit

**Application Date:** February 26, 2018

**Public Hearing Required** 

**Opening Date:** 

May 2, 2018 (65 days)

Proposed Meeting Date: April 26, 2018

### **Process to Date**

On February 21, 2017, Symes Development and Permitting, Inc., submitted a sketch balanced housing development plan for 443 Lincoln Street. This iteration of a balanced housing plan was discussed by the Planning Board on the evening of April 05, 2017. This submission was followed by a second sketch plan on October 25, 2017, which was discusses at the Planning Board November 15, 2017 meeting.

### **Submittal Standards**

The material submitted meets the criteria laid out for a definitive special permit plan in §176-6.4. The Planning Board (Board) will review the plan set, dated February 20, 2018, and respond to the applicant with comment, as they have done previously. The approval of this special permit will require a supermajority of the Board.

## Plan Set Review & Staff Comments

The submitted plan contains the necessary information for the Board to provide meaningful feedback to the applicant. The Board requested the following information during the first meeting in April, which was addressed by the applicant on the meeting of November 15<sup>th</sup> (see attached material provided by the applicant):

- The applicant must explain how useable the open space is;
- The applicant should be prepared to discuss the constraints of the land due to the utility easement on the property, if any;
- The parking plan for the balanced housing development proposal must be explained;
- The footprint of the abutting, recent development should be provided on the plan set;
- The applicant should get documentation from Cambridge identifying what they would allow for salting and snow storage, due to the proximity of the site to the Cambridge Reservoir;
- The applicant must explain if the two-foot deep retention basin is adequate, or if it needs to be modified;
- The applicant will be responsible for repaying the street if and when utilities are laid out and connected. A paying plan should be provided going forward; and
- An answer to the question of what the emission of the power lines, or voltage of the lines, is

currently.

#### **Submitted Plans**

Staff reviewed the plans submitted by the applicant. The applicant has previously addressed any staff concerns regarding Eversource's easement on the site. The sanitary sewer service provided in the proposed plans appears to have been altered from the previous proposal and will now offer sanitary grinders and pumps for each structure. Engineering Division staff had the following to offer in relation to the proposed sanitary sewer system:

- provide all pump calculations used for pump sizing.
- provide calculations confirming the addition of the proposed pump system will not affect the functionality of the existing pumping systems on the existing two in force main.
- We request that a comment be added to the plans that the entire proposed pumping system will be privately owned and maintained. This is to include proper signs placed on the pumping equipment along with emergency contact information in the event of pump failure.

Other comments from the Town's Engineering Division is provided under a separate cover.

Regarding the applicant's previous comment of providing documentation from Cambridge identifying what the City would allow for salting and snow storage, due to the proximity of the site to the Cambridge Reservoir, official documentation has yet to be provided; this is something the Board may wish to request from the applicant during this hearing (i.e., the attached letter received for a previous filing at 435-439 Lincoln Street can serve as a reference).

#### **Other Staff Comments**

After several iterations of this project staff believes that the current proposal is superior to the conventional subdivision that could otherwise be built at this site. If there are any lingering concerns of the Board as yet to be identified, these can be addressed by the applicant during the public hearing process. Staff recommends approving the proposed balanced housing residential development at 443 Lincoln Street. The reasoning for this is that the site is already developed and all land on site has been disturbed, potentially contaminated, or encumbered with utilities or buildings. Furthermore, this site has no direct abutters, but for Grey Oaks Circle, making any disruption that could occur during construction very minimal to the surrounding area. Furthermore, the positive increase in the diversity of housing stock within the town is preferable to the construction of four, large single family homes.

### Responses submitted regarding staff concerns prior to the 11/15/2017 meeting of the Planning Board

Plan Set Review & Staff Comments (Symes Responses – November 15, 2017)

• The applicant must explain how useable the open space is;

The Open Space will be available for passive recreation. The open meadow within the easement will be improved thru the control of invasive species vegetation, by removal of the gravel parking area and remnant debris piles. The existing open meadow is anticipated to be mowed on a semi-annual basis in order to control height of vegetation and invasive species regrowth.

• The applicant should be prepared to discuss the constraints of the land due to the utility easement on the property, if any;

There will be limitations to the height of vegetation. The actual construction of utilities lines will be coordinated with Eversource Energy to avoid impact on its equipment.

• The parking plan for the balanced housing development proposal must be explained;

Each Dwelling will have two spaces. Single car garages will have the second space in front of garage door. Dwellings with two-car garages satisfy parking requirements inside garage.

• The footprint of the abutting, recent development should be provided on the plan set;

A Neighborhood Overlay Plan has been provided which illustrates the As-built Oak Circle dwellings and their proposed approved landscaping feature.

• The applicant should get documentation from Cambridge identifying what they would allow for salting and snow storage, due to the proximity of the site to the Cambridge Reservoir;

The verbal instructions obtained from were to minimize deicing. The allowable mixture of salt and sand is 80% sand and 20% calcium chloride. Snow storage will be located along edge of driveway and to the west within open space.

• The applicant must explain if the two-foot deep retention basin is adequate, or if it needs to be modified:

The Infiltration Basin will be designed in accordance with applicable regulations. Final footprint and location may be subject to adjustment. If necessary, additional subsurface storage or a second basin to the west of Building A may also complement this basin.

• The applicant will be responsible for repaying the street if and when utilities are laid out and connected. A paying plan should be provided going forward; and

All necessary repaving in Lincoln Street will be completed by Applicant per current Town Standards.

• An answer to the question of what the emission of the power lines, or voltage of the lines, is currently.

There are two sets of three lines within the easement. The first set is offset greater than 52' from the edge of easement and the second set is offset greater than 175' from the edge of easement. Per the instructions of Eversource, our office surveyed the elevations of the wires along the site for review and approval. The Eversource letter is based on the review of available clearance to the wires from the proposed grades shown.

• Staff reviewed the plans submitted by the applicant. The applicant has addressed staff concerns regarding the utility easement on the site. The applicant should be asked to confirm the capacity of the connecting sewer main that will service the proposed site and address how the main will function (i.e., forced or gravity).

The low-pressure sewer main has already been extended down to this development with two stubs provided for the existing structures. We spoke early on with the vendor (F.R. Mahoney) for the low pressure sewer system regarding this development and are confident we can provide a suitable system. Similar to the abutting Grey Oaks Circle development, we propose a gravity sewer within the site to a pump chamber along the frontage. The pump chamber will connect to the low-pressure line within the right-of-way. Sewer collection system will be designed and installed per current Town of Lexington standards.



#### CITY OF CAMBRIDGE

#### MASSACHUSETTS

Water Department 250 Fresh Pond Parkway Cambridge, Mass. 02138 (617) 349-4770



January 8, 2016

Conservation Commission Town of Lexington 1625 Massachusetts Avenue Lexington, MA 02420

via email

Re: 435 and 439, Lincoln St., Lexington, MA

#### Dear Commissioners:

The Cambridge Water Department (CWD) appreciates the opportunity to submit comments on the proposed development at 435 and 439 Lincoln Street. Water from the site drains towards Hobbs Brook and the Hobbs Brook Reservoir, important surface waters within the City of Cambridge drinking water supply system. After reviewing the Notice of Intent and the Definitive Subdivision Plans dated November 20, 2015, CWD believes that the proposed stormwater management system will be sufficient to maintain water quality and quantity contingent on the following:

- The subsurface infiltration systems be equipped with a shut off valve to protect against potential spills.
- The Long-Term Pollution Prevention Plan and Order of Conditions are updated to:
  - Prohibit the use of sodium-based deicing agents (such as NaCl) on the roadway and limit the use of chloride-containing deicers.
    - Acceptable forms of deicing chemicals would include a mix of at least 80 percent sand and no more than 20 percent sodium-free deicing agent (such as MgCl) and/or Calcium Magnesium Acetate (CMA). Other low sodium and low chloride deicing options could be used if permission is granted by CWD.
  - Prohibit use of herbicides and pesticides in the common areas unless permission has been granted by CWD.
  - For fertilizer application, require compliance with all components of 330 CMR 31.00.
     Nitrogen fertilizer used in common areas must be slow-release.
- The Order of Conditions require:
  - The party responsible for the Operations and Maintenance (O&M) plan to regrade the
    private road if post-construction conditions reveal that stormwater is bypassing catch
    basins # 1 and # 2, thereby allowing stormwater to flow unmitigated to Lincoln Street and
    preventing the infiltration system from functioning as intended.

 The party responsible for the O&M Plan to submit an annual report to the Conservation Commission showing compliance with the schedule outlined in the Post-Construction Stormwater Maintenance Plan. CWD should be CCed on this communication.

CWD also notes that the project takes place within Zone A of an Outstanding Resource Water (ORW). As such, the Part C question 5 of the NOI should be updated accordingly. The project is also located within the Charles River Basin, which has a phosphorus TMDL, so Standard 4 of the Stormwater Report Checklist should be updated with the appropriate information.

Jan Ownell

Jamie O'Connell, Watershed Protection Supervisor City of Cambridge Water Department

(617) 349-4781

cc: David Kaplan, Watershed Manager, CWD Stephen S. Corda, Managing Director, CWD

Cambridge Water Board



#### **MEMORANDUM**

TO: Aaron Henry, Senior Planner

FROM: David Pavlik, Senior Civil Engineer

Michael Sprague, Senior Civil Engineer

DATE: March 20, 2018

SUBJECT: Homes at Hobbs Brook Definitive Special Permit Plan

CC: John Livsey, Town Engineer

The engineering division has reviewed the Definitive Special Permit Plans titled "Homes at Hobbs Brook" dated February 20, 2018. We submit the following;

#### Comment to Planning:

Please be aware that Lincoln St is still under moratorium until the beginning of the 2019paving season, on April 16, 2019.

#### Utilities:

#### Water

- Hydrants shall be American-Darling 5 ¼ inch B-84-B-5. Hydrant color; should conform to Lexington Fire Dept rules. We require this information be clearly noted on the plans.
- All hydrants, valves and valve boxes shall be American made only. Valves shall open **right** (**clockwise**), **hydrants shall open right** (**clockwise**). We require this information be clearly noted on the plans.
- All proposed vertical and horizontal bends for the proposed water main shall be on plans with adequate restraining glands, rods and thrust restraints.
- Please identify locations of any bends in the water main, bends will require restraints in accordance with town standards.
- An effort should be made to reduce the amount of clutter on plans so the proposed water services can be clearly identified. Will make addition comments after review of revised plans.

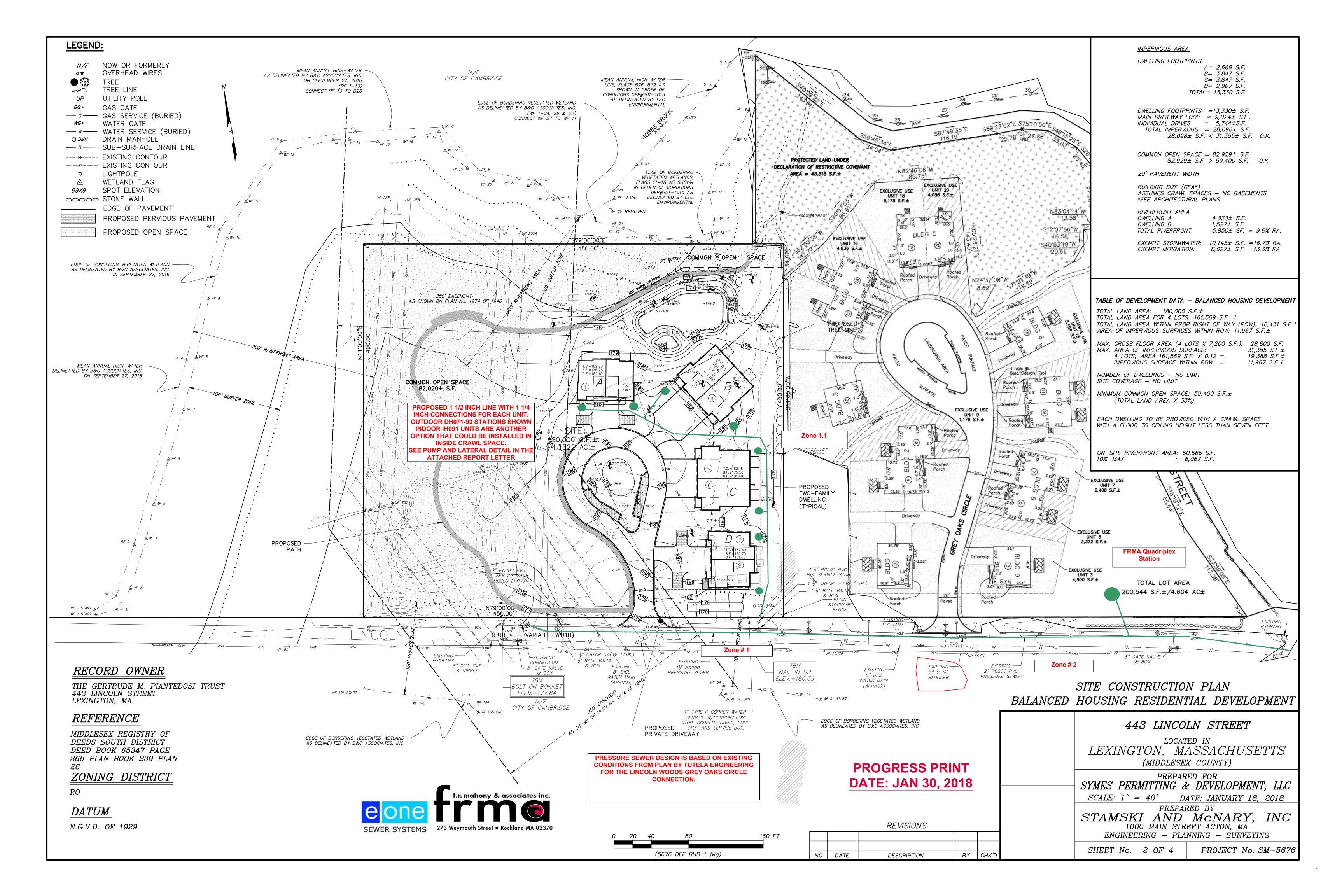
#### Sanitary Sewer

- Please provide all pump calculations used for pump sizing.
- Please provide calculations confirming the addition of the proposed pump system will not affect the functionality of the existing pumping systems on the existing two in force main.

- We request that a comment be added to the plans that the entire proposed pumping system will be privately owned and maintained. This is to include proper sings placed on the pumping equipment along with emergency contact information in the event of pump failure.
- Maintain separation of utilities in particular the drain and sewer mains.
- A minimum two course brick detail shall be shown on all sewer and drain manhole details.
- All manhole frame and covers should be consistent with Town of Lexington Standards.
- All sewer and drain pipes should conform to Town of Lexington Standards.

#### Drainage for roadway, sidewalk, driveway aprons, and site grading:

- The drainage analysis was complete and acceptable.
- Any trees that may be cut should be reviewed with the Tree Warden, Chris Filadoro at the DPW.
- Stormwater management report and Operation and Maintenance report is acceptable.
- Any stormwater BMP's that are to be used post construction, should not be used during construction unless they are cleaned properly to remove the higher sediment loadings found in construction runoff.





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# E/ONE Pressure System Design Report For 443 LINCOLN STREET

Lexington, MA February 2, 2018







info@frmahony.com www.frmahony.com

February 2, 2018

Richard J. Harrington, P.E. Stamski and McNary, Inc. 1000 Main Street Acton, MA 01720

RE: 443 Lincoln Street, Lexington, MA

Dear Richard;

This preliminary design analysis examines the use of the E/One Pressure Sewer System for your project. E/One has begun its fiftieth year of installation and O&M experience along with considerable research and development leading to continuous product and system improvements. E/One remains the worldwide industry standard and industry leader in the pressure sewer technology. The unique characteristics of the E/One Pressure Sewer approach provides not only a technical solution, but also an economic advantage to be realized with low up front and O&M costs.

#### **System Analysis**

This project proposes to collect wastewater from 8 single family residences from 4 duplex structures and discharge to the existing 1-1/2 inch PVC pressure sewer in Lincoln Street.

Using the information you provided and previous plans and reports for the Grey Oaks Circle abutting project, we ran the enclosed preliminary pressure sewer pipe sizing analysis. This was run through our Low Pressure Sewer Design Software that employs our Flow Velocity and Friction Head Loss vs. Pumps in Simultaneous Operation Spreadsheet. We have used the surface topography provided to make our analyses.

#### **Zone Layout**

Using your site plan we laid out a system of 4 flow zones leading to the final discharge point. We followed topography from your plan sheet 2 of 4 and matched to plans by Tutela Engineering Associates, Inc. for Sewer and Water Main Connection dated February 2001. The initial design report by FRMA had 3 flow zones terminating ay Weston Street at elevation 198. We have added Zone 1.1 common piping for your project to discharge to the former Zone # 1.

Computations are based on the Hazen-Williams formula for friction loss, using calculations of cross-sectional area and flow rate to determine pipe sizes that create



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"self-cleaning" velocities of 2.0 fps or higher. A "C" factor of 150, SDR 21 PVC pipe and the average expected daily volumes for single family homes are also used in this analysis.

The highest Total Dynamic Head generated is approximately 110 feet which comprised of static head and friction loss in the proposed pipeline. This is well below our pump's continuous-run rating of 185 ft, and well within its intermittent, i.e., normal, operating range. Flow velocity throughout the system meets or exceeds 2 fps. These characteristics and low retention time indicate that this will be a reliable, low-maintenance system.

#### **Design Flows & System Velocity**

We normally use average daily flows for system designs rather than the peak design flows commonly used for gravity sewer sizing. We do this because the system is sealed and void of inflow and infiltration commonly allowed for in gravity sewer designs. We size the system for an average daily flow of 200+/- gpd generally for single family homes. The pumps selected are rated to flows up to 700 gpd thus peak flows are easily handled. We size the pipelines for the proper scouring velocity based on the pump's output which has a consistent flow rate over a wide range of head conditions. We then look at the pipeline retention time to optimize the line size for the lowest retention that will pass wastewater in a short period of time to reduce sediment in the lines and prevent odor issues. This makes for a very reliable and maintenance free wastewater collection system.

Often we are asked to use the published "State" design values from various flow tables in order to secure approval. We can do this; but then we run the reports based on the actual predicted average flow to optimize the line size as mentioned above.

Many of our installations have seen flows that more closely mirror the EPA water use goals of 70 gpd/capita. We also look at seasonal uses a little more closely due to greater reductions in flow in the offseason. In applications of this type we look to find the best for both seasons.

#### **Appurtenances**

Cleanouts, Air/Vacuum Release

Our normal recommendations for valve placement are as follows: flushing connections at 1,000' to 1,500' intervals and at branch ends and junctions; isolation valves at branch junctions; and air release valves at peaks of 25 ft. or more and/or at intervals of 2,000 to 2,500 ft.

Flushing can also be accomplished with a portable flushing tool that can be used at each pump to flush the system. As the service left for this property is a 1-1/2 inch



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lateral line, we would suggest continuing that line size as the common header for each connection which would then be reduced to 1-1/4 inch.

Service Laterals and Check Valves

Common practice in pressure sewers requires the ability to isolate each lot with a corporation stop off the main and service lateral kit to the lot line. E/One now requires that each pump connection be isolated with a combination curb stop/redundant check valve.

E/One has developed a true wastewater rated check valve which is built in to our stainless steel lateral kit shown in this report. These components are rated to 235 psi and with standard connection fittings rated to 150 psi. These items are included in the budget analyses and shown in this report.

We strongly advise against the use of waterworks check valves as they are not rated for sewage environments. We do not like to recommend brass due to concerns for corrosion. **WEF Manual of Practice FD-12, Second Edition**, page 45 speaks to the limited success of brass or bronze alloys.

"Besides corrosion considerations, brass is subject to de-alloying, while some bronze, such as 85-5-5, will give better performance. The terms *brass* and *bronze* are used loosely, despite having different meanings; the engineer is advised to evaluate these materials with caution."

We have also seen PVC body check valves with pressure rating to 150 psi that do not have the same rating for back pressure on the check valve. This can result in damage to the check valve and pumping issues as the check valve disc can become dislodged under pressure and then become a line obstruction.

Corporation Stops/ Mainline Connections

Connections to the main pressure line do not require WYE type fittings. We commonly use a TEE or saddle connection. We isolate each connection to the main line with a stainless steel corporation valve in the same manner used for other utilities such as gas and water services.

We recommend that the service laterals connect to the mainline and do not need to enter the cleanout manhole as shown in the "discussion plan". You will find this easier to install and service without having to align and install fittings within the cleanout manhole.



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#### **Budget Notes**

We show both our outdoor Model DH071-93 pumps and indoor pump Model IH091-IDU in this report. We have used the Outdoor pump in the budget estimate. We can also provide pricing for our indoor pump model. We have note used the E/One Design Assistant Budget form as it would also include the existing pipe work as a default.

- Onsite pipe installation would likely be in the range of \$15.00 to \$20.00 per foot.
- Laterals \$299 each with added installation cost
- Corporations \$125.00 each with added installation cost
- DH071-93 pumps with Bal-Last \$4,900 each with added installation cost
- IH091 Optional Indoor \$3,900 plus plumbing and wiring cost.
  - o I generally include a 5% overhead and 15% contingency in my budgets

Costs of pipeline excavation and pump installation are best obtained from sources in your region. You may be better able to determine these costs.

I am looking forward to working with you on this and future projects. Please contact me if you have any questions or require additional information.

Best regards,

Henry 8. Albro

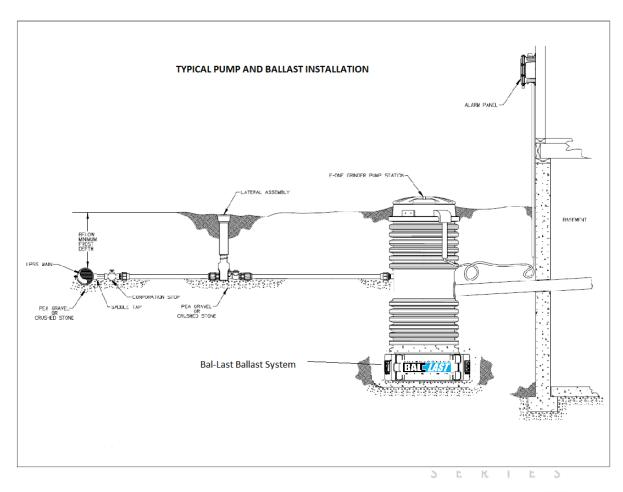
West Townsend Office
781-982-9300, Ext. 222
henryalbro@frmahony.com

SERIES

**Enclosures** 



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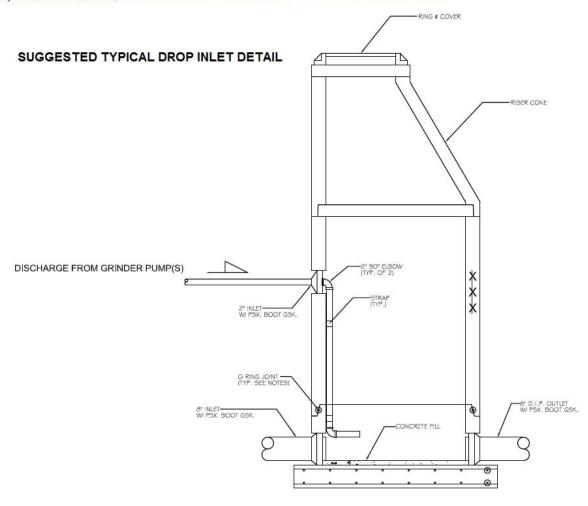


This image shows the typical layout of an outdoor pump unit for single-family home use. The pump unit is furnished complete, ready for installation. The installer needs to confirm the power cord length and discharge and inlet configuration. Standard products are supplied with 32 foot power supply cable. Standard inlets are 4-inch Schedule 40 Grommets (@ zero degrees) with 1-1/4 inch discharge (@ 180 degrees). Other configurations are available.





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IN-LINE MANHOLE
ELEVATION VIEW

This detail is shown as a concept sketch when major grade adjustments are required. We recommend that smaller inlet lines match the crown of outlet gravity sewer lines in all cases in order to direct flow to properly drain to the gravity sewer



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<u>Model IH091 Indoor Pump</u> Connection options for this station can be adapted to connect above the sill plumbing or below slab plumbing as seen in the sketches below.





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Standard alarm panels are the Sentry® panel mounted outside of the home as shown in the drawing (above).

Options include emergency generator connection (see photo) and Redundant alarm Remote Sentry® panel shown. Other panel configurations are available. See the partial listing of panel options below.



- Basic Panels include circuit breaker for the pump and separate breaker for the alarm. These panels include alarm light, alarm buzzer and alarm silence button. All F. R. Mahony panels are equipped with dry contacts to enable the connection of the Remote Sentry® (battery powered redundant alarm panel option)
- Standard options include auto transfer generator connection shown above.
   This panel provides automatic power transfer without having to open the alarm panel or having to operate any manual transfer switching. This feature can be added to the basic panel or the panels offered below.
- Popular options include the "Protection Package" which monitors and protects the system from:
  - Pump Run Dry Condition (Pump running out of water)
  - Pump Overpressure Condition (Closed valve)<sup>S</sup>
  - o Brownout Condition (Main voltage under 12% of nameplate)
  - High Liquid Level
- The "Protect Plus" panel features offer the same items in the "Protection Package" plus the following:
  - High & Low Amperage draw by the pump
  - o High & Low voltage to the pump
  - Extended Runtime by the pump (indicating wear or excessive flow) (field adjustable settings)
  - Monitoring of:
    - Real-time Pump Voltage and Current
    - Cycles & Hours (can be reset)
    - Minimum & Maximum Amperage (can be reset)
    - Minimum, Maximum, Average, and Last Run Cycle (in minutes, can be reset)



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#### **Emergency Generator Transfer Options.**

The indoor pump units may be furnished with a receptacle for connection of emergency power supplies. The image to the right shows the connection receptacle on the right side of our Sentry panels. This connection may be connected by your electrician to a remote connection port outside of the home.



Wiring must be performed by a licensed electrician and conforming to NEC and local electrical codes.

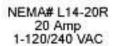
The box (left) is shown in the face view (face up) and is intended to be mounted on the outside wall to permit connection of a portable generator to the receptacle on the bottom. Generator operation must always be in well ventilated areas outside of any living space.

The pump may be operated under emergency power provided the automatic transfer option is selected with the Sentry® panel. Normal pump run times are short and should not require the continuous connection of a generator. A single portable generator may be used to

service several homes effectively.











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Pump models may be the DH071-93 (standard height) for outdoor use or the Model IH091 indoor unit. Both products are UL listed NSF and CSA certified and Massachusetts Plumbing Board Accepted.

#### Model DH071-93 Outdoor Pump With Bal-Last<sup>TM</sup>

The outdoor model is complete - ready for installation and connection to exterior plumbing and power supply. This unit is fully tested for operation and factory leak tested. No assembly is required and there are no floats to adjust. The pump is furnished complete with the alarm panel and direct bury power supply cable. Standard cable length is 32 feet with 50, 75, and 100 and up to 150 foot cables available. (See Alarm Panel options above)



Other station configurations are available for higher flow requirements. Please contact us for more information. Additional information may be found at <a href="https://www.eone.com">www.eone.com</a>

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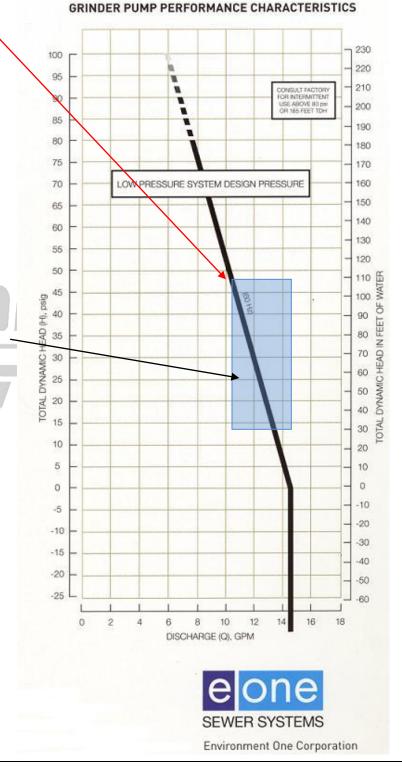
#### **Operation Conditions**

111 Feet is the highest TDH at simultaneous operating conditions with the expected number of pumps operating in each zone, or the head of an individual pump operating in a single zone condition.

Operating range of E/One pumps from 0-185 feet TDH and from 0 to -60 feet TDH.

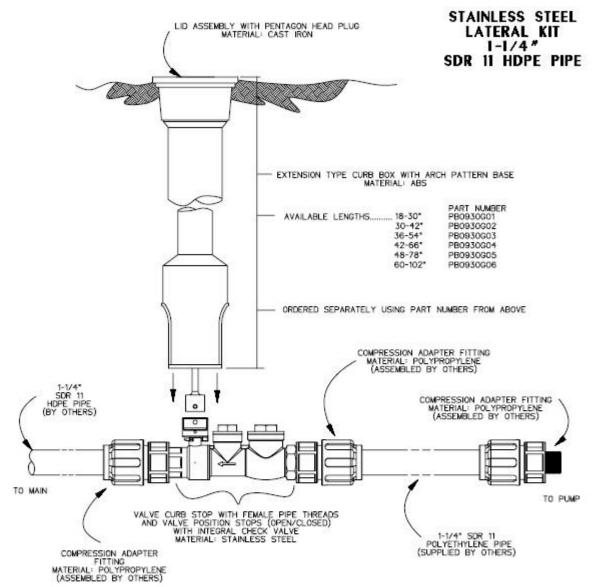
Your System Range

Anti-siphon valves in E/One cores provide for negative head pumping. In common systems with negative heads of 25-30 feet or more we recommend the use of combination air/vacuum release valves as described below.





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#### NOTES:

- SS CURB STOP/CHECK VALVE AND FITTINGS ARE PROVIDED SEPARATELY, TO BE ASSEMBLED BY OTHERS
- TO ASSEMBLE, APPLY A DOUBLE LAYER OF TEFLON TAPE, AND A LAYER OF PIPE DOPE (SUPPLIED BY OTHERS) TO THE THREADS ON THE PLASTIC FITTINGS AND INSTALL PER THE MANUFACTURER'S INSTRUCTIONS
- 3. ASSEMBLY IS TO BE PRESSURE TESTED (BY OTHERS)
- 4. ASSEMBLY IS TO BE USED WITH SDR11 HDPE PIPE
- 5. TO ORDER SS LATERAL KIT, USE PART NUMBER NC0193G01
- 6. CURB BOX IS TO BE ORDERED SEPARATELY, SEE ABOVE

#### KIT PARTS ARE NOT ASSEMBLED

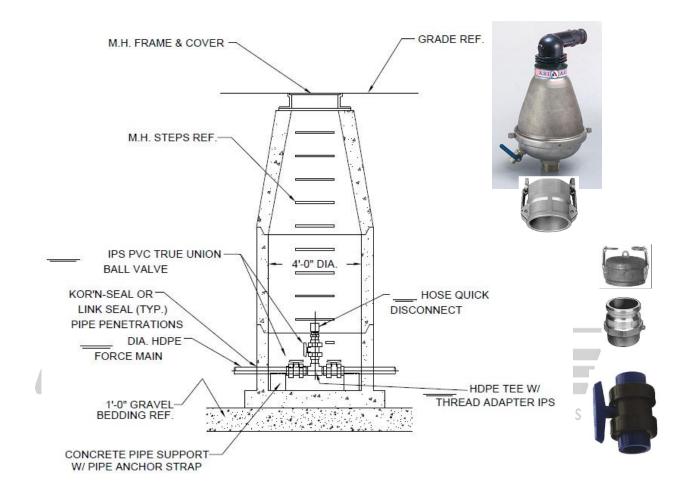
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# Typical Cleanout Detail (Optional Air/Vacuum Valve shown –right)



Cleanout detail can be modified to match typical installation needs. Inline shut offs may be added to isolate flow direction. Image shown is flow through cleanout. These structures can be terminal end of line cleanouts, or junction cleanouts as may be required. Optional air and vacuum relief valves may be added when required.



## **Environment One Corporation**

# Pressure Sewer Preliminary Cost and Design Analysis For 443 Lincoln Street Extension Lexington, MA

**Prepared For:** 

Acton

Stamski and McNary

1000 Main Street

MA 01720 USA

Tel: (978) 263-8585 ext. 211

Fax: rjh @ stamskiand mcnary.com

Prepared By: frma/eq/ Henry Albro REV

**February 1, 2018** 

# 443 Lincoln Street Extension Lexington, MA

**Prepared by :** frma/eq/ Henry Albro REV **On:** February 1, 2018

Notes:

This report looks at adding 8 Pumps to existing zone # 1 with 1-1/2 inch PVC Pipe.

#### PRELIMINARY PRESSURE SEWER - PIPE SIZING AND BRANCH ANALYSIS

443 Lincoln Street Extension

Prepared By: frma/eq/ Henry Albro REV February 1, 2018 Lexington, MA

Zone	Connects	Number	Accum	Gals/day	Max Flow	Max	Max Flow	Pipe Size	Max	Length of Main	Friction Loss	Friction	Accum Fric	Max Main	Minimum Pump	Static Head	Total
Number	to Zone				Per Pump	Sim Ops	(GPM)	(inches)	Velocity	this Zone	Factor	Loss This	Loss (feet)	Elevation	Elevation	(feet)	Dynamic
		in Zone	in Zone		(gpm)				(FPS)		(ft/100 ft)	Zone					Head (ft)
This spread	This spreadsheet was calculated using pipe diameters for: SDR21PVC Friction loss calculations were based on a Constant for inside roughness "C" of: 150																
1.00	2.00	2	10	200	10.89	4	43.56	1.50	5.64	450.00	6.77	30.45	69.56	198.00	176.00	22.00	91.56
1.10	1.00	8	8	200	10.03	3	30.09	1.50	4.16	475.00	3.85	18.28	87.84	198.00	175.00	23.00	110.84
2.00	3.00	3	13	200	12.25	4	48.99	2.00	3.78	1,250.00	2.49	31.11	39.11	198.00	176.00	22.00	61.11
3.00	3.00	2	15	200	13.72	4	44.34	2.00	3.92	300.00	2.67	8.00	8.00	198.00	178.00	20.00	28.00

#### PRELIMINARY PRESSURE SEWER - ACCUMULATED RETENTION TIME (HR)

443 Lincoln Street Extension Lexington, MA

February 1, 2018

Prepared By: frma/eq/ Henry Albro REV

Page 1

Zone Number	Connects to Zone	Accumulated Total of Pumps this Zone	Pipe Size (inches)	Gallons per 100 lineal feet	Length of Zone	Capacity of Zone	Average Daily Flow	Average Fluid Changes per Day	Average Retention Time (Hr)	Accumulated Retention Time (Hr)	
This spreadsheet was calculated using pipe diameters for: SDR21PVC  Gals per Day per Dwelling											
1.00	2.00	10	1.50	12.07	450.00	54.32	2,000	36.82	0.65	3.28	
1.10	1.00	8	1.50	12.07	475.00	57.33	1,600	27.91	0.86	4.14	
2.00	3.00	13	2.00	18.84	1,250.00	235.53	2,600	11.04	2.17	2.63	
3.00	3.00	15	2.00	18.84	300.00	56.53	3,000	53.07	0.45	0.45	

#### STAMSKI AND MCNARY, INC.

1000 Main Street Acton, Massachusetts 01720 (978) 263-8585 FAX (978) 263-9883

JOSEPH MARCH, P.E., P.L.S. GEORGE DIMAKARAKOS, P.E.

May 15, 2018

Lexington Planning Board 201 Bedford Street Rm 202 Lexington, MA 02420

Re:

Homes at Hobbs Brook 443 Lincoln Street

Members of the Board,

On behalf of our client, Symes Permitting and Development LLC, our office has revised the Definitive Balanced Housing Development Plan Set dated May 15, 2018. The plan revisions are in response to both the written review comments received to date and the verbal review comments received during the public hearing.

#### A summary of the Plan revisions are as follows:

- All of the Engineering comments have been addressed as detailed below.
- The Planting List is now all native plants on the Landscape Plan.
- A letter from the Cambridge Water Department has been requested.
- The Notice of Intent application has been filed with Conservation.
- A neighborhood land use timeline has been prepared for NOI (see attached).
- Only select plan sheets 4, 5, 6, 7, 9 & 10 have been updated.

#### Responses to Engineering Division Memorandum from David Pavlik dated March 20, 2018

#### Water

- The fire hydrant detail has been modified to call for use of American-Darling 5 ¼ inch B-84-B-5 to be painted per town requirements (sheet 10).
- General Note 4 has been modified to specify that all hydrants, valves, and valve boxes shall be American made only (sheet 9).
- Bends in the proposed water main have been identified (sheet 6) and thrust block specifications are provided per detail (sheet 10). The proposed water main has been relocated under the proposed access drive (sheet 6).
- A larger, 1"=20' scale, utility detail has been provided (sheet 6).

#### Sewer

- Sewer details and inverts updated (sheet 10). Also see F.R. Mahony report.
- See F.R. Mahony report relative to existing line and services.
- General Note 18 has been added to specify that the proposed sewer system will be privately owned and maintained and a sign with contact information will be placed on each pumping unit (Sheet 9).
- The proposed pressure sewer has been reconfigured. The pressure sewer line is now located behind Buildings A&B. The total number of E/One units has been reduced from 8 to 4. The proposed E/One units are now type DH152. Overall utility layout has been adjusted to provide separation.
- Two course bricks are now shown and specified in the drain manhole detail (Sheet 9).
- General Note 21 has been added to specify all manhole frame and covers to meet Town of Lexington Standards (Sheet 9).
- General Notes 19 and 20 have been added to specify all sewer and drain pipes shall meet Town of Lexington Standards (Sheet 9).

#### Drainage for roadway, sidewalk, driveway aprons, and site grading

• Stormwater details relative to catch basins, drain manhole, area drain and level spreader have labels which have been edited per engineering comments (sheet 10).

#### Electric

• Services will now be provided overhead across Lincoln Street to an onsite utility pole where it will then proceed underground to dwelling units similar to Grey Oaks Circle.

#### Response to Agenda Item Summary a & Staff Recommendations from Planning Office

#### **Submitted Plans**

• The BHD Application and Notice of Intent have been submitted to the Cambridge Water Department and a letter from them has been requested.

Thank you for your attention to this mater. We look forward to further discussing this project at the next Planning Board hearing. Please contract our office if there are questions.

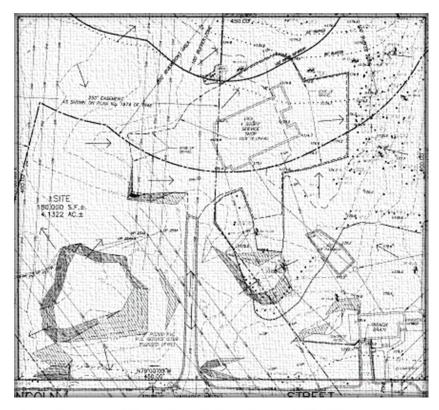
Respectfully,

Stamski and McNary, Inc.

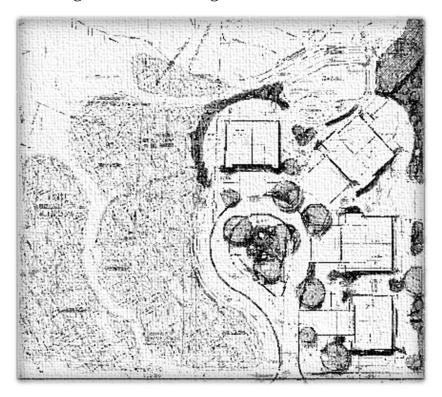
Paul Kirchner, E.I.T.

Richard J. Harrington, P.E.

# The Homes at Hobbs Brook



Existing Land Use with Higher Potential Pollutant Load



Future residential use similar to abutting Grey Oaks Circle



# 2005 – AERIAL VIEW

#### BACK IN THE DAY

Substantial alteration of onsite area

Active onsite auto shop & abutting shop

Higher onsite land use operations

Multiple onsite material storage areas and debris stock piles

Greater auto storage activity on gravel driveways and parking lots

Additional dirt and gravel access driveways

Multiple driveways and dwellings opposite reservoir on both sites



# 2016 – AERIAL VIEW

#### THE OLD NEIGHBORHOOD

Onsite land use operations reduced from 2005

One onsite auto service shop & one abutting shop

Land use operations reduced within onsite riverfront area

Remnant material areas and stock piles remain

Reduced auto storage on gravel driveways and parking lots

Minor overgrowth of abandoned dirt and gravel paths within easement



2017 – AERIAL VIEW

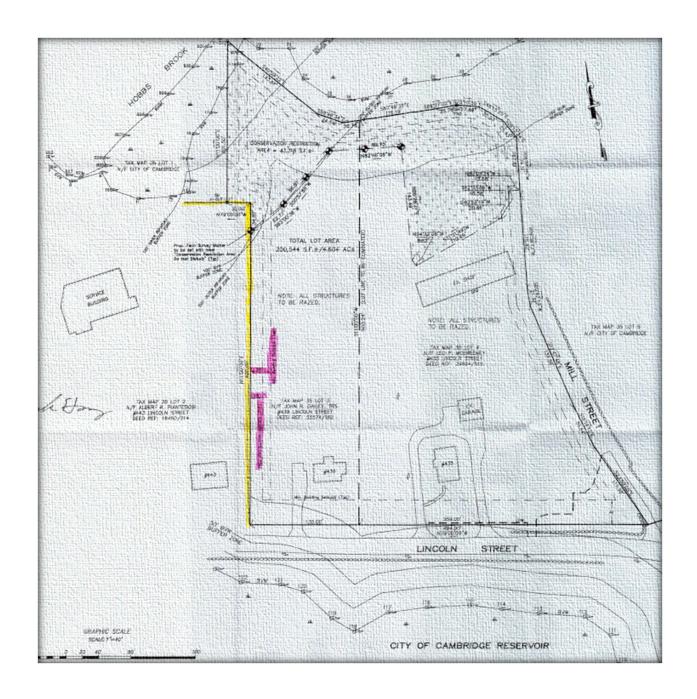
#### BEGINNING OF A NEW NEIGHBORHOOD

Little onsite change from 2016 aerial view

Active on-site auto repair shop remains

Abutting Balanced Housing Development - Grey Oaks Circle under construction

Applicant submits Sketch Plan for on-site Balanced Housing Development



# 2016 - PLAN VIEW

#### THE OLD NEIGHBORHOOD

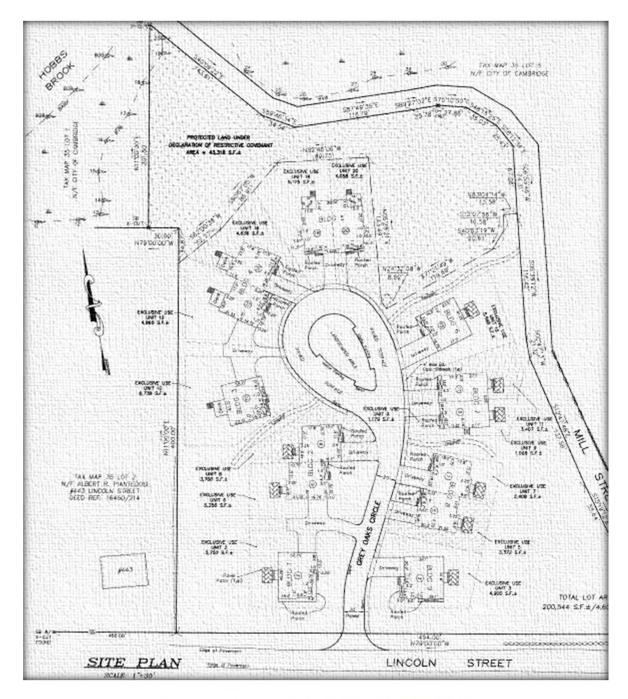
Two shops

Three residential dwellings

Six individual paved curb-cuts

Acres of unprotected open space

Lack of stormwater management controls



# 2017 - PLAN VIEW

#### BEGINNING OF A NEW NEIGHBORHOOD

Abutting Grey Oaks Circle Complete

Removal of the abutting service shop and two dwellings

Abutting balanced housing development with common areas

Abutting Mill Street walking path



# 2018 - FOCUS

#### IMPROVEMENT FOR THE FUTURE

Remove remaining auto repair shop and one dwelling

Revegetate inner riparian zone

Redevelop riverfront area

Eliminate on-site private sewage disposal system

Protect common areas

Provide additional walking paths

Connect vista view to abutting Mill Street path



# 2020 - VISION

#### A COMPLETE AMD IMPROVED NEIGHBORHOOD

Two balanced housing developments

One neighborhood

Protected common areas

Walking trails

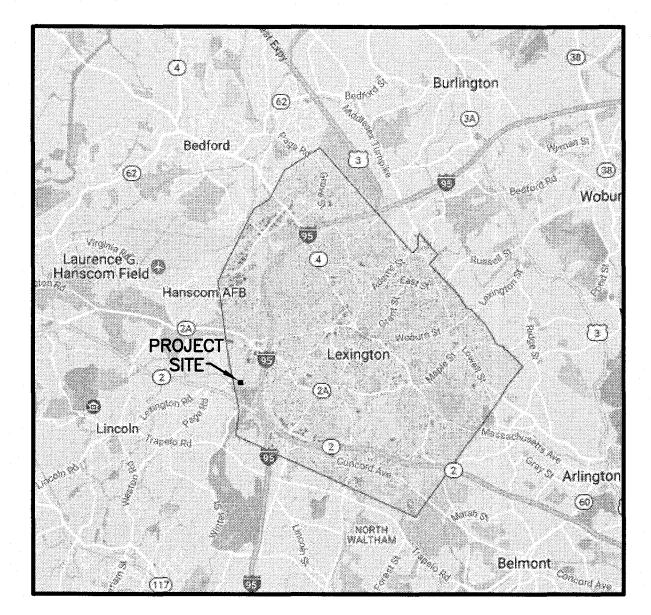
Stormwater management controls

Prohibition on any further development

# HOMES AT HOBBS BROOK

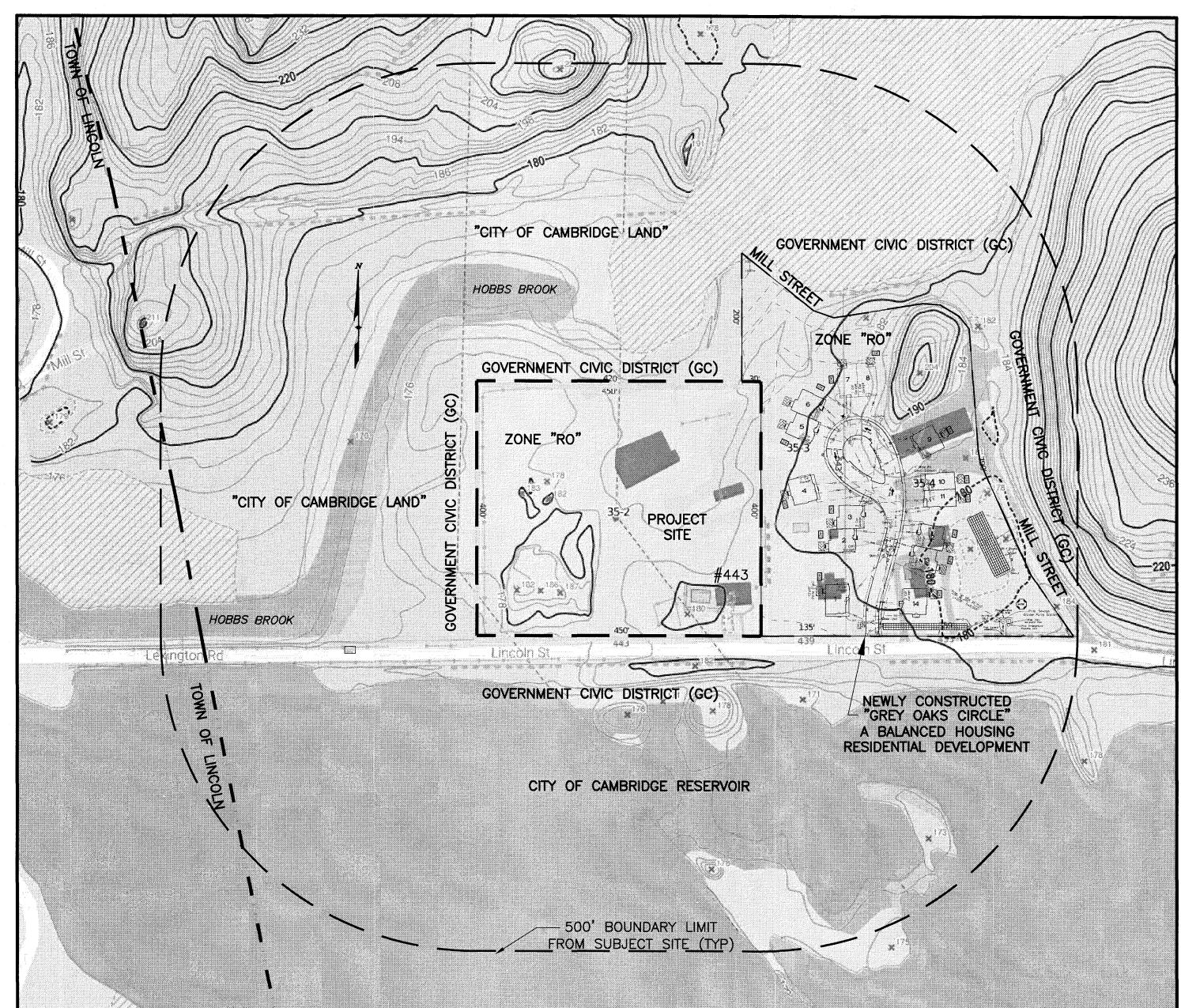
# DEFINITIVE PLAN BALANCED HOUSING RESIDENTIAL DEVELOPMENT 443 LINCOLN STREET LEXINGTON, MASSACHUSETTS

FEBRUARY 20, 2018 REVISED: MAY 15, 2018



TOWN LOCUS

SCALE: 1"=10,000"



# SHEET INDEX

SHEET 1 TITLE SHEET

SHEET 2 SITE ANALYSIS MAP

SHEET 3 PROPERTY RIGHTS PLAN OF LAND

SHEET 4 SITE CONSTRUCTION PLAN

SHEET 5 PLAN AND PROFILE

SHEET 6 UTILITY PLAN

SHEET 7 LANDSCAPE PLAN

SHEET 8 CONVENTIONAL SUBDIVISION PROOF PLAN

SHEET 9-10 CONSTRUCTION DETAILS

SHEET 11 EROSION AND SEDIMENT CONSTROL PLAN

# LOCUS MAP SCALE: 1"=120"

# **APPLICANT**

SYMES DEVELOPMENT & PERMITTING, LLC 50 DODGE STREET BEVERLY, MA 01915

# LANDSCAPE ARCHITECT

JAMES EMMANUEL, ASSOCIATES 22 CARLTON ROAD MARBLEHEAD, MA 01945

# JOSEPH SURVEYOR/ENGINEER

STAMSKI AND MCNARY, INC 1000 MAIN STREET ACTON, MA 01720

# **ATTORNEY**

LATHAM LAW OFFICES, LLC 643 MAIN STREET READING, MA 01867-3096

# RECORD OWNER

THE GERTRUDE M. PIANTEDOSI TRUST 443 LINCOLN STREET LEXINGTON, MA

# REFERENCE

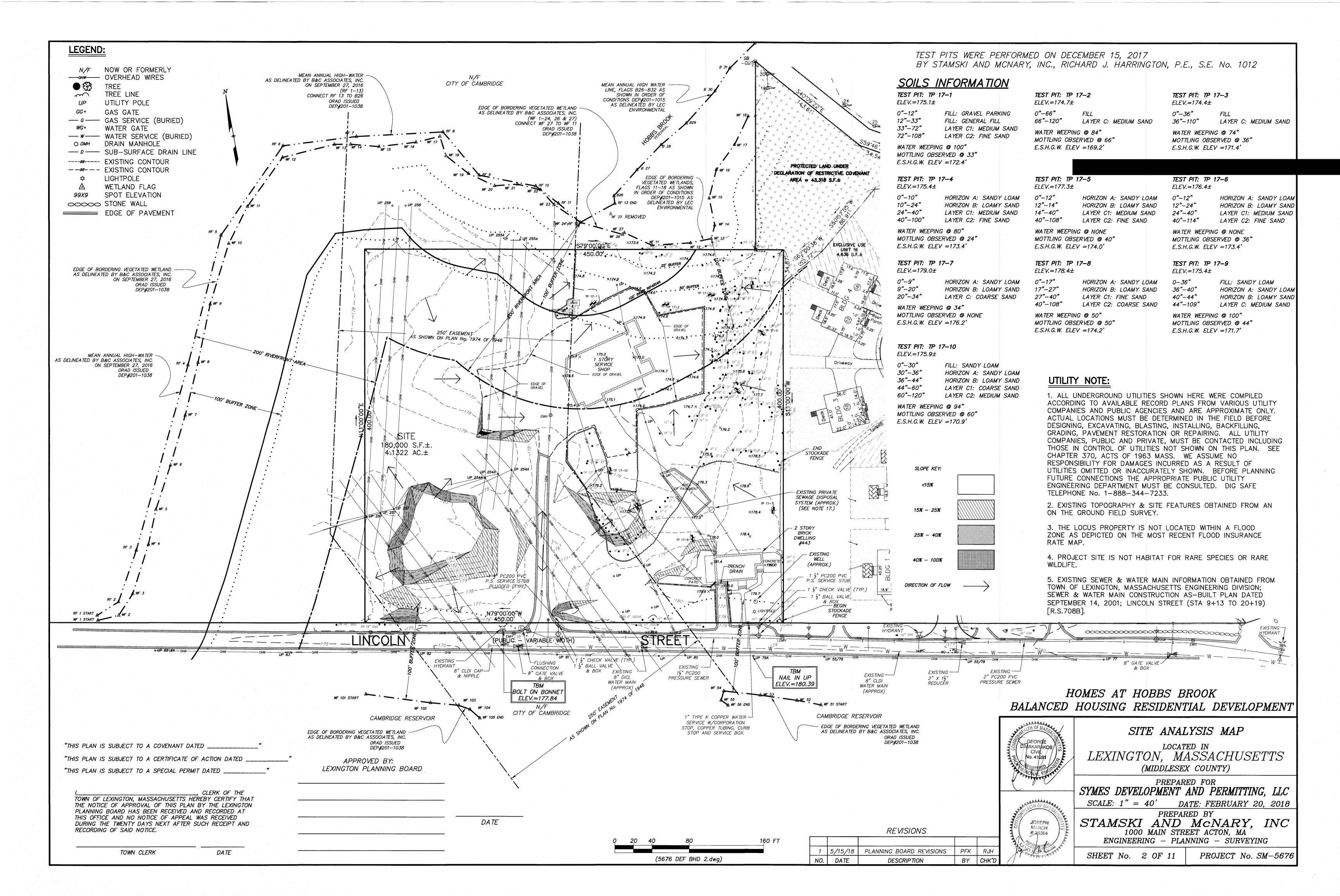
MIDDLESEX REGISTRY OF DEEDS SOUTH DISTRICT DEED BOOK 65347 PAGE 366 PLAN BOOK 239 PLAN 26 ASSESSOR'S MAP 35 PARCEL 2

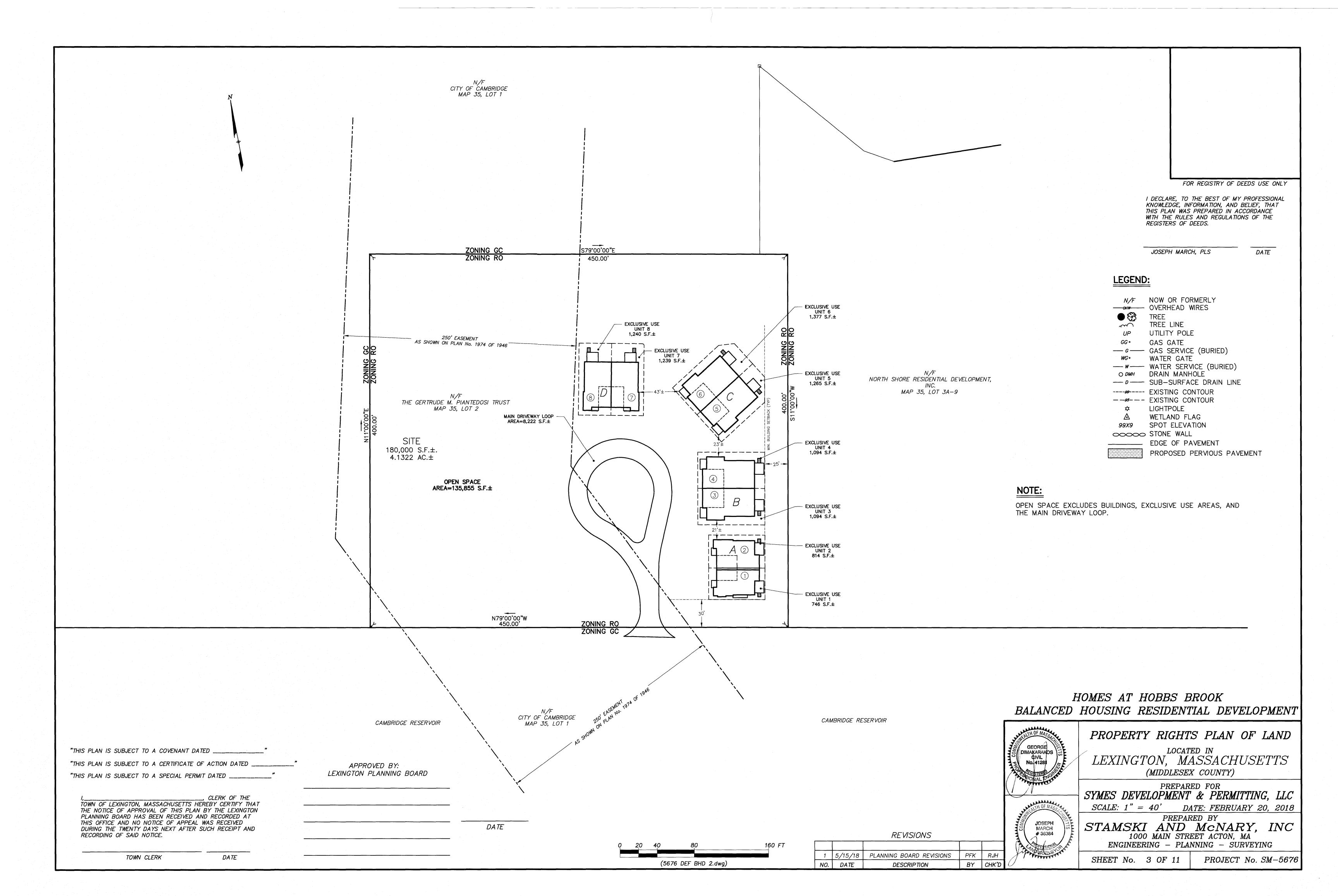
# **ZONING DISTRICT**

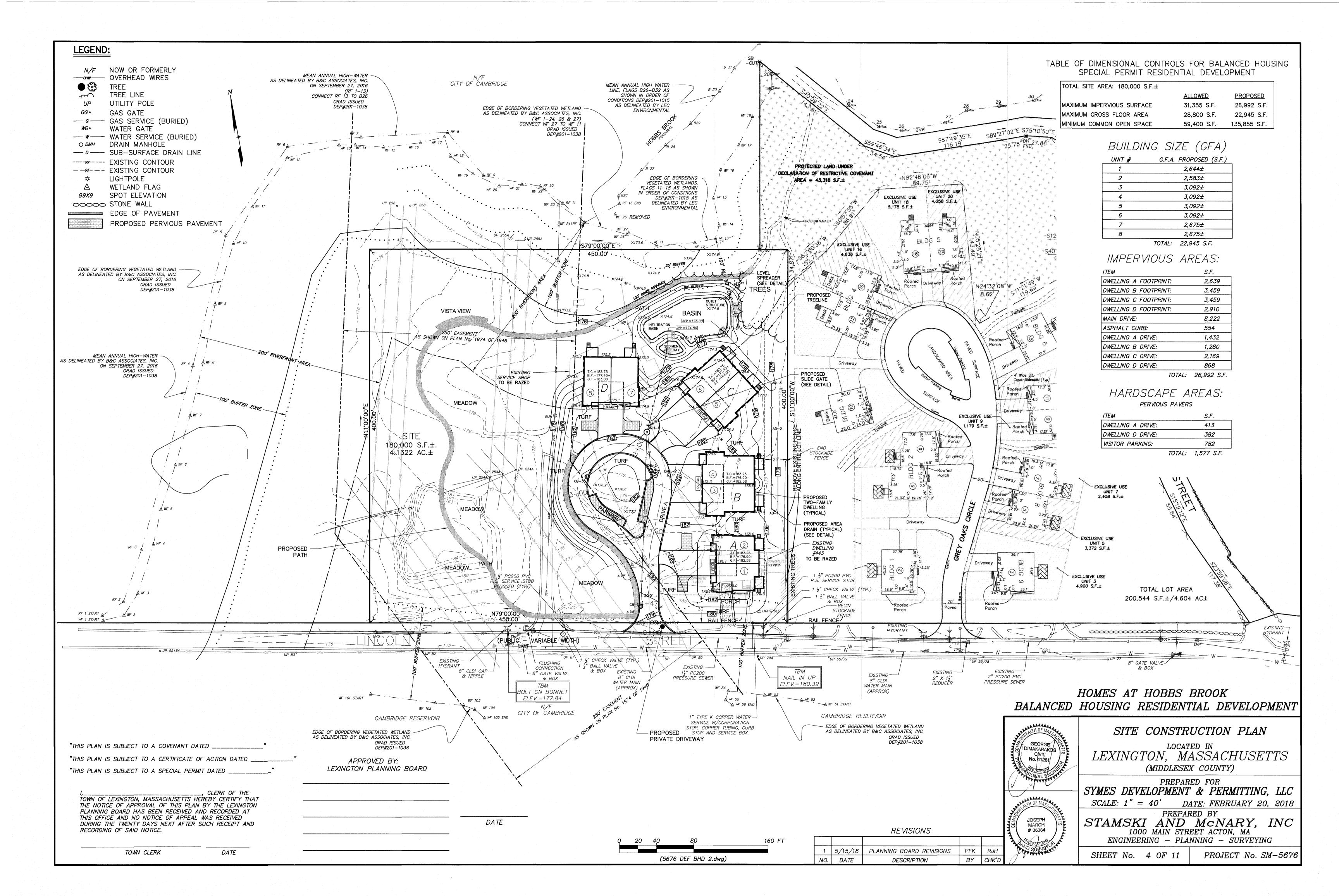
)

# DATUM

N.G.V.D. OF 1929







#### AVERAGE EXISTING GRADE CALCULATION / BUILDING HEIGHT AVERAGE HIGHEST BUILDING EXISTING GRADE ELEVATIONS AT BUILDING CORNERS EXISTING RIDGE HEIGHT UNIT GRADE 181.4 179.9 179.7 179.6 180.15 217.43 37.28 181.4 179.9 178.4 178.2 179.48 217.43 37.96 176.3 178.6 177.0 177.58 178.4 213.60 36.03 176.3 178.6 177.33 178.5 175.9 213.60 36.28 174.7 175.6 174.2 176.05 177.7 214.10 38.05 174.7 175.6 174.3 174.6 174.80 214.10 39.30 175.1 175.2 174.9 175.08 175.1 214.68 39.61 175.1 175.2 175.4 175.4 175.28 214.68 39.41

UNIT	FFE	T.C.	G.F.	B.F.		
1	184.33	183.25	182.58	176.90*		
2	184.33	183.25	182.58	176.90*		
3	184.33	183.25	182.58	176.90*		
4	184.33	183.25	182.58	176.90*		
5	184.83	183.75	183.08	177.40*		
6	184.83	183.75	183.08	177.40*		
7	184.83	183.75	183.08	177.40*		
8	184.83	183.75	183.08	177.40*		
1	* CRAWL SPACE - MAX HEIGHT = 6'-8"**  ** MEASURED FROM BOTTOM JOIST TO BASEMENT FLOOR					

SITE CONSTRUCTION PLAN

"THIS PLAN IS SUBJECT TO A COVENANT DATED \_\_\_\_\_\_"

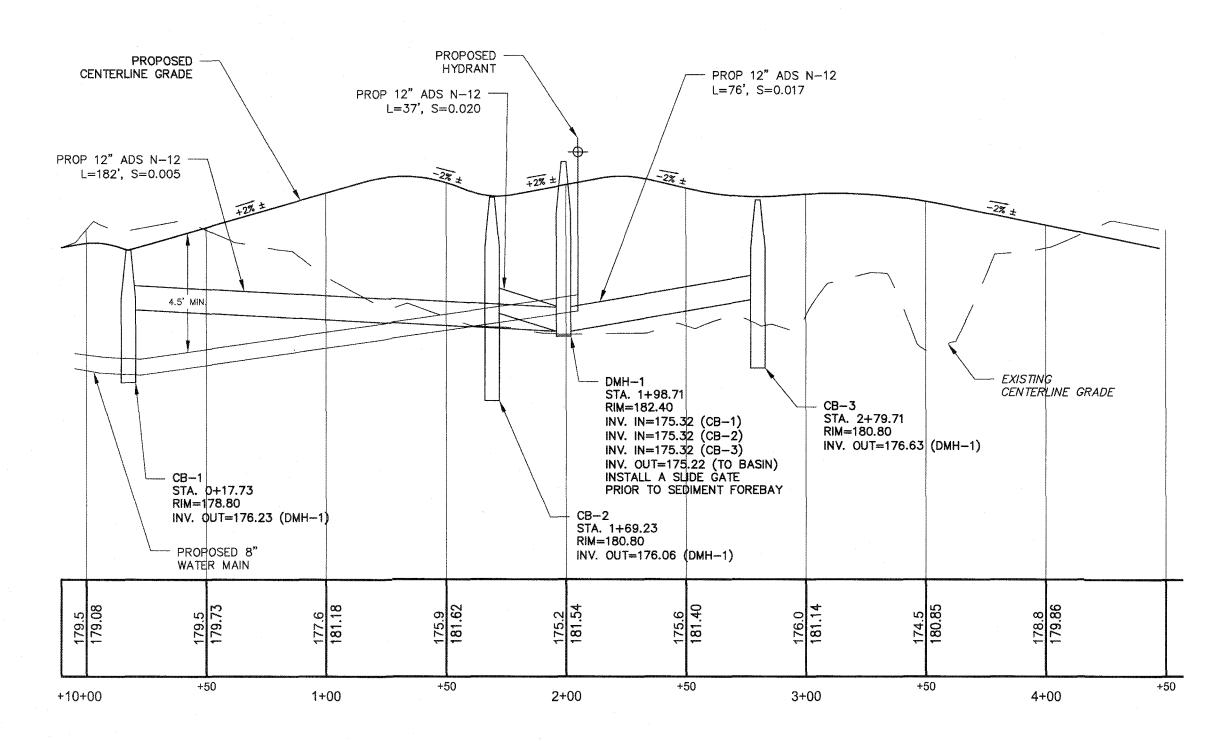
"THIS PLAN IS SUBJECT TO A CERTIFICATE OF ACTION DATED \_\_\_\_\_"

"THIS PLAN IS SUBJECT TO A SPECIAL PERMIT DATED \_\_\_\_\_"

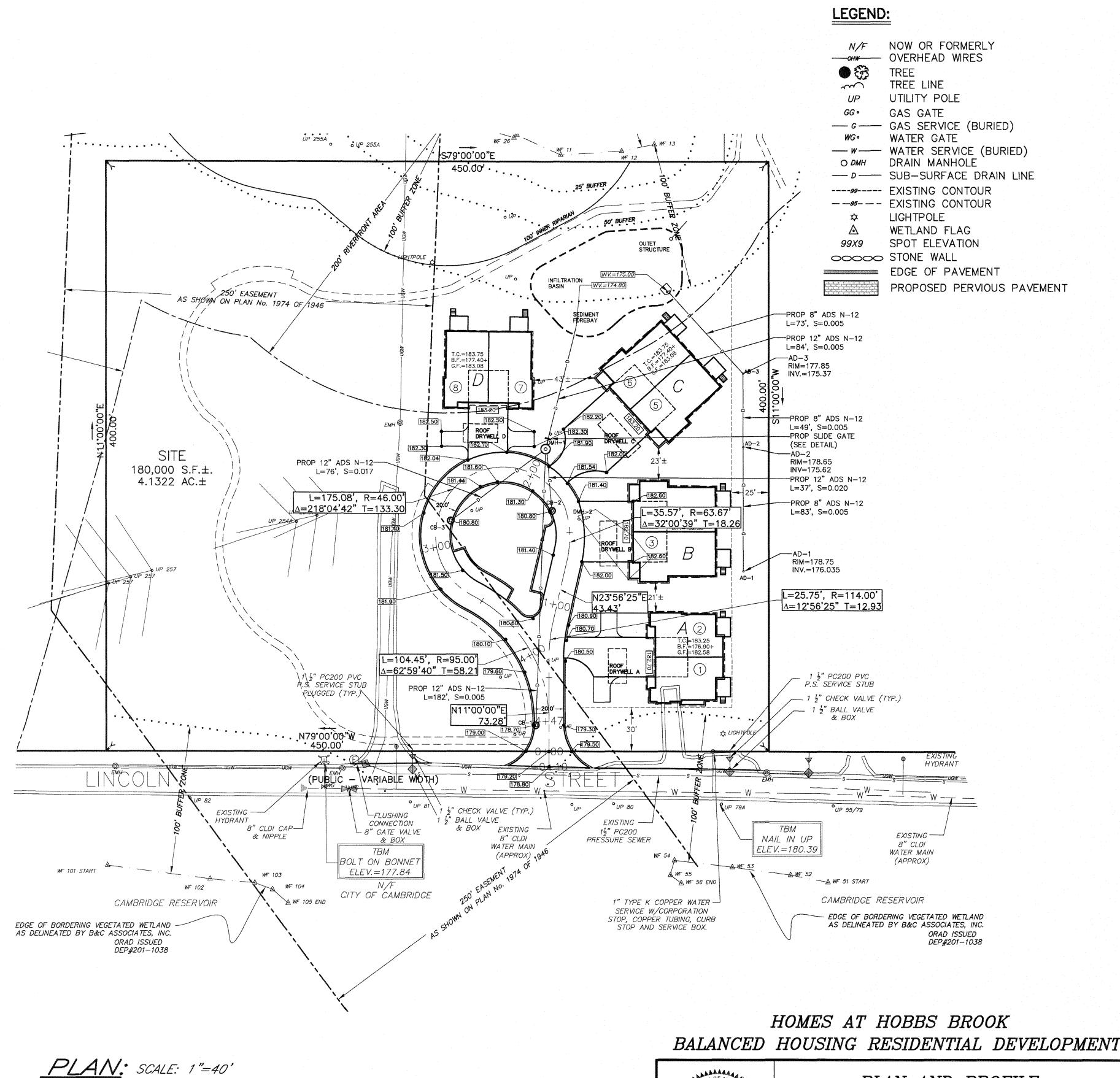
LEXINGTON PLANNING BOARD

I, \_\_\_\_, CLERK OF THE
TOWN OF LEXINGTON, MASSACHUSETTS HEREBY CERTIFY THAT
THE NOTICE OF APPROVAL OF THIS PLAN BY THE LEXINGTON
PLANNING BOARD HAS BEEN RECEIVED AND RECORDED AT
THIS OFFICE AND NO NOTICE OF APPEAL WAS RECEIVED
DURING THE TWENTY DAYS NEXT AFTER SUCH RECEIPT AND
RECORDING OF SAID NOTICE.

TOWN CLERK DATE



PROFILE: SCALE: 1"= 40' H.



REVISIONS

PLANNING BOARD REVISIONS

DESCRIPTION

PFK |

BY

1 5/15/18

NO. DATE

PLAN AND PROFILE

LEXINGTON, MASSACHUSETTS

(MIDDLESEX COUNTY)

PREPARED FOR

SYMES DEVELOPMENT & PERMITTING, LLC

SCALE: 1" = 40' DATE: FEBRUARY 20, 2018

PREPARED BY

STAMSKI AND McNARY, INC

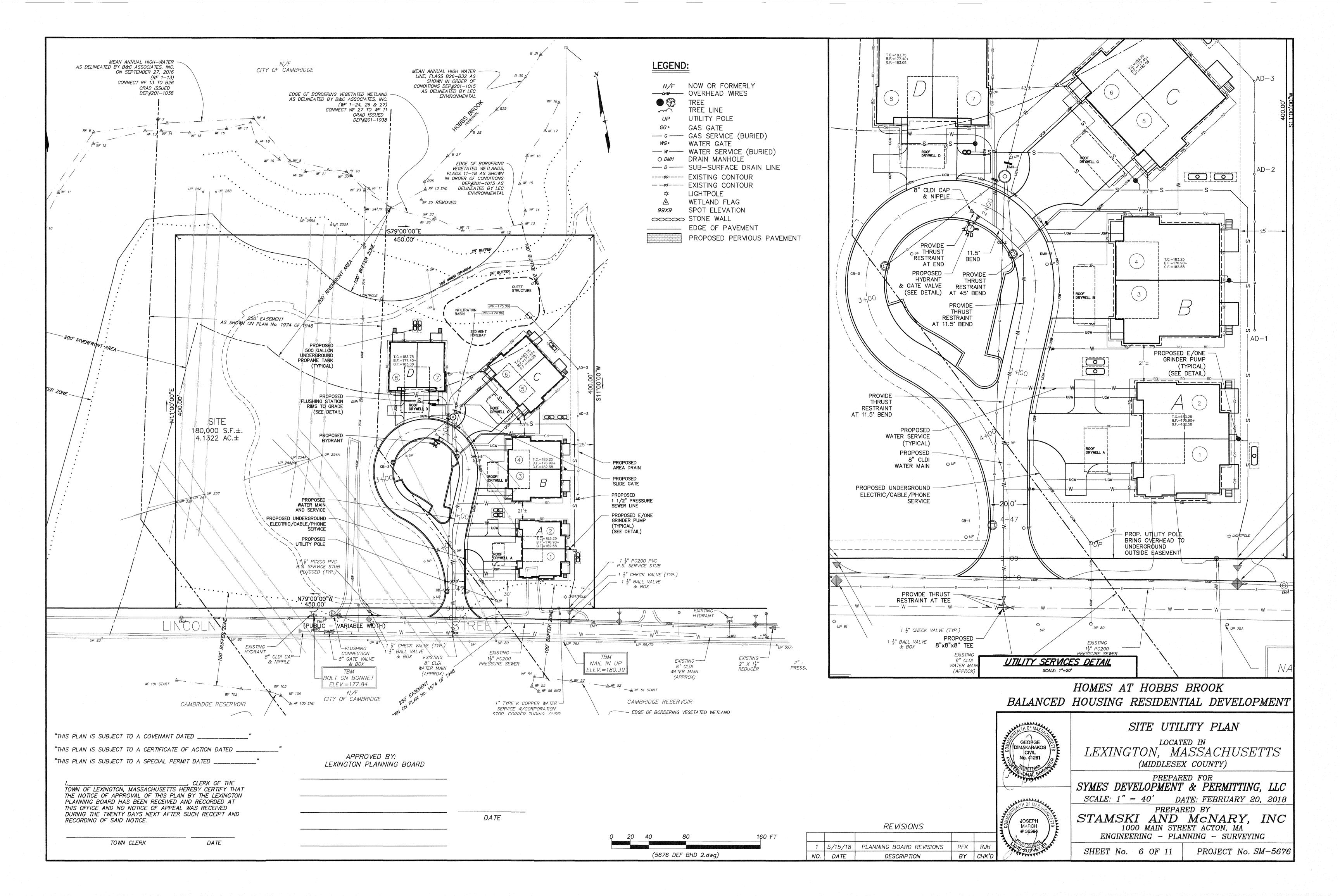
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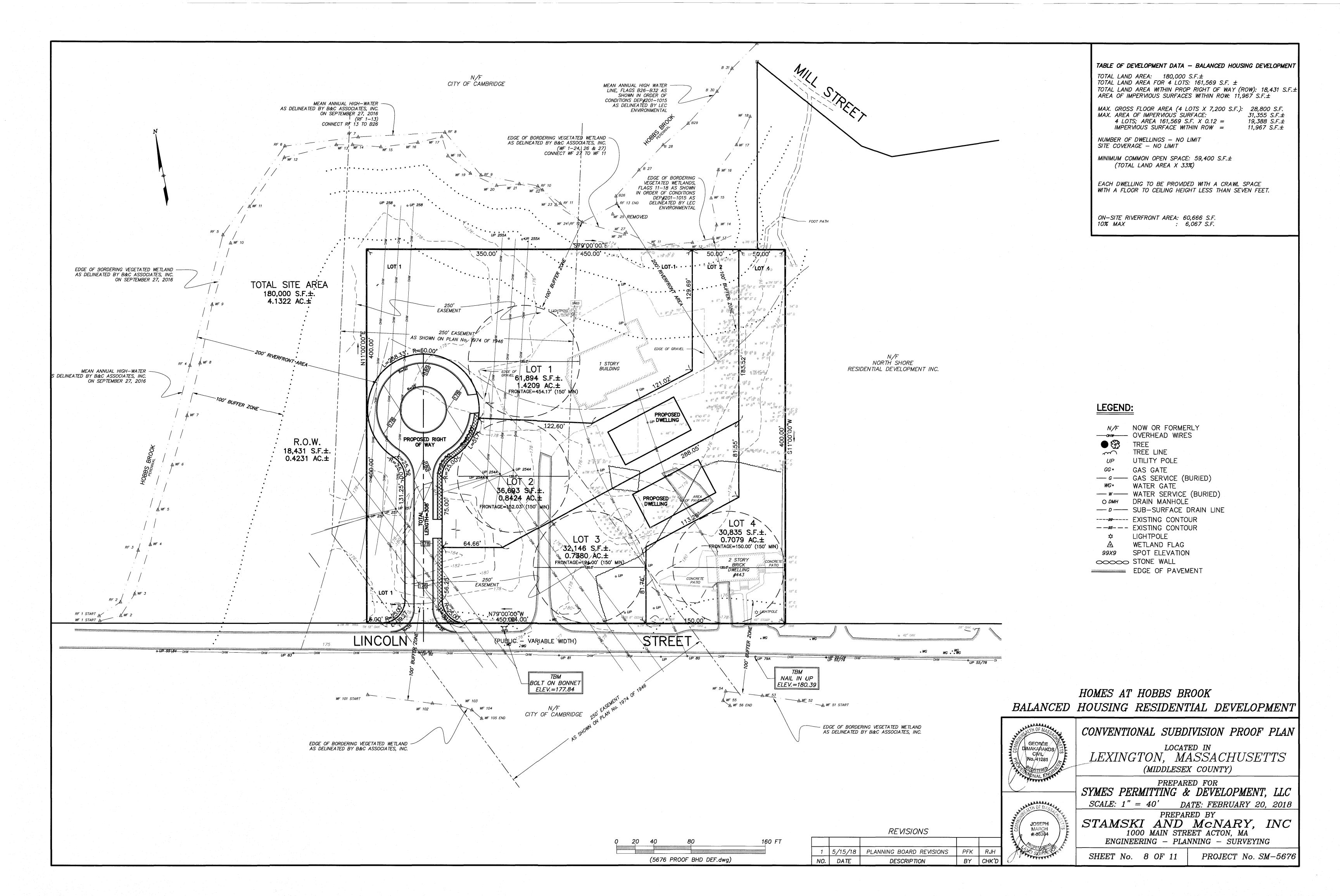
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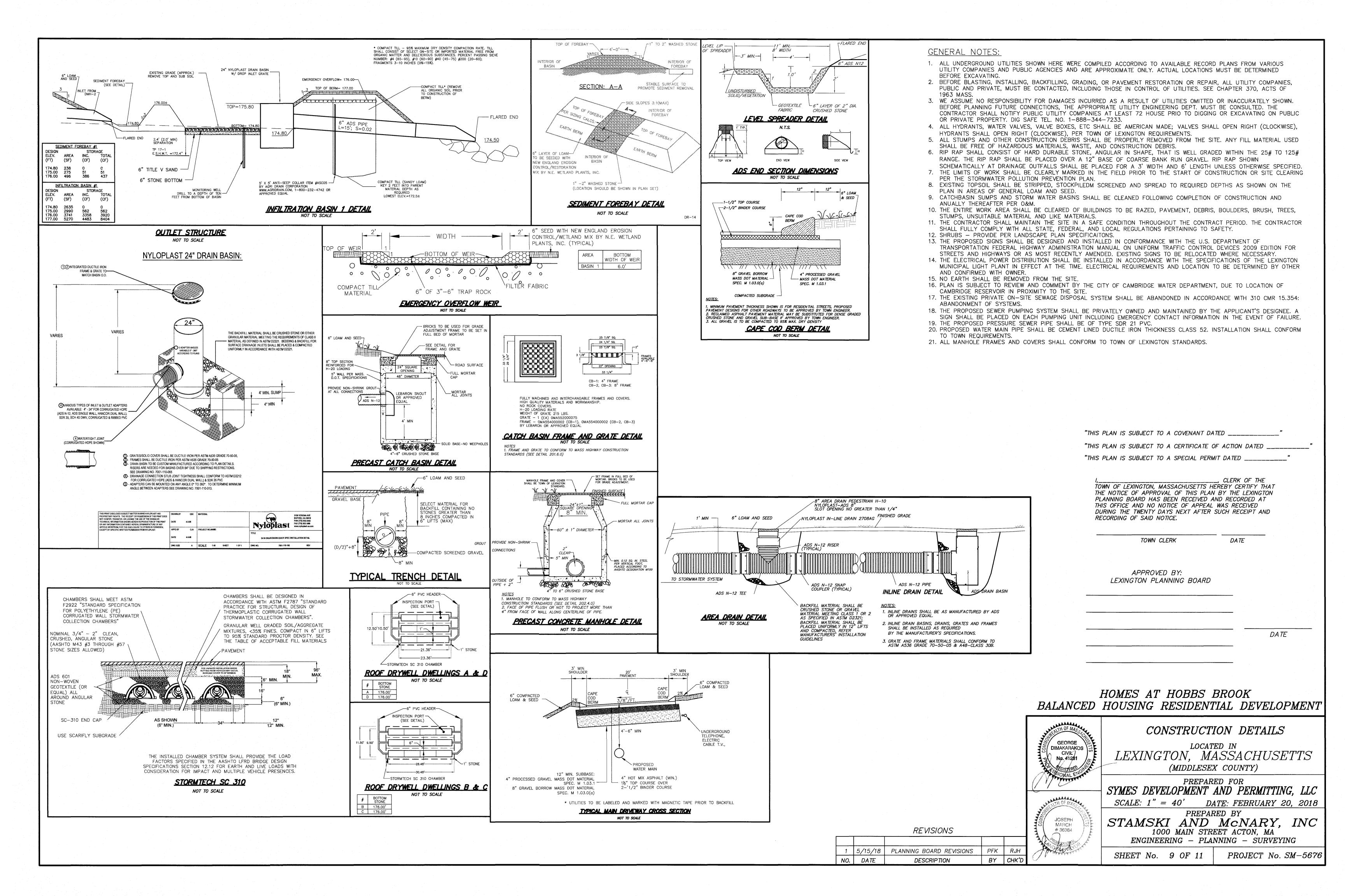
PROJECT No. SM-5676

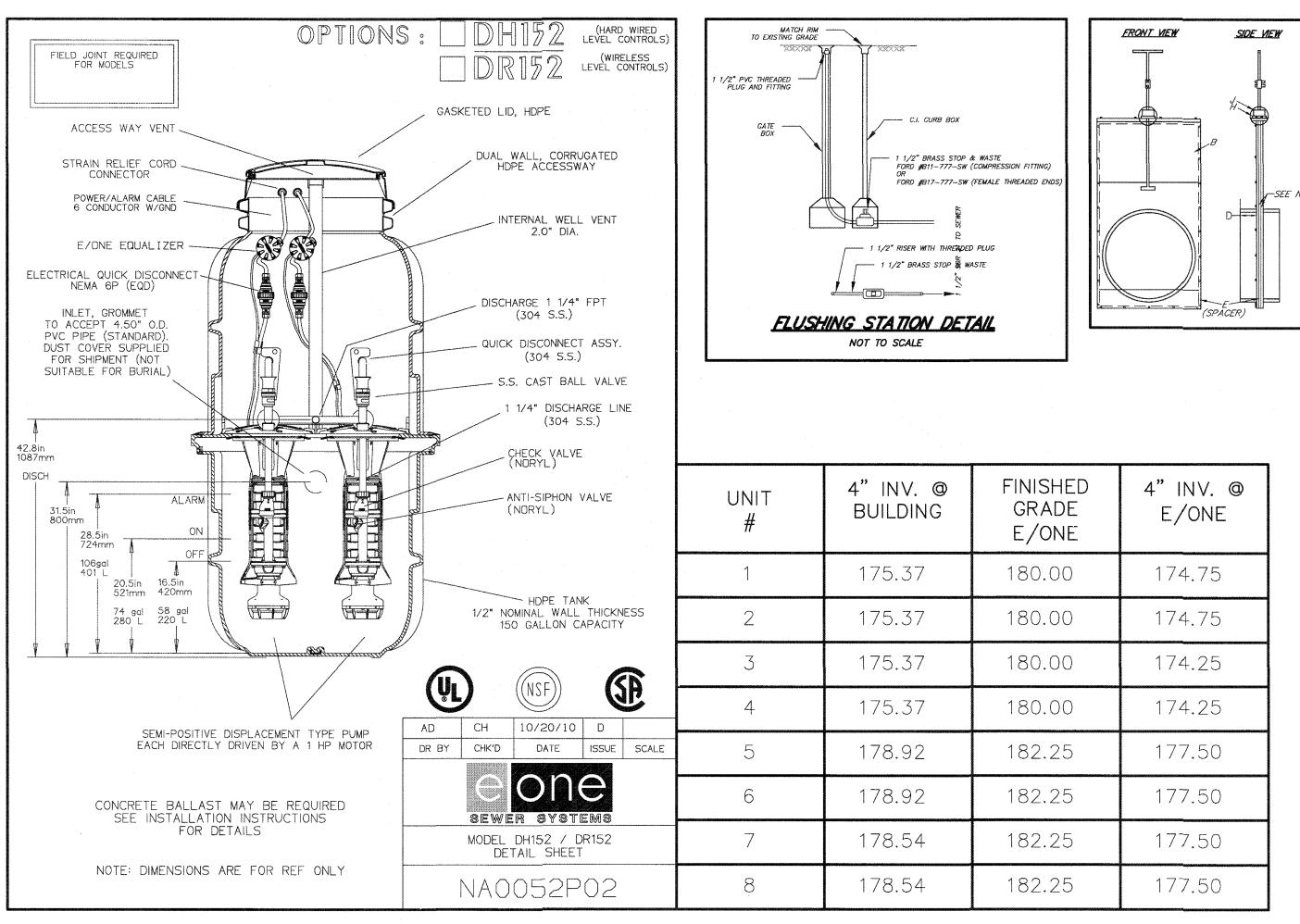
SHEET No. 5 OF 11

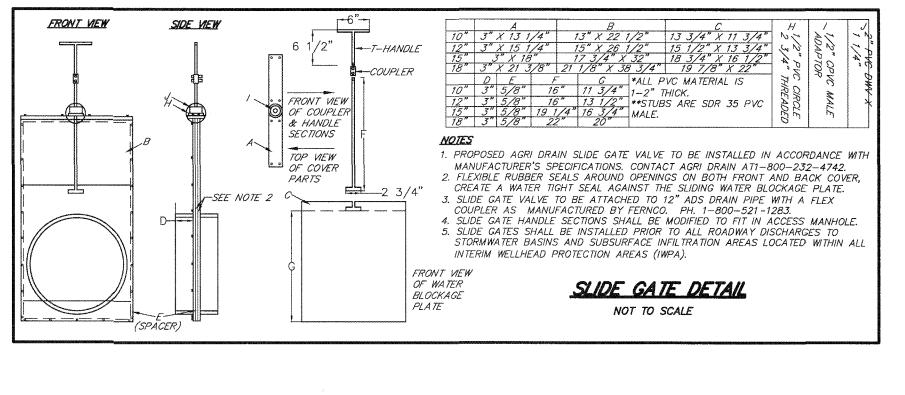
JOSEPH MARCH #38384

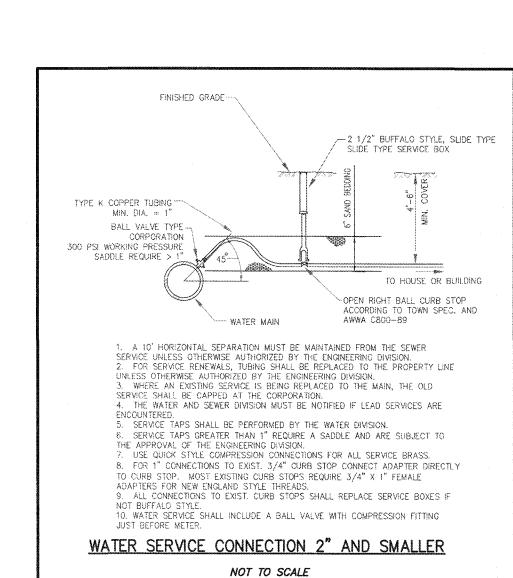


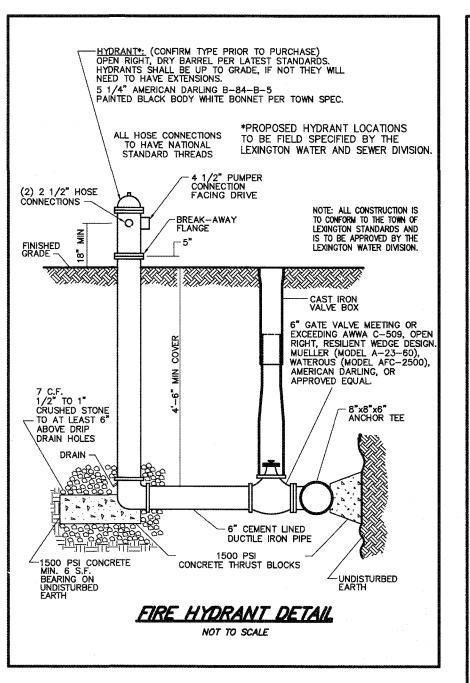


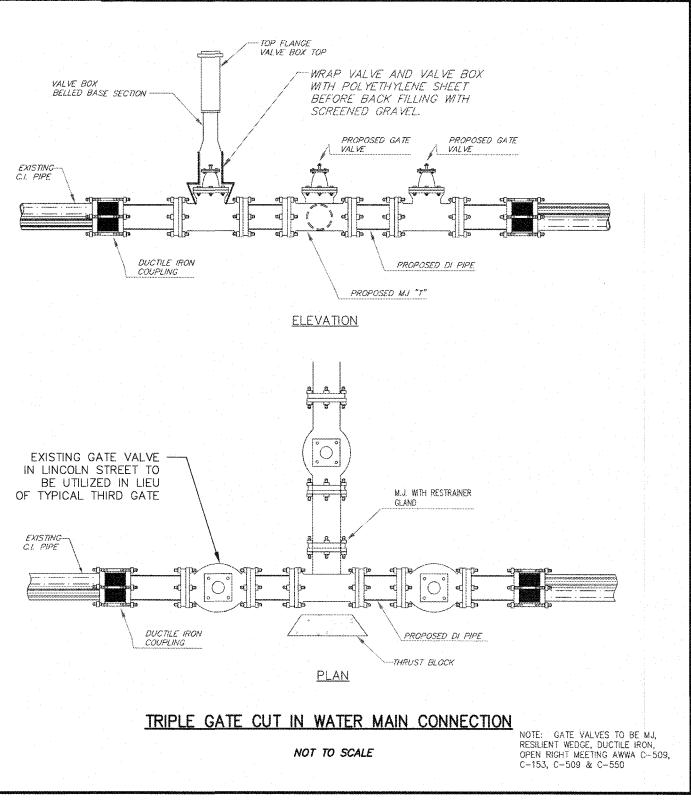


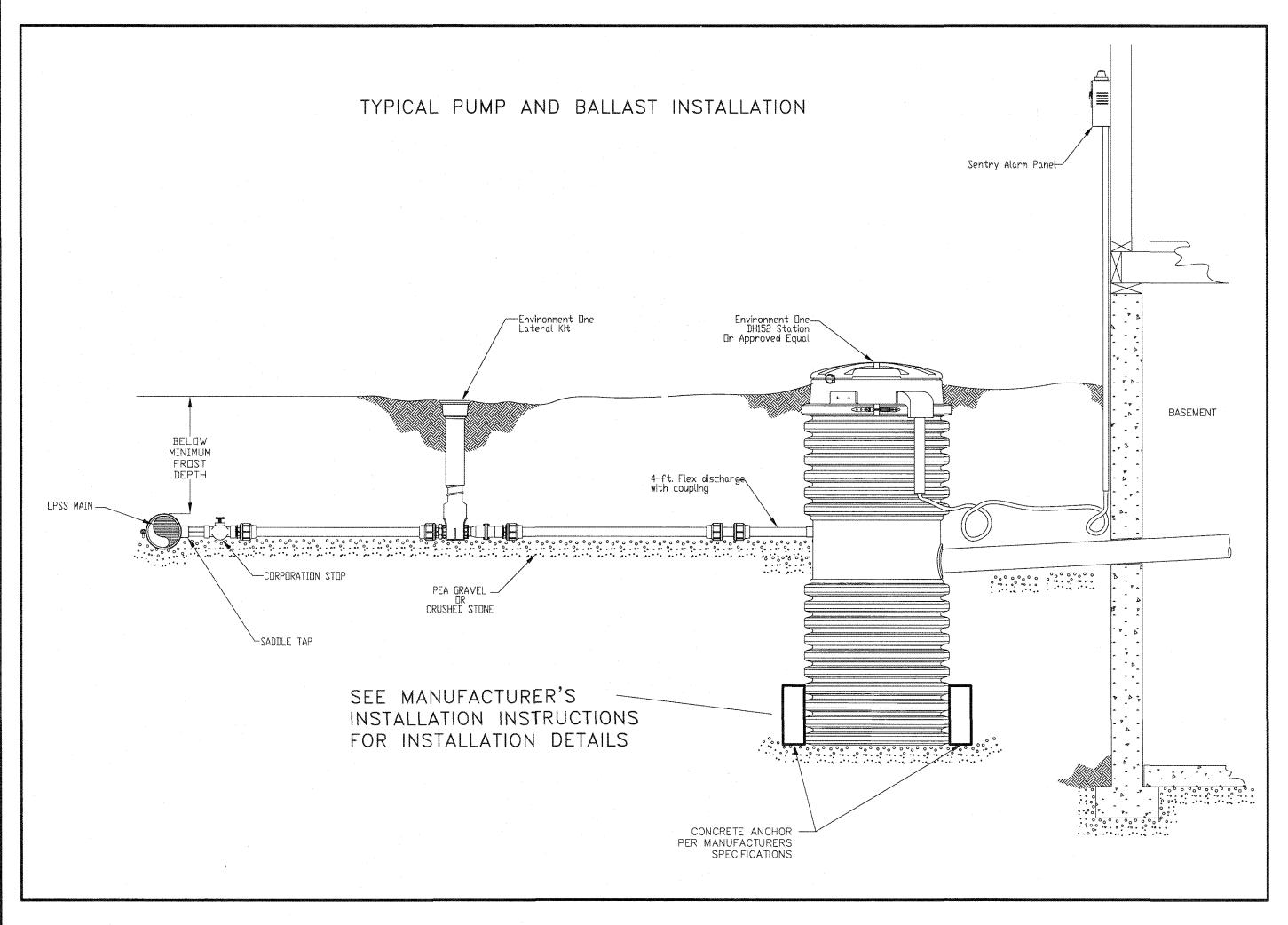


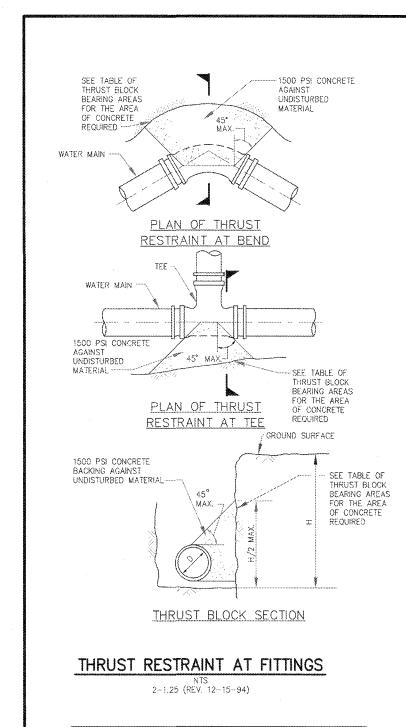


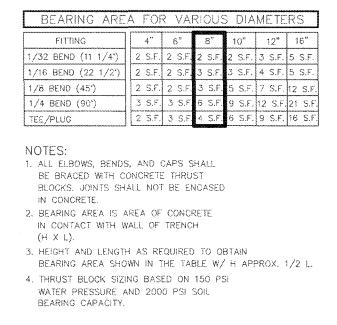


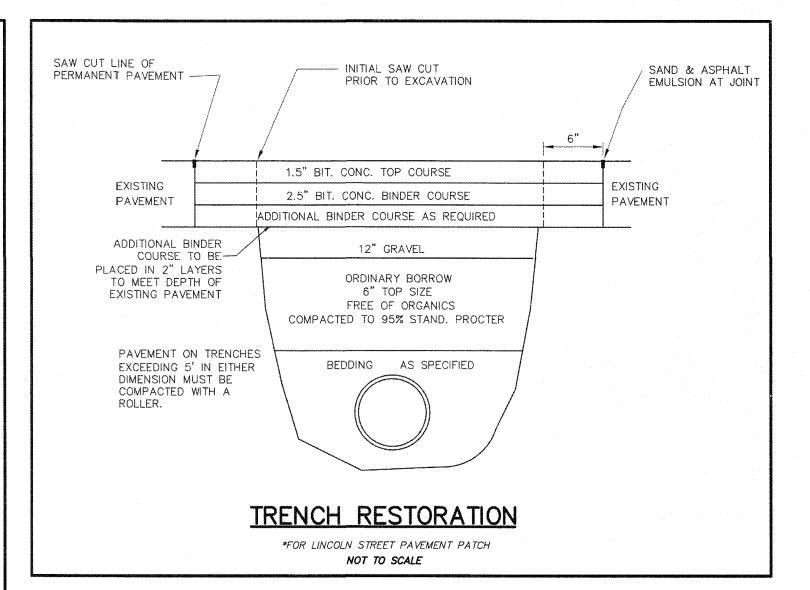












"THIS PLAN IS SUBJECT TO A COVENANT DATED \_\_\_\_\_"

"THIS PLAN IS SUBJECT TO A CERTIFICATE OF ACTION DATED \_\_\_\_\_"

"THIS PLAN IS SUBJECT TO A SPECIAL PERMIT DATED \_\_\_\_\_"

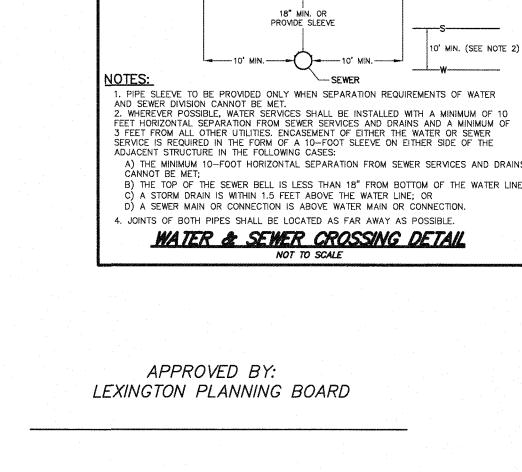
I,\_\_\_\_\_, CLERK OF THE TOWN OF LEXINGTON, MASSACHUSETTS HEREBY CERTIFY THAT THE NOTICE OF APPROVAL OF THIS PLAN BY THE LEXINGTON PLANNING BOARD HAS BEEN RECEIVED AND RECORDED AT THIS OFFICE AND NO NOTICE OF APPEAL WAS RECEIVED DURING THE TWENTY DAYS NEXT AFTER SUCH RECEIPT AND RECORDING OF SAID NOTICE.

TOWN CLERK

REVISIONS

DATE

1	5/15/18	PLANNING BOARD REVISIONS	PFK	RJH
NO.	DATE	DESCRIPTION	BY	CHK'D

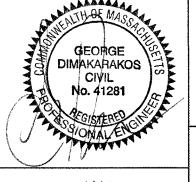


LARGER PIPE DIAMETER SLEEVE

WATER MAIN

FILL WITH
GRANULAR MATERIAL

HOMES AT HOBBS BROOK
BALANCED HOUSING RESIDENTIAL DEVELOPMENT



# CONSTRUCTION DETAILS

LOCATED IN
LEXINGTON, MASSACHUSETTS
(MIDDLESEX COUNTY)

DATE

PREPARED FOR

SYMES DEVELOPMENT AND PERMITTING, LLC

SCALE: 1" = 40' DATE: FEBRUARY 20, 2018

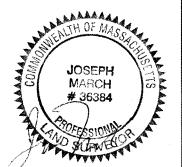
PREPARED BY

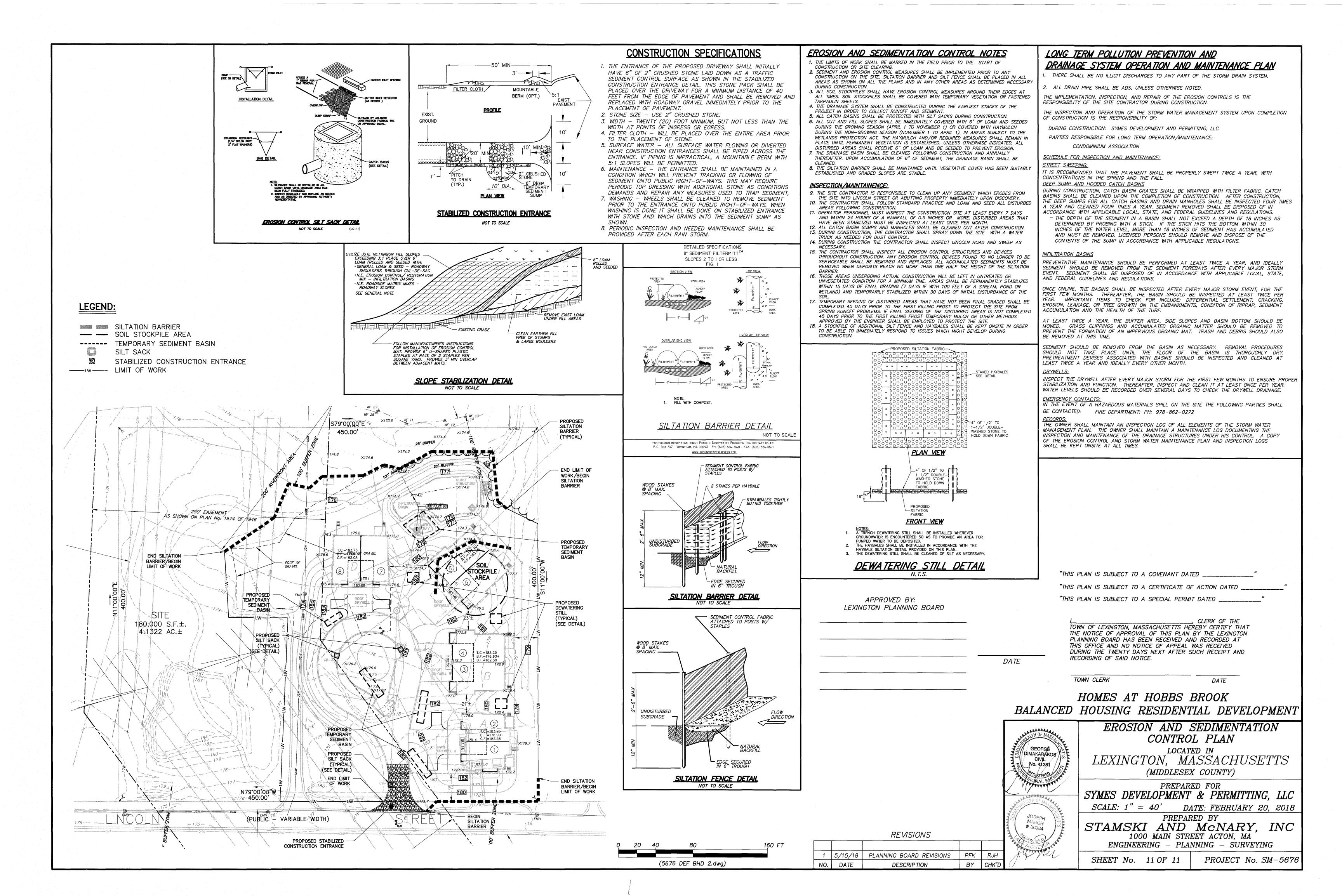
STAMSKI AND McNARY, INC

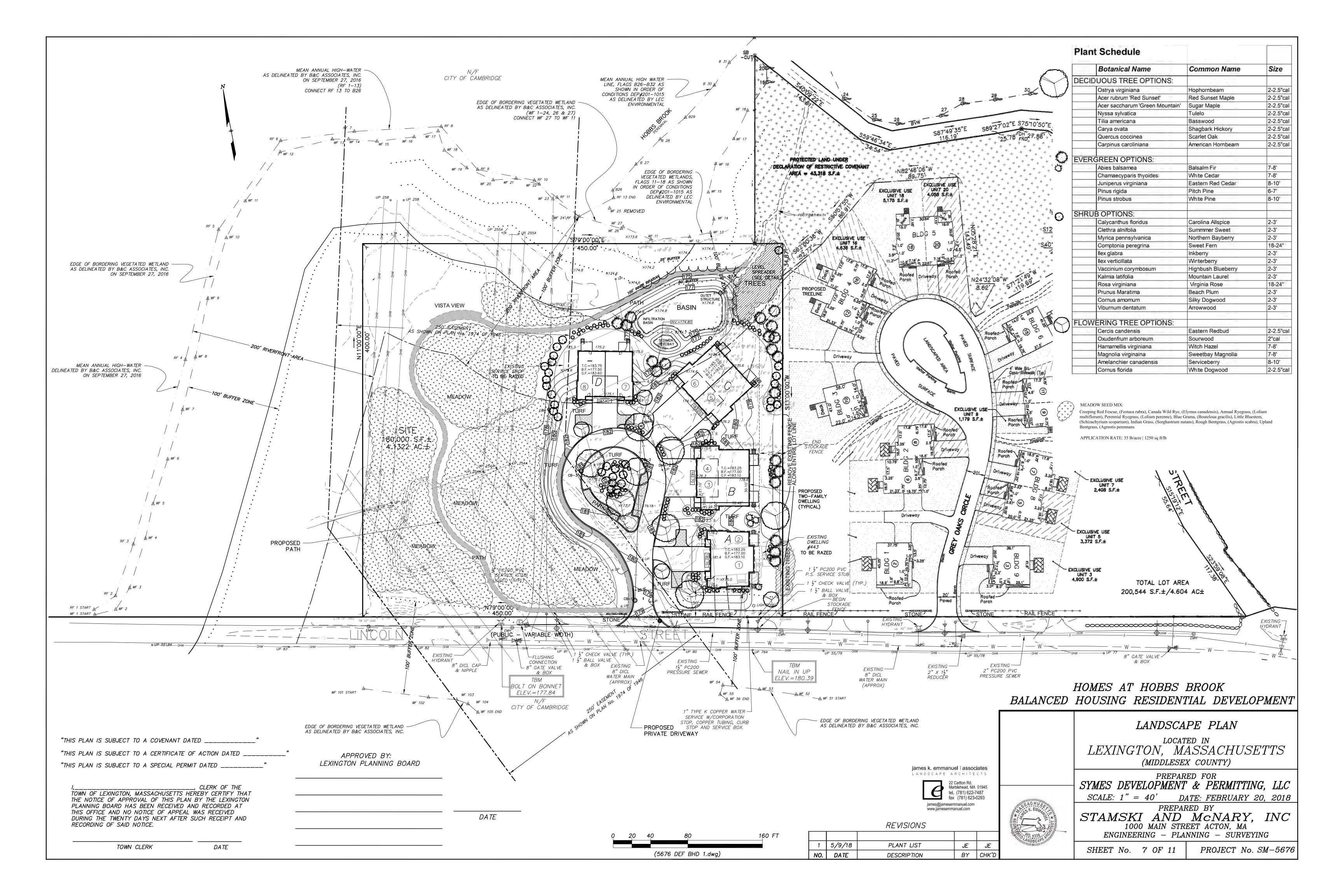
1000 MAIN STREET ACTON, MA

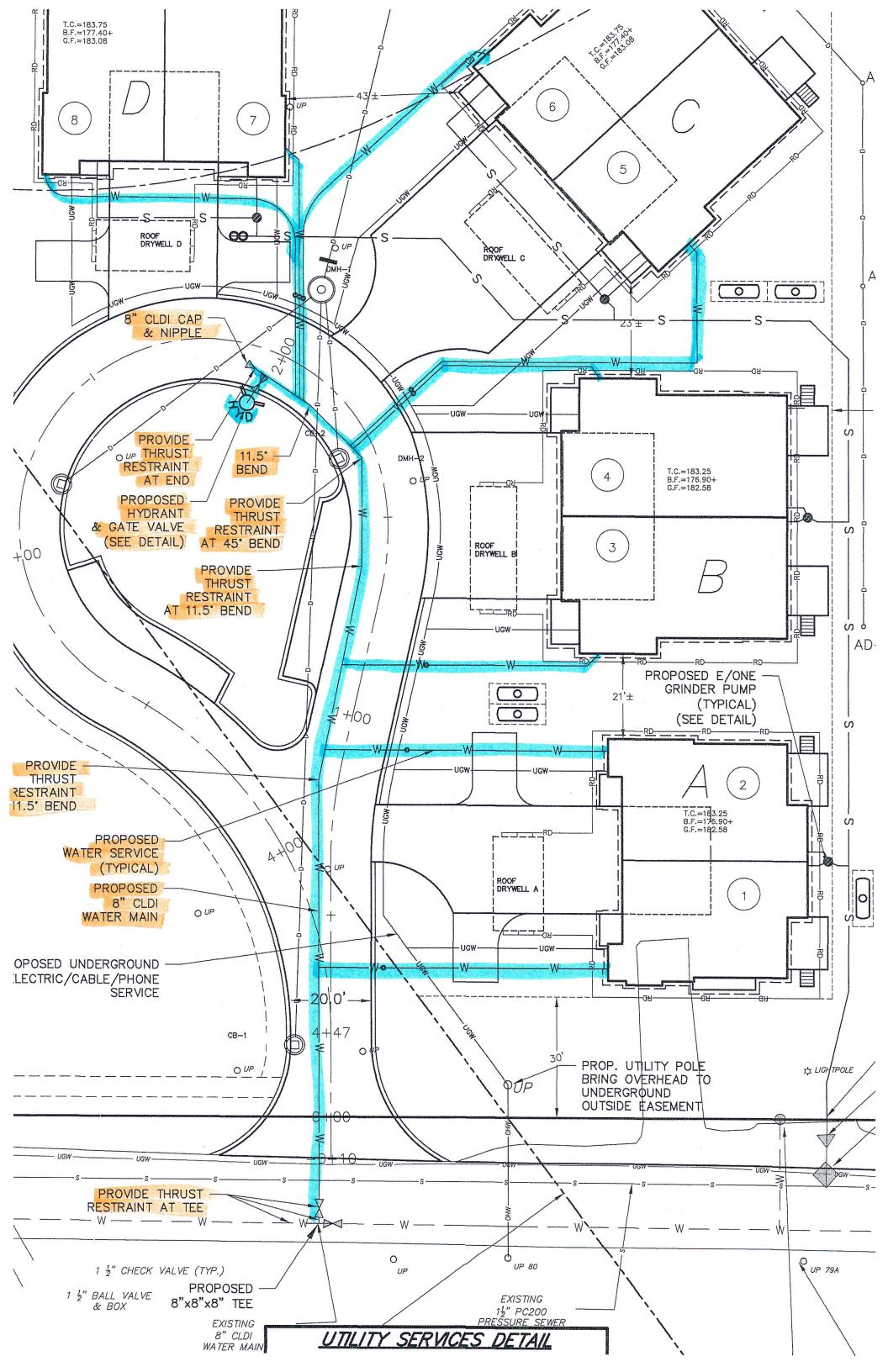
ENGINEERING - PLANNING - SURVEYING

SHEET No. 10 OF 11 PROJECT No. SM-5676





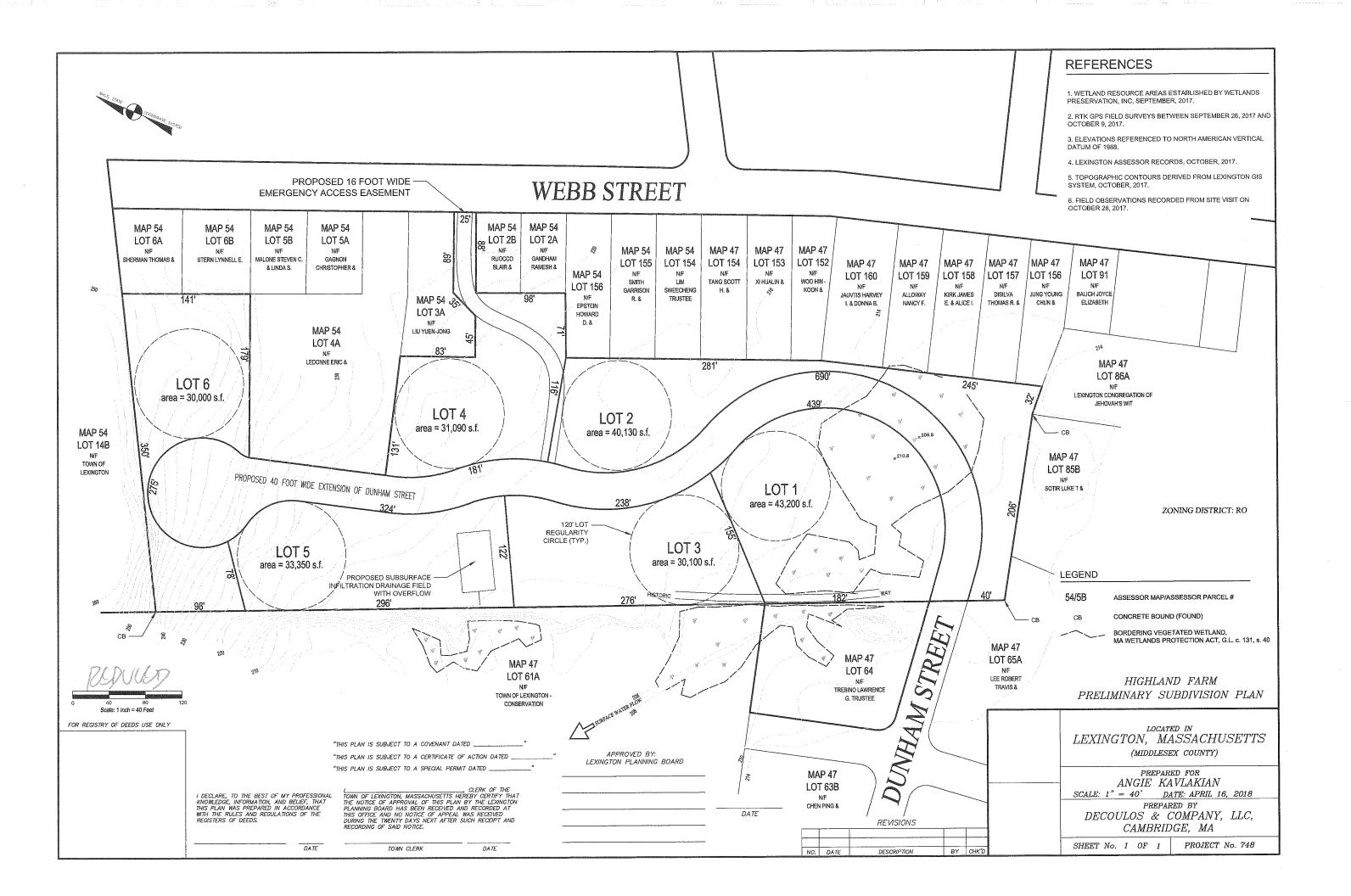




#### LEXINGTON PLANNING BOARD

<b>AGENDA</b>	<b>ITEM</b>	TITLE:
---------------	-------------	--------

56 V	Webb Street: Preliminary Plan	
<u>PR</u>	ESENTER:	ITEM NUMBER
<u>SUN</u>	MMARY:	
Sub		y subdivision plan under Section 175-5.0 of the Planning Board's mal subdivision. Attached is a copy of the subdivision plan and
SUC	GGESTED MOTION:	
FOI	LLOW-UP:	
	ΓΕ AND APPROXIMATE TIME O	ON AGENDA:
5/24/	/2018	
AT'	TACHMENTS:	
	Description	Туре
D	56 Webb Street Preliminary Plan	Backup Material
D	Staff Report	Backup Material





**Item Name/Description:** 56 Webb Street Preliminary Subdivision Plan

**Application Date:** April 26, 2018

**Constructive Approval** 

Date:

June 10, 2018 (45 days)

Proposed Meeting Date: May 24, 2018

#### **Procedural Summary**

Decoulos and Company, LLC., on behalf of Angie Kavlakian (applicant), submitted a plan for a preliminary subdivision at 56 Webb Street and 0 Dunham Street, Assessor's map 47, Lot 155A and Lot 64, respectively, on April 26, 2018. This is the first time this matter will come before the Planning Board (the Board).

#### **Staff Comments**

The proposal for a conventional subdivision consists of six (6) lots laid out on a single street terminating in a cul-de-sac. The street is proposed to be an extension of Dunham Street, which currently only exists in paper form adjacent to the property owned by the applicant. The applicant has not requested any waivers from the Board for the current preliminary plan. The lots, as laid out, all appear to meet the zoning requirements for the RO zone in which the parcel resides.

For the reasons explained below, staff does not believe this plan shows a conforming subdivision, primarily because it includes a dead-end street that exceeds the limits permitted by the Planning Board *Subdivision Regulations*, Chapter 175 of Lexington Code.

Specifically, the single sheet preliminary subdivision plan, titled "Highland Farm," submitted to the Planning Office does not conform to the requirements of §175-7.2.E(7)(a), which reads:

A dead-end street may not be longer than 650 feet from the point of beginning following the centerline to the furthest point on the right-of-way line. The point of beginning of a dead end street or way or of a system of dead end streets or ways is the point of intersection of street centerlines with a street of which there are two or more distinct vehicular access routes to the general street network of the Town.

Section §175-7.2 in turn defines a dead-end street, road, or way as follows:

Either [A] a street providing only one vehicular access route to the general street network of the Town or [B] a system of two or more intersecting streets whose overall layout provides only one vehicular access route to the general street network of the Town. Multiple vehicular access points less than 125 feet apart are considered a single access point.

The current paved way entering off of Woburn Street, consisting of Utica and then Dunham Streets, is a pre-existing, nonconforming dead-end street approximately 1,000 feet in length with only one means of ingress and egress. There is a paper, laid out right-of-way that then continues for approximately another 225 feet before terminating at the parcel owned by the applicant, map and lot number 47-155A. The proposed way, as shown on the preliminary plan, is approximately 1,200 feet in length not including the existing, paved way and also has only one means of ingress and egress. Combining the proposed way and the existing way would create a dead-end street approximately 2,200 feet in length, over three times the distance the current *Subdivision Regulations* allow for a dead-end street, and nearly a half-mile in length.

The proposal also includes a 16 foot wide paved easement that would connect the proposed extension of Dunham Street to Webb Street. Staff does not believe that this "emergency access easement" meets the definition of a street, road or way, as stated in the Zoning Bylaw, §135-10.1, nor does it conform to the standards laid out in the *Subdivision Regulations*, §175-7.2.E(1)(c). The "emergency access easement" would be too narrow to satisfy the design standards for streets and rights-of-way in the *Subdivision Regulations* §175-7.2.E(1)(c). Thus, in staff's opinion, the easement is not a street, rendering the proposed plan invalid.

Further, the emergency access easement does not augment the proposed dead end road in a manner that avoids its violation of the *Subdivision Regulations* as described above. The applicant appears to be claiming that the emergency access easement as laid out allows for a second means of vehicular access to the proposed forty (40) foot right-of-way such that this latter, wider right of way would not be a dead end street. However, as explained above, the access easement has too many deficiencies in the layout to qualify as a "street, road, or way," meaning the entirety of the extended Dunham Street is a dead-end.

Staff notes that the means of vehicular access must be a way as laid out in the Town's *Subdivision Regulations*, unless waived by the Planning Board in such a way as to not endanger the health and safety of the public. In other words, such "vehicular access routes" must qualify as "streets, roads, or ways" under the *Subdivision Regulations*. The proposed emergency access route does not meet this requirement.

Requiring adequate emergency access to new subdivisions is consistent with the goals of the of the Commonwealth's Subdivision Control Law. As described in G.L. c. 41, §81M the Planning Board's powers are to be exercised:

with due regard for the provision of adequate access to all of the lots in a subdivision by ways that will be safe and convenient for travel....for securing

safety in the case of fire, flood, panic and other emergencies....

The current plan, in staff's opinion, does not adequately meet the requirements for streets as described in Lexington's *Subdivision Regulations* because emergency access will be too limited.

#### Other Office or Division Comments

The Engineering Office comments will be submitted under a separate cover upon their submission. The Health Office has not submitted any comments in regard to this subdivision plan. The Departments of Fire and Public Safety have not submitted comments on this project.

#### Staff Recommendation

Planning Office staff does not recommend approval of this preliminary subdivision plan for the reasons stated above. The plan does not comply with §175-7.2 with regard to the proposed lay out of the right-of-way. Given the issues with the right-of-way, staff has not analyzed other potential issues with this preliminary plan. Any other issues, including whether it would be appropriate for the Planning Board to grant a waiver of this requirement if the applicant were to request one, would require further analysis by staff. However, potential concerns are bulleted below:

- The horizontal curvature of the laid out way proposed as an extension of Dunham Street would need to be reviewed by the Engineering Department;
- The drainage and stormwater system needs further clarification and submission of a drainage and stormwater management plans is required by §175-5.3.A(2);
- The developable site area for each lot shown on the plan requires calculation per §135-4.2.3 of the Code of Lexington.

#### LEXINGTON PLANNING BOARD

LEAINGION FLANNING BUARD	
AGENDA ITEM TITLE:	
PSDUP Sketch Decision: 7 Hartwell Avenue	
PRESENTER:  NUMB	
SUMMARY:	
Decision is in the process of being drafted and will be posted before meeting occurs.	
SUGGESTED MOTION:	
FOLLOW-UP:	
DATE AND APPROXIMATE TIME ON AGENDA:	

5/24/2018

#### LEXINGTON PLANNING BOARD

#### **AGENDA ITEM TITLE:**

Comprehensive Plan Update

PRESENTER:

ITEM
NUMBER:

Aaron Henry, Planning Director

3

#### **SUMMARY:**

This is a standing item to allow staff to update the Board on the status of the Comprehensive Plan and related initiatives. Upcoming meetings include the following:

- Housing Panel May 29, 2018 (7PM) Lexington Community Center Rm. 237
- Comprehensive Plan Kick-Off Event June 4, 2018 (7PM) Battin Hall, Cary Memorial Building

#### **SUGGESTED MOTION:**

There is no Board action required for this item.

#### **FOLLOW-UP:**

#### **DATE AND APPROXIMATE TIME ON AGENDA:**

5/24/2018

#### LEXINGTON PLANNING BOARD

#### **AGENDA ITEM TITLE:**

Upcoming Meetings & Anticipated Schedule

PRESENTER:

NUMBER:

Aaron Henry, Planning Director

2

#### **SUMMARY:**

This recurring agenda item is to inform the Board and public of the proposed meeting schedule. The next Planning Board Meetings are scheduled for the following dates:

- Thursday, June 7, 2018
- Thursday, June 21, 2018

FY 19 (July 2018-June 2019) meeting calendar & schedule are attached for the Board's review.

#### **SUGGESTED MOTION:**

There is no need for the Board to act on this item.

#### **FOLLOW-UP:**

Should Board members have any known conflicts with any of the proposed dates or wish to request an item be placed on a meeting agenda, please follow up with staff.

#### **DATE AND APPROXIMATE TIME ON AGENDA:**

5/24/2018

#### **ATTACHMENTS:**

Description Type

☐ FY19 Planning Board Calendar Backup Material

FY19 Planning Board Meeting Schedule Backup Material

# Fiscal Year 2019

2018				2019							
July	August	September	October	November	December	January	February	March	April	May	June
1 Su	1 We	1 Sa	1 Mo	1 Th PB MTG	1 Sa	1 Tu New Year's Day	1 Fr	1 Fr	1 Mo ATM	1 We ATM	1 Sa
2 Mo	2 Th	2 Su	2 Tu	2 Fr	2 Su	2 We	2 Sa	2 Sa	2 Tu	2 Th	2 Su
3 Tu	3 Fr	3 Mo Labor Day	3 We	3 Sa	3 Mo	3 Th	3 Su	3 Su	3 We ATM	3 Fr	3 Mo
4 We Independe nce Day	4 Sa	4 Tu	4 Th PB MTG	4 Su	4 Tu	4 Fr	4 Mo	4 Mo ELECTION	4 Th	4 Sa	4 Tu
5 Th	5 Su	5 We	5 Fr	5 Mo	5 We	5 Sa	5 Tu	5 Tu	5 Fr	5 Su	5 We
6 Fr	6 Mo	6 Th	6 Sa	6 Tu	6 Th	6 Su	6 We	6 We	6 Sa	6 Mo	6 Th PB MTG
7 Sa	7 Tu	7 Fr	7 Su	7 We	7 Fr	7 Mo	7 Th	7 Th	7 Su	7 Tu	7 Fr
8 Su	8 We	8 Sa	8 Mo Columbus Day	8 Th	8 Sa	8 Tu	8 Fr	8 Fr	8 Mo ATM	8 We	8 Sa
9 Mo	9 Th	9 Su	9 Tu	9 Fr	9 Su	9 We	9 Sa	9 Sa	9 Tu	9 Th PB MTG	9 Su
10 Tu	10 Fr	10 Mo Rosh	10 We	10 Sa	10 Mo	10Th PB MTG	10 Su	10 Su	10 We ATM	10 Fr	10 Mo
11 We	11 Sa		11 Th	11 Su	11 Tu	11 Fr	11 Mo	11 Mo	11 Th	11 Sa	11 Tu
12 Th PB MTG	12 Su	12We	12 Fr	12 Mo Veterans Day	12 We	12 Sa	12 Tu	12 Tu	12 Fr	12 Su	12 We
13 Fr	13 Mo	13Th PB MTG	13 Sa	13 Tu STM	13 Th PB MTG	13 Su	13 We	13 We	13 Sa	13 Mo	13 Th
14 Sa	14 Tu	14Fr	14 Su	14 We STM	14 Fr	14 Mo	14 Th PB MTG	14 Th PB MTG	14 Su	14 Tu	14 Fr
15 Su	15 We	15Sa	15 Mo	15 Th STM	15 Sa	15 Tu	15 Fr	15 Fr	15 Mo Patriot's Day	15 We	15 Sa
16 Mo	16 Th PB MTG	16Su	16 Tu	16 Fr	16 Su	16 We	16 Sa	16 Sa	16 Tu	16 Th	16 Su
17 Tu	17 Fr	17Mo	17 We	17 Sa	17 Mo	17 Th PB MTG	17 Su	17 Su	17 We	17 Fr	17 Mo
18 We	18 Sa	18Tu Eve Yom Kippur	18 Th <b>PB MTG</b>	18 Su	18 Tu	18 Fr	18 Mo Presidents' Day	18 Mo	18 Th	18 Sa	18 Tu
19 Th	19 Su	19We Kippur	19 Fr	19 Mo	19 We	19 Sa	19 Tu	19 Tu	19 Fr	19 Su	19 We
20 Fr	20 Mo	20Th PB MTG	20 Sa	20 Tu	20 Th	20 Su	20 We	20 We	20 Sa	20 Mo	20 Th PB MTG
21 Sa	21 Tu	21 Fr	21 Su	21 We	21 Fr	21 Mo MLK Day	21 Th	21 Th	21 Su	21 Tu	21 Fr
22 Su	22 We	22Sa	22 Mo	22 Th Thanks-giving	22 Sa	22 Tu	22 Fr	22 Fr	22 Mo ATM	22 We	22 Sa
23 Mo	23 Th	23 Su	23 Tu	23 Fr	23 Su	23 We	23 Sa	23 Sa	23 Tu	23 Th PB MTG	23 Su
24 Tu	24 Fr	24 Mo	24 We	24 Sa	24 Mo	24 Th	24 Su	24 Su	24 We ATM	24 Fr	24 Mo
25 We	25 Sa	25Tu	25 Th	25 Su	25 Tu Christmas Day	25 Fr	25 Mo	25 Mo ATM	25 Th PB MTG	25 Sa	25 Tu
26 Th PB MTG	26 Su	26We	26 Fr	26 Mo	26 We	26 Sa	26 Tu	26 Tu	26 Fr	26 Su	26 We
27 Fr	27 Mo	27Th	27 Sa	27 Tu	27 Th	27 Su	27 We	27 We ATM	27 Sa	27 Mo Memorial Day	27 Th
28 Sa	28 Tu	28Fr	28 Sa	28 We	28 Fr	28 Mo	28 Th PB MTG	28 Th	28 Su	28 Tu	28 Fr
29 Su	29 We	29 Sa	29 Mo	29 Th PB MTG	29 Sa	29 Tu		29 Fr	29 Mo ATM	29 We	29 Sa
30 Mo	30 Th PB MTG	30 Su	30 Tu	30 Fr	30 Su	30 We	$\times$	30 Sa	30 Tu	30 Th	30 Su
31 Tu	31 Fr		31 We		31 Mo	31 Th PB MTG		31 Su		31 Fr	

FY		Ad Due	Ad Run Dates #1 #2		Notes	
MTG#	Important dates	(LMM)				
1	07/12/2018	06/21/18	06/28/18	07/05/18		
2	07/26/2018	07/05/18	07/12/18	07/19/18		
3	08/16/2018	07/26/18	08/02/18	08/09/18		
	08/20/2018				BOS meeting regarding warrant STM?	
	08/22/2018				legal ad due to LMM/motions ready	
4	08/30/2018	08/09/18	08/16/18	08/23/18	legal ad 1 STM PH	
	09/06/2018				legal ad 2 STM PH	
5	09/13/2018	08/23/18	08/30/18	09/06/18	Open STM Public Hearings-1	
6	09/20/2018	08/30/18	09/06/18	09/13/18	STM Public Hearing 2	
7	10/04/2018	09/13/18	09/20/18	09/27/18	STM Public Hearing 3	
8	10/18/2018	09/27/18	10/04/18	10/11/18	Close Public hearings	
9	11/01/2018	10/11/18	10/18/18	10/25/18	DUE: STM REPORTS	
	11/13/2018				STM; Pre-TM Mtg	
	11/14/2018				STM; Pre-TM Mtg	
10	11/15/2018	10/25/18	11/01/18	11/08/18	STM; Pre-TM Mtg	
11	11/29/2018	11/07/18	11/14/18	11/21/18		
12	12/13/2018	11/20/18	11/29/18	12/06/18	legal ad in early LMM Thanksgiving holiday	
	12/28/2018				DUE: ATM MOTIONS to BOS	
13	01/10/2019	12/18/18	12/27/18	01/03/19		
					legal ad in early LMM Christmas Legal ad 1	
14	01/17/2019	12/26/18	01/03/19	01/10/19	ATM PH motion ready	
	01/24/2019				legal ad 2 ATM PH	
					Legal ad in early LMM presidents day	
15	01/31/2019	01/10/19	01/17/19	01/24/19	Open ATM Public Hearings-1	
16	02/14/2019	01/24/19	01/31/19	02/07/19	ATM Public Hearing 2	
17	02/28/2019	02/07/19	02/14/19	02/21/19	Close ATM Public hearings	
18	03/13/2019	02/21/19	02/28/19	03/06/19	DUE: ATM REPORTS	
19	03/25/2019	02/28/19	03/07/19	03/14/19	Town Meeting Start; Pre-TM Mtg	
20	03/27/2019	02/28/19	03/07/19	03/14/19	Pre-TM Mtg	
21	04/01/2019	03/07/19	03/14/19	03/21/19	Pre-TM Mtg	
22	04/03/2019	03/07/19	03/14/19	03/21/19	Pre-TM Mtg	
23	04/08/2019	03/14/19	03/21/19	03/28/19	Pre-TM Mtg	
24	04/10/2019	03/14/19	03/21/19	03/28/19	Pre-TM Mtg	
25	04/22/2019	03/28/19	04/04/19	04/11/19	Pre-TM Mtg	
26	04/24/2019	03/28/19	04/04/19	04/11/19	Pre-TM Mtg	
27	04/29/2019	04/04/19	04/11/19	04/18/19	Pre-TM Mtg	
28	05/01/2019	04/04/19	04/11/19	04/18/19	Pre-TM Mtg	
29	05/09/2019	04/18/19	04/25/19	05/02/19	Begin Reg Updates; PB Reorganize	
30	05/23/2019	05/02/19	05/09/19	05/16/19		
31	06/06/2019	06/16/19	05/23/19	05/30/19		
					Legal ad in early LMM Memorial day	
32	06/20/2019	05/29/19	06/06/19	06/13/19	Finalize Reg Updates	

#### LEXINGTON PLANNING BOARD

AGENDA ITEM TITLE:	
Minutes	
PRESENTER:	<u>ITEM</u> NUMBER
SUMMARY:	
Drafts of the following meeting minutes will be reviewed by • May 10, 2018	the Planning Board:
SUGGESTED MOTION:	
FOLLOW-UP:	
DATE AND APPROXIMATE TIME ON AGENDA	<u>\( \cdot \):</u>
5/24/2018	
ATTACHMENTS:	Tyro
Description Draft PB Meeting Minutes 5-10-18	Type  Backup Material
	•

#### PLANNING BOARD MINUTES

MEETING OF MAY10, 2018

### **Upcoming Meetings & Anticipated Meetings:**

The next three Planning Board meetings are May 24, June 7 and 21.

Other upcoming meetings are May 22, CPAC Meeting, May 23, Economic Development Panel #2, May 29, Housing Panel #2, May 30, Joint BOS and PB- Hartwell Avenue Initiative, and June 4, Comprehensive Plan Kick Off Event.

#### **Comprehensive Plan Update:**

The RFP deadline was April 20 and a decision will be made next week and shared at the next meeting. Board Members can send staff recommendations on the RFP.

#### **Planning Director Position:**

Mr. Valenti explained the transition plan for the departure of Mr. Henry, Planning Director. The recruitment process began last week with a closing date of June 8, 2018 and are looking at Labor Day to have a new director in place. In the meantime Mr. Valenti recommended Carol Kowalski, Assistant Town Manager for Development serve as the interim Planning Director.

#### **Board Comments:**

- There was concern about the additional work since a full time staff member is needed and
  wants to make sure there will enough time for Ms. Kowalski to be able to handle the
  work load that would be required.
- Board members are delighted to work with her more closely.
- If additional resources are needed can the extra monies from salary be used for additional help? Can go to Town Meeting and can be done if needed.

On a motion of Ms. Johnson, seconded by Ms. Corcoran-Ronchetti, it was voted, 5-0, to accept the Town Manager's recommendation of Carol Kowalski as the interim Planning Director.

#### **SPRD Committee:**

The Board discussed the draft charge for the Special Permit Residential Development Committee and Mr. Canale's proposed changes.

#### **Board Comments:**

- The charge needs to be clear about what was meant by joint and if both boards do not agree that does not stop the process.
- Would like Board of Selectmen (BOS) Member be a voting member as well as Residential Policy Committee Members.
- This committee would be subject to open meeting law.
- Need to see data and documentation.
- The committee should go back to basics and should leave the scope broad.
- The feasibility piece has been hard to get, the focus should be on what the Board wants to
  get from the project and what is being built and not the amount of money made by the
  developer for the project.
- Do you see this as a policy making committee or a stakeholder committee?
- Having a Real Estate agent on the committee would not be balanced.
- Bring in seven people as committee members and others to participate.
- Advocate moving this forward as soon as possible since this was promised to be brought back for the Fall Special Town Meeting.
- Mr. Canale will speak with Ms. Hai and the Town Manager to get things moving.

#### Net Zero Plan Update:

Mr. Mark Sandeen presented Getting Net Zero Emissions Road map and recommendations to update the Planning Board. The presentation can be found in the meeting packet for May 10, 2018.

The goal would be how to get this incorporated into the Comprehensive Plan.

#### 17 Tower Road, ANR:

On a motion of Mr. Hornig, seconded by Ms. Corcoran-Ronchetti, it was voted, 5-0, to endorse the plan as it does not show a subdivision.

#### **Belmont Country Club Land, ANR:**

On a motion of Mr. Hornig, seconded by Ms. Johnson, it was voted, 5-0, to endorse the plan as it does not show a subdivision.

#### 7 Hartwell Avenue, Sketch PSDUP:

Mr. Bob Buckley, attorney from Riemer and Braunstein representing the Russian School of mathematics was present.

This was CD-1 when amended in 2001 and is coming to establish a new Planned Development and go to Town Meeting. The major issue appears to be traffic and will have to look at the impacts on the Town's infrastructure.

#### **Board Comments:**

- Is there anything you are asking for that is not permitted for uses? *The only thing is non-confirming is the frontage and lot area*. It would be better to make it part of the CM District and would require a zoning change.
- The parking is problematic with the traffic with all the cars entering and exiting at the same time. The applicant needs to design a new circulation pattern.
- Want to see side and yard and front setbacks respected.
- Accessibility and multi-model transportation and pedestrian crossings need to be would need to be addressed.
- Did not see a landscape plan with the existing trees and those that will be removed and make the site look nice.
- When does the school operate? *Monday through Friday from 3:30 p.m. to 8:30 p.m. and 9 a.m. to 6p.m. on weekends with cars coming and going ever two hours.*
- 20 cars coming and going every 10 minutes is a lot of traffic.
- Is there a plan for public access (easement) on the corner for pedestrians to get to a good spot?

The Board will need to draft a decision for the next meeting.

#### 1106 Massachusetts Avenue, Review and Endorse Special Permit SSD decision:

Staff provided a draft decision and received no comments from Board members.

On a motion of Mr. Hornig, seconded, by Ms. Corcoran-Ronchetti, it was voted, 5-0, to approve the special permit for 1106 Massachusetts Avenue.

#### 1106 Massachusetts Avenue, preliminary Subdivision:

On a motion of Mr. Hornig, seconded, by Ms. Corcoran-Ronchetti, it was voted, 5-0, to approve The preliminary subdivision plan for 1106 Masssachusetts Avenue.

On a motion of Mr. Hornig, seconded, by Ms. Johnson, it was voted, 5-0, to authorize the Planning Director to accept on behalf of the Board the withdrawal from the applicant if it is given before Friday.

#### **Minutes Review and Approval:**

On a motion of Mr. Hornig, seconded by Ms. Johnson, it was voted, 5-0, to approve April 23, 2018, and April 26, 2018 as amended.

#### Fiscal Year 2019 Workplan Discussion:

The Fall Special Town Meeting will include some if not all of the following:

Belmont Country Club, North Hartwell Avenue initiative, 7 Hartwell Avenue, 331 Concord Avenue, 186 Bedford Street, Marijuana, Special Permit Residential Development, and the TMOD for Hartwell Avenue.

The Board discussed Mr. Creech's proposed items to the Planning Board Work plan 2018-2019.

#### **Board Reorganization:**

The Board held its annual election of officers.

On a motion of Mr. Canale, seconded by Mr. Creech, it was voted, 5-0, to elect Ms. Ginna Johnson as chair, Mr. Creech as vice chair, and Ms. Corcoran-Ronchetti as clerk.

On a motion, duly made and seconded, it was voted to adjourn the meeting at 9:51 p.m. The meeting was recorded by LexMedia.

The following documents used at the meeting can be found on the Planning Board website in Planning Board packets.

- Draft charge for the Special Permit residential Committee (2 pages).
- Agenda Item Summary and Staff recommendations for 17 Tower Road, ANR (2 pages)
- Plan of Land 17 Tower Road (1 page).
- Approval Not required for Belmont Country Club (1 page).
- Cover Letter from Riemer and Braunstein for 7 Hartwell Avenue (2 pages).
- PSDUP Document for 7 Hartwell Avenue (8 pages).
- Proposed plans for the Russian School of Mathematics (9 pages).
- Staff memo for 7 Hartwell Avenue (sketch PSDUP) (2 pages).
- Draft of Grant of Special Permit for 1106 Massachusetts Avenue (6 pages).
- Agenda Item Summary and Staff recommendations for 1106 Massachusetts Avenue (1 page).
- Richard Canale's comments to the draft SPRD charge (2 pages).
- Presentation for Getting net Zero Emissions Road map and recommendations.
- Mr. Creech Planning Board Work plan 2018-2019 (2 pages).